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FLIGHT TEST OF A COMPOSITE MULTI-TUBULAR SPAR MAIN ROTOR BLADE ON THE AH-1G HELICOPTER

Volume I - Materials, Design, and Test

Hughes Helicopters
Division of Summa Corporation
Culver City, Calif. 90230



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EUSTIS DIRECTORATE
U. S. ARMY AIR MOBILITY RESEARCH AND DEVELOPMENT LABORATORY
Fort Eustis, Vg. 23604

EUSTIS DIRECTORATE POSITION STATEMENT

The work reported herein was performed under Contract DAAJ02-74-G-0055 with Hughes Helicopter Company, Culver City, California, and Fiber Science, Inc., Gardena, California, as primary contractor and subcontractor respectively.

The data contained in this report are the results of flight and laboratory testing. The reported work was performed to determine the applicability of the filament winding co-cure fabrication process, in conjunction with the Multi-tubular Spar concept, in fabricating helicopter rotor blades with improved fatigue life, ballistic damage tolerance, low radar cross-section signature, and low production cost.



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PREFACE

This report was prepared by Hughes Helicopters, Division of Summa Corporation, Culver City, California 90230, for the U.S. Army Air Mobility Research and Development Laboratory, Fort Eustis, Virginia 23604, under Contract DAAJ02-74-C-0055.

Hughes Helicopters (HH) was the prime contractor and Fiber Science, Inc. (FSI) was the subcontractor. HH and FSI cooperated on the design, FSI fabricated the blades, and HH tested them. Mr. R. E. Head was HH program manager and Mr. L. J. Ashton was program manager at FSI. The Eustis Directorate technical monitors for the programs were Mr. I. E. Figge and Mr. N. J. Calapodas.

This final report on the development program for the composite multi-tubular spar (MTS) main rotor blade for the AH-1G helicopter is presented in three volumes: Volume I, Materials, Design, and Test; Volume II, Cost Estimates and Process Specifications; and Volume III (S), Ballistic Damage Tolerance and Radar Cross Section.

This volume documents the work done to establish composite material properties; to design the MTS blade; to develop the wet-filament winding (WFW) co-cure manufacturing process; and to evaluate the blade through laboratory, ground, and flight tests.

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INTRODUCTION

This volume describes the design of the multi-tubular spar (MTS) blade and testing to verify that the concept is viable for producing long-life, low-cost, ballistically tolerant composite main rotor blades.

The first step was establishing allowable loads for wet-filament-wound (WFW) components. The basic filament strength and stiffness had been documented, but information was needed on the specific characteristics, especially their fatigue characteristics, of WFW tubular and unidirectional filament components. Small specimens of both configurations were tested for static strength and stiffness in tension, compression, and shear, and their fatigue strength was documented. Compression/creep properties, static properties, and S-N data determined in these tests were used in the stress analysis of the blade.

Blade preliminary design work was concurrent with the materials test work. The basic blade design concept was established by the title of the program: "Multi-Tubular Spar." FSI and HH separately and together proposed a number of concepts for the blade, all based on the co-cure process. The midspan portion of the blade appeared amenable to any one of a number of different designs. The problems lay in the root and tip ends where a reliable mechanical connection between the midspan filaments and the end fittings was considered to be mandatory; reliance on interlaminar shear through the resin was to be avoided if at all possible. From nine root and six tip candidate designs, the final selection was made.

An integral part of the program was improving the WFW co-cure manufacturing technology to assure repeatable fabrication of aircraft quality primary structure components. A manufacturing technology program established the necessary processes and demonstrated them with two full-size "toolproofing" blades before building the eight blades for the test program. It was refined to the point where weight and center of gravity control had the same tolerances normally experienced with metal blade production technology. In going to a production composite blade program, even closer tolerances may be anticipated. The process specification used in fabricating the blades appears in Volume II.

HH and FSI cooperated in the final detail design of the blade with FSI preparing the engineering drawings, and HH performing the stress, weight, and dynamic analyses. This blade makes use of the WFW, co-cure process, has the dynamic characteristics necessary for operation on the AH-1G helicopter, has a calculated 3600-hour fatigue life, has ballistic tolerance to 23mm high explosive incendiary-tracer (HEI-T) projectiles, has low radar cross section compared with the production metal blade, is repairable, and can be produced at low cost.

Throughout the blade detail design process, close liaison was maintained between the tool designers and the WFW manufacturing engineers. Unlike aircraft structure where the designer can call for, say, an extrusion of a certain size made from some certain metal with a particular heat treat, the WFW components must be capable of: being wound in a reasonable shape (cylinder, cone, longo, etc), being moved from the winding machine to the blade mold, ending up in the mold in the proper location with the filaments going the proper direction(s), and, in certain instances, performing a built-in tooling function to aid in forcing all the components into their proper places in the mold. All this must be done while the resin remains in an uncured condition with pot life long enough to permit complete assembly before the resin is deliberately cured by the application of controlled heat and pressure as the final assembly process. As a result of this design/manufacturing integration, the MTS blade is a reliable structure that meets all the objectives of the program.

The laboratory tests for the full-scale MTS blade demonstrated that the blade strength, stiffness, and dynamic properties were suitable for flight. The eight blades were built as complete, full-length blades. All except the flight test blades were cut into segments with each segment assigned to a specific test. These tests, conducted in HH Structures Test Laboratory, established that the static and fatigue strength, stiffness, and dynamic characteristics of the MTS blade were in agreement with the predicted values, and that the concept was ready for ground and flight tests.

MTS blades were ground- and flight-tested on an AH-1G helicopter (Army S/N 67-15683), newly out of the Army's Corpus Christi Repair Depot. An instrumented 540 hub and two MTS blades were installed on the helicopter. The aircraft was tied to the ground for a 10-hour whirl test program, and then was flight tested for approximately 15 hours to explore 80 percent of the production AH-1G flight envelope. The ground test investigated the influence of rotor rpm, collective pitch setting, and cyclic pitch inputs. The flight tests covered a speed range up to 136 knots indicated airspeed (KIAS) and vertical accelerations between 0.3 and 1.9g. All basic AH-1G maneuvers except those that required ordnance firing were flown in this restricted envelope.

After the MTS blade flight test was completed, 540 metal blades were reinstalled on the helicopter, and a short program was flown for direct hub and mast loads comparison, and for a pilot qualitative comparison of the two blade systems. The pilot reported a smoother ride with the MTS blades, but otherwise no significant differences in handling qualities. The rotor loads measured for the MTS blades were the same as or a little lower than those for the 540 blades.

The success of this test program indicates that the all-composite MTS blade is a viable concept and should be introduced into an Army service evaluation program to establish its characteristics in the field.

SECTION I - PRELIMINARY DESIGN DEVELOPMENT

The MTS blade development work described in this section led to the detail design of the blade, and to the establishment of the blade fabrication process.

Allowable loads for WFW components were established. Small specimens of tubular and unidirectional filament configurations were tested for static strength and stiffness in tension, compression, and shear. Their fatigue strength was documented through tension-tension fatigue tests. Compression/creep properties were also established for temperatures ranging from -95°F to +160°F. The static properties and S/N data thus determined were used in the stress analysis of the blade.

MATERIAL PROPERTIES INVESTIGATION

The initial selection of materials for the MTS blade was based on FSI's previous experience with WFW structures. This indicated that only three filaments were worthy of consideration:

- a. S-1014 fiberglass filaments (Ferro Corporation)
- b. Thornel-300 graphite filaments (Union Carbide Corporation)
- c. Kevlar-49 aramid filaments (DuPont Corporation)

Table 1 shows their basic physical properties.

TABLE 1. COMPOSITE MATERIALS PHYSICAL PROPERTIES

		Ultimate Strength		Stiffness			
Material	Density (1b/in.3)			Compression (psi)	Tension (106 psi)	Shear (10 ⁶ psi)	
Kevlar-49 Aramid Filament	0.0524	325, 000	70,000	19.0	0.30		
Thornel-300 Graphite Filament	0.0636	325, 000	215,000	34.0	3.50		
S-1014 Fiberglass Filament	0.0900	325,000	215, 000	12.6	5.20		
APCO 2434/2347 Resin	0.0412	100-00		100			
APCO 2434/2340 Resin	0.0412	-	_ = 0.00 eV		•		

Data supplied by material manufacturers

Prior to this Contract, FSI, in conjunction with Applied Plastics Corporation (APCO) of El Segundo, California, investigated epoxy resin systems that were compatible with the WFW process. The principal combinations investigated were:

- a. APCO 2434/2347* 250°F cure
- b. APCO 2434 -0 room temperature cure
- c. APCO 2450/2 41 two-phase resin
- d. APCO 2450/2342 two-phase resin
- e. APCO 2430A/2347 brominated resin

The two-phase resins were supposed to improve fatigue strength and the brominated resin was fire retardant but these three resins showed inferior fatigue strength characteristics so were rejected from further consideration.

A test program was conducted to evaluate structural properties of WFW materials. Three configurations of test specimens were used: tubular, "fan belt", and cylindrical. Tests were made on a total of 169 individual specimens to determine the static and fatigue strength of the candidate blade materials.

Tubular specimens, Figure 1, were wet-filament wound as a hollow tube with test-fixture end pieces integrally wound on at each end. The wrap angle terminology for test specimens is shown in Figure 2. Some tubular specimens were tested in an undamaged state; others were tested in a damaged condition, i.e., with a 0.25-inch diameter hole drilled through and with a 5.56 mm API bullet shot through.

^{*}Number before the slash mark denotes resin, number after the slash denotes hardener.



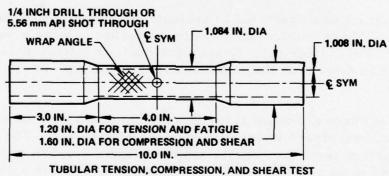


Figure 1. Tubular test specimens.

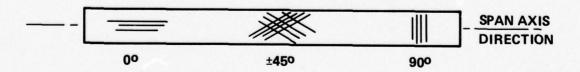
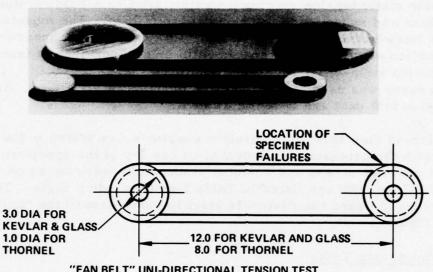


Figure 2. Wrap angle terminology.

The "fan belt" specimens, Figure 3, were fabricated by wet-filament winding a band of unidirectional filaments around grooved-disc, metal end fittings.



"FAN BELT" UNI-DIRECTIONAL TENSION TEST

Figure 3. "Fan belt" test specimens.

The cylindrical specimens, Figure 4, were wet-filament, hoop wound as a hollow cylinder with the middle being S-glass and each end Kevlar-49.

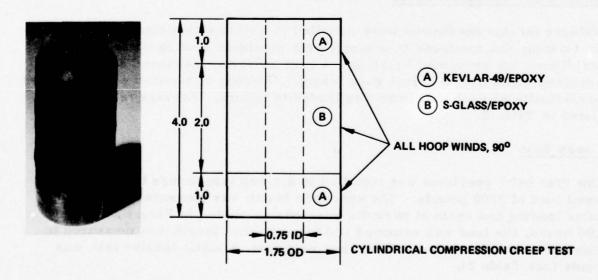


Figure 4. Cylindrical test specimen.

Static Tension Tests

Each tubular static tension specimen was installed in a Baldwin Universal Test Machine and static loads were applied to failure. The mounting precluded the introduction of bending loads. An extensometer measured the axial deflection of each tubular specimen in inches-per-inch of travel, and a load-deflection strip-chart recorder monitored the applied load. The load-deflection curve was used to calculate the modulus of elasticity. Average static tension test data are listed in Table 2.

Each Kevlar-49 "fan belt" configuration specimen was tested in the same manner, with the extensometer mounted on one leg of the specimen. The calculated ultimate stress and modulus of elasticity were based on the total area of both legs, and are listed in Table 2 as 0° winding angle. The failures always occurred where the filaments start to curve around the "pulley", as shown in Figure 3.

Static Compression Tests

Static compression tests were conducted on tubular specimens only. A stabilizing bar inside each specimen prevented buckling, and an extensometer measured deflection. The load-deflection strip-chart recorder monitored the applied load and the load-deflection curve was used in calculating the modulus of elasticity. Each compression specimen was tested to failure. Table 2 lists the average test results.

Static Shear (Torsion) Tests

Tubular torsion specimens were installed in a fixture that applied shear loads by twisting the specimens in a manner that precluded bending while an internal stabilizing bar prevented buckling. A gage indicator measured degrees of specimen twist over a 2-inch gage length. Degrees of rotation were recorded periodically as each specimen was loaded to failure. Average test data are listed in Table 2.

Creep Test

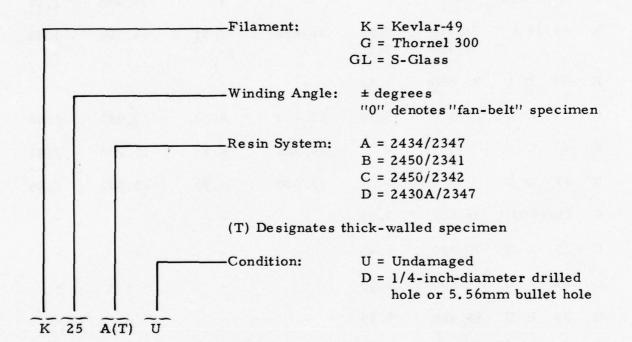
One "fan belt" specimen was installed in a creep test fixture that applied an axial load of 3500 pounds. The specimen length was measured immediately after loading and again at periodic intervals as plotted in Figure 5. After 100 hours, the load was removed and the specimen length was measured to determine permanent set. After the creep test, a static tension test was made (see Table 2).

TABLE 2. AVERAGE ULTIMATE STATIC STRENGTH AND STIFFNESS TEST DATA

				Tension		Compression		Shear	
				Stress (psi)	Modulus (10 ⁶ psi)	Stress (psi)	Modulus (10 ⁶ psi)	Stress (psi)	Modulus (10 ⁶ psi)
K	0	A	U	130,900	9.21	<u>-</u>	65 A 950		
K	25	A	U D	94,460 37,430	3.84 3.71	13,490	3.24	11,880	1.31
K	45	A	U D	20,380 14,880	0.86 0.85	13,500	2.57	12,220	1.73
K	45	A(T	') U	-	-	<u>-</u>	-	24,860	1.97
K	15/	45 .	A U D		3.87 3.86	16,690	3.31	14,350	1,43
K	45	В	U	75,820	3.43	<u>.</u>	-	-	-
K	25	С	U	84,370	5.18	13,180	4.50	9,940	1.06
K	45	С	U	-		10,500	0.85	11,770	1.91
K	45	D	U			13,320	0.96	15,000	2.29
K	15/	45	D U	56,560	3.55	-		-	-
G	25	A	U	73,720	6.46	-	-	-	-
G	45	A	U	15,260	1.50	-	-	-	
G	25	В	U	68,920	5.59	-	-	1	•
G	45	В	U	16,950	1.55	-	-	-	
G	25	С	U	75,190	6.03	21,770	5.56	22,790	2.13
G	45	С	U	-	-	17,490	Take no	32,840	2.66
GL	25	A	U	94,270	4.19		-	-	
GL	45	A	U	25,310	1.88	•	-	37,440	1.59

TABLE 2 - Continued

			Tension		Compression		Shear	
1 9 9 1 1 9 9 1			Stress (psi)	Modulus (10 ⁶ psi)	Stress (psi)	Modulus (10 ⁶ psi)	Stress (psi)	Modulus (10 ⁶ psi)
GL 25	В	U	85,030	3.72	•	16.0 <u>-</u>		
GL 45	В	U	22,160	1.55		•		
GL 25	С	U	-	ra o -	17,030	4.12	13,140	1.06
GL 45	С	U	-	-	9,920	1.46	12,590	1.89



Average fiber volume ratio equals 41 percent.

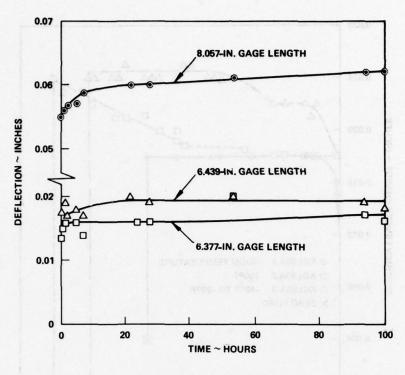


Figure 5. "Fan belt" configuration creep test - total deflection versus time.

Three cylindrical compression specimens were individually tested for creep. One specimen was tested at room temperature, one at 160°F, and one at -45° to -95°F. A measuring device recorded changes in length of the test specimen under a compression load of 2474 pounds. The data is plotted in Figure 6.

Fatigue Tests

Each end of each tubular fatigue test specimen was bonded to a set of grips and was installed in a constant-amplitude fatigue machine which ran at 30 hertz. An airstream passed through the test section of each specimen to keep it cool. Thermocouples on the inside and outside of the specimen monitored temperature, which was not allowed to exceed 95°F. The test machine had a safety device to prevent overloads and automatically shut down if the specimen failed.

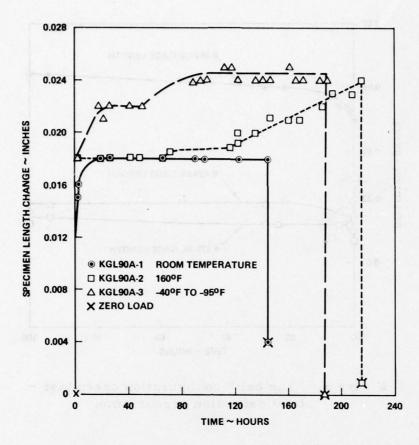


Figure 6. Cylindrical configuration compression creep test.

Each "fan belt" fatigue test specimen was installed in a test machine that used a hydraulic closed-loop servomechanism to apply and control the load cycle. The load was applied in the form of a sine wave and was monitored on a direct-reading oscilloscope. Safety devices prevented inadvertent overloads and shut down the system in event of a malfunction. Each "fan belt" fatigue specimen was tested at a rate of 20 hertz.

The tubular and "fan belt" fatigue specimens were tested at a load ratio of one-tenth; that is, the ratio of minimum load to maximum load was 0.1. Each specimen was tested to failure or until 10 million cycles had been applied, whichever occurred first. If a "runout" occurred (10 million cycles), the cyclic load was increased and testing continued until the specimen failed. Typical data for Kevlar-49 is plotted in Figures 7, 8, and 9 in the familiar load/cycle type of curve.

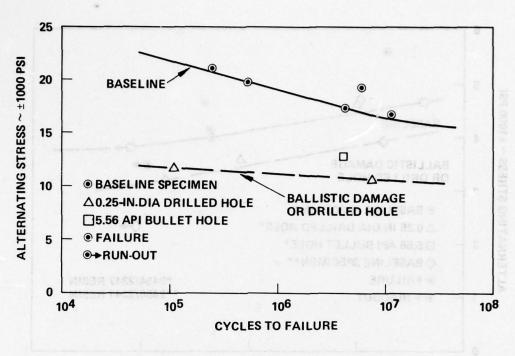


Figure 7. S-N curve for ±25° Kevlar-49/epoxy tubular specimen.

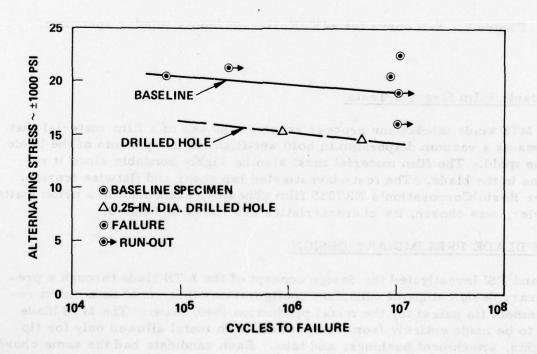


Figure 8. S-N curve for ±15°/±45° Kevlar-49/epoxy tubular specimen.

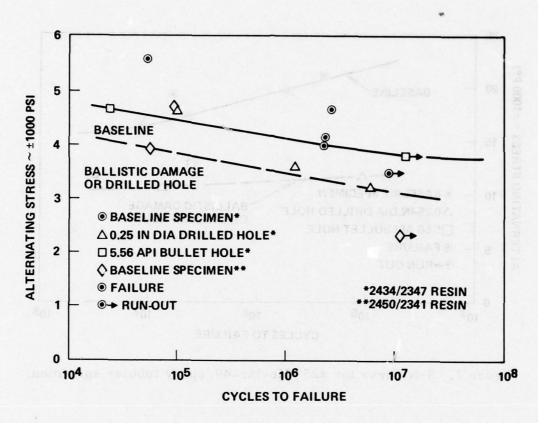


Figure 9. S-N curve for ±45° Kevlar-49/epoxy tubular specimen.

Bondable Film Strength Tests

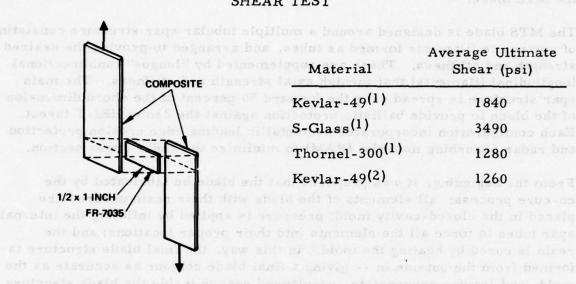
The MTS blade fabrication process requires the use of a film material that serves as a vacuum diaphragm to hold wet-filament components of the blade in the mold. The film material must also be highly bondable since it remains in the blade. The tests investigated lap shear and flatwise tension. Fiber Resin Corporation's FR7035 film adhesive, suspended in a nylon matte carrier, was chosen; its characteristics are listed in Table 3.

MTS BLADE PRELIMINARY DESIGN

HH and FSI investigated the design concept of the MTS blade through a preliminary design study of candidate configurations that would be a direct replacement (in pairs) for the metal production (540) blade. The MTS blade was to be made entirely from composites, with metal allowed only for tip weights, attachment bushings, and tabs. Each candidate had the same chord, twist, and airfoil as the 540 blade, and had dynamic characteristics

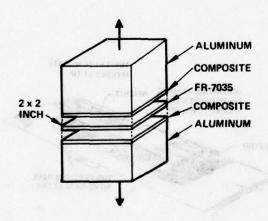
TABLE 3. FR-7035 FILM ADHESIVE SHEAR AND TENSION STRENGTH

SHEAR TEST



Material	Average Ultimate Shear (psi)		
Kevlar-49(1)	1840		
S-Glass(1)	3490		
Thornel-300(1)	1280		
Kevlar-49(2)	1260		
Kevlar-49(2)	1260		

TENSION TEST



Material	Average Ultimate Shear (psi)
S-Glass(1)	4700
Kevlar-49(1)	4700
Thornel-300(1)	1800

⁽¹⁾ APCO 2434/2347 Resin

⁽²⁾ APCO 2434/2340 Resin

suitable for flight on the AH-1G. An alteration of the airfoil shape inboard of the 32-percent radius station (blade station (BS) 85) for root-end strengthening was permitted. Figure 10 provides the nomenclature used in describing the MTS blade.

The MTS blade is designed around a multiple tubular spar structure consisting of composite filaments formed as tubes, and arranged to provide the desired strength and stiffness. These are supplemented by "longos" (unidirectional longitudinal filaments) that furnish axial strength and stiffness. The main spar structure is spread over the forward 50 percent of the chord dimension of the blade to provide ballistic protection against the 23mm HEI-T threat. Each configuration incorporates nonmetallic leading edge erosion protection and radar-absorbing material (RAM) to minimize the radar cross section.

From the beginning, it was proposed that the blade be fabricated by the co-cure process: all elements of the blade with their resin uncured are placed in the closed-cavity mold; pressure is applied by inflating the internal spar tubes to force all the elements into their proper locations; and the resin is cured by heating the mold. In this way, the final blade structure is formed from the outside in -- giving a final blade contour as accurate as the mold, and leaving appropriate, preplanned spaces inside the blade structure

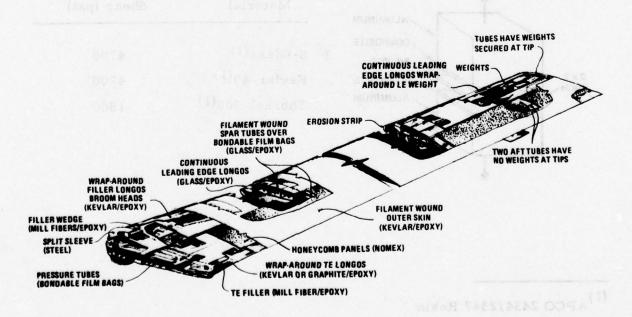


Figure 10. MTS blade nomenclature.

to accommodate tolerances. The co-cure process results in a very strong structure because all elements are forced into intimate contact while still in a soft, flexible condition. Then the resin is cured only once, creating a secure chemical bond.

The constant-airfoil, midspan section of the blade could be designed successfully in a number of configurations, but the main problem was integrating this section of the blade with a satisfactory root end and tip end. Designs in which a mechanical tie of the filaments was made to the metal components at the root and tip were judged to be more satisfactory than designs that relied on interlaminar shear through resins and adhesives.

Of the many configurations considered, nine root-end/midspan designs and six tip-end designs were considered for final evaluation and selection. These are discussed below.

Blade-Root/Midspan Configuration Descriptions

The basic blade structure sections for each configuration are shown in Figure 11 in which the vertical scale of the drawings is enlarged four times.

Configuration 1 (Figures 11 and 12). All spar longos wrap around the main retention bolt bushing. They are formed and precured into a C-shaped leading edge pack. Three filament-wound tubes, located just aft of the longos, formed the multi-tubular spar. A thick skin made from a flattened, filament-wound tube encloses the multi-tubular spars and the leading edge longos.

The trailing edge portion consists of thin honeycomb panels covered with a skin made from a filament-wound tube that has been cut open. The triangular cross section trailing edge longo wraps around the drag brace bushing, and two thin-walled filament-wound tubes complete the inner structure.

In the root area additional strength and flapwise bending stiffness is achieved by adding "broom longos" top and bottom just below the spar longos. This longo material runs predominantly spanwise in the blade, but fans out chordwise to the full width of the spar structure. It wraps around the main retention bushing for good mechanical attachment and extends out to the beginning of the constant section of the blade (BS 85). This is a feature of all blades shown here. It replaces the stack of doubler plates commonly used in metal blades, but is internal to the blade moldline rather than external.

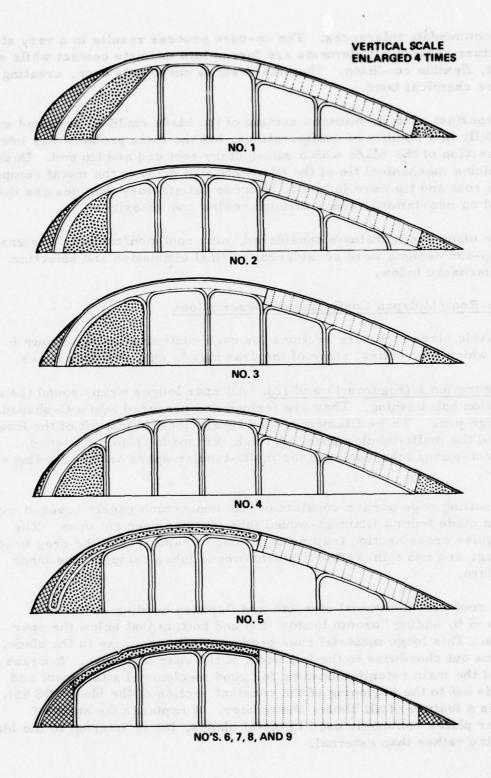


Figure 11. Basic blade structural sections.

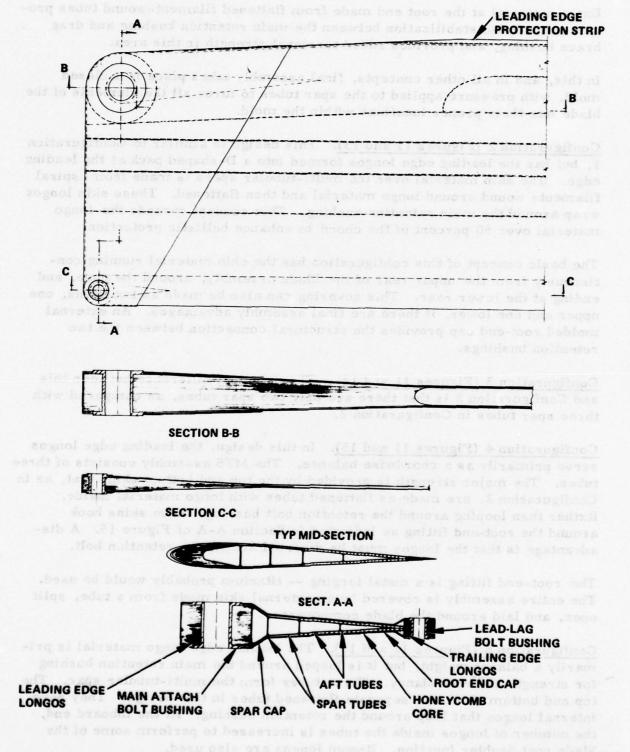


Figure 12. Blade root Configuration 1.

Extra material at the root end made from flattened filament-wound tubes provides chordwise stabilization between the main retention bushing and drag brace bushing, and provides added torsional strength in this area.

In this, and in all other concepts, final assembly takes place in a closed mold, with pressure applied to the spar tubes to force all the elements of the blade into their proper locations within the mold.

Configuration 2 (Figures 11 and 13). This design is similar to Configuration 1, but has the leading edge longos formed into a D-shaped pack at the leading edge. The skin material over the multi-tubular spars is made from spiral filaments wound around longo material and then flattened. These skin longos wrap around the main retention bushing. This concept spreads the longo material over 50 percent of the chord to enhance ballistic protection.

The basic concept of this configuration has the skin material running continuously from the upper rear of the blade assembly, around the nose, and ending at the lower rear. This covering can also be made as two skins, one upper and one lower, if there are final assembly advantages. An external molded root-end cap provides the structural connection between the two retention bushings.

Configuration 3 (Figures 11 and 14). The principal difference between this and Configuration 2 is that there are only two spar tubes, as compared with three spar tubes in Configuration 2.

Configuration 4 (Figures 11 and 15). In this design, the leading edge longos serve primarily as a chordwise balance. The MTS assembly consists of three tubes. The major strength is provided by the top and bottom skins that, as in Configuration 2, are made as flattened tubes with longo material inside. Rather than looping around the retention bolt bushing, these skins hook around the root-end fitting as indicated in Section A-A of Figure 15. A disadvantage is that the longos must be diverted around the retention bolt.

The root-end fitting is a metal forging -- titanium probably would be used. The entire assembly is covered by an external skin made from a tube, split open, and laid around the blade components.

Configuration 5 (Figures 11 and 16). The leading edge longo material is primarily a balance weight, but it is looped around the main retention bushing for strength and redundancy. Three tubes form the multi-tubular spar. The top and bottom skins are separate flattened tubes in this design. They have internal longos that loop around the retention bushing. At the inboard end, the number of longos inside the tubes is increased to perform some of the blade root doubler function. Broom longos are also used.

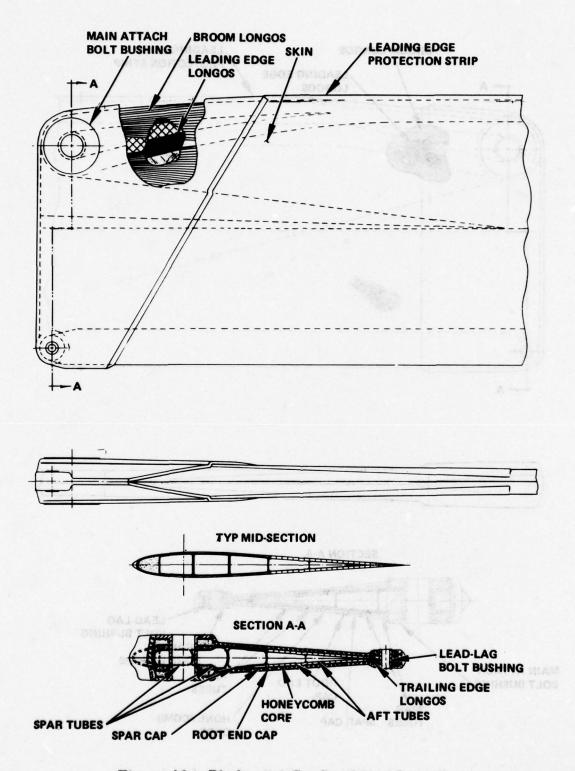


Figure 13. Blade root Configuration 2.

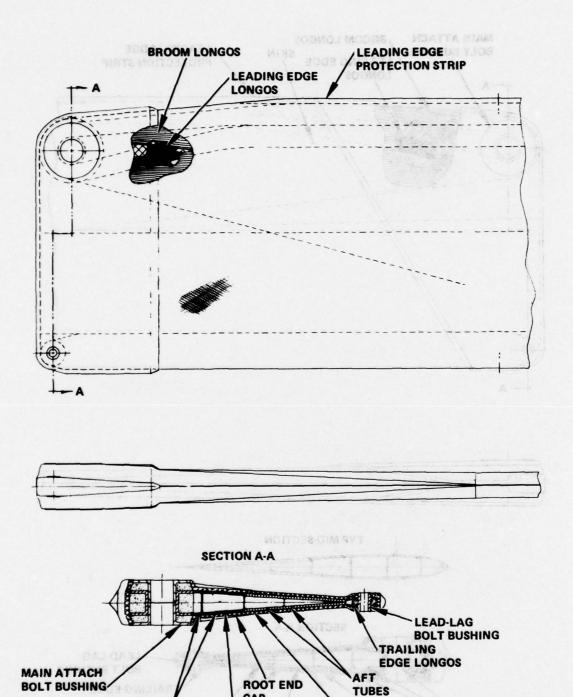


Figure 14. Blade root Configuration 3.

CAP

TUBES SPAR CAP

HONEYCOMB

CORE

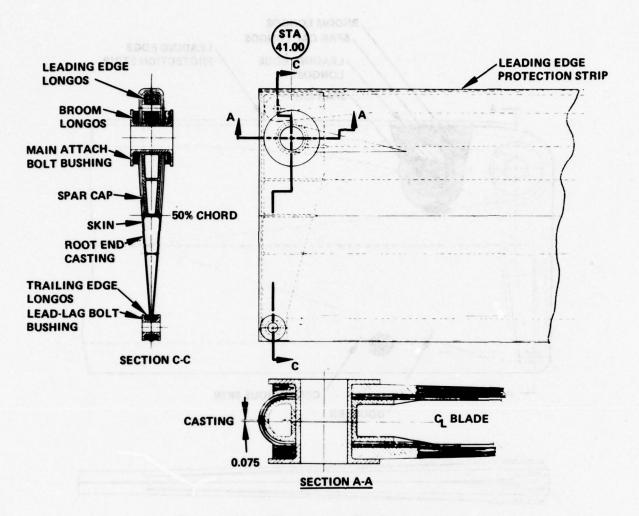
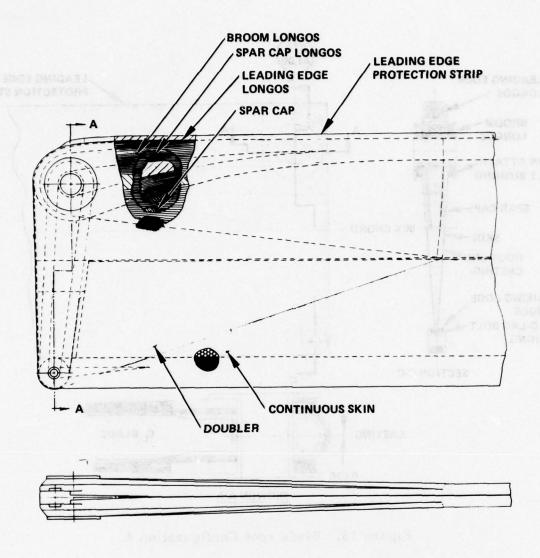


Figure 15. Blade root Configuration 4.

The root-end bushing chordwise stabilization is accomplished by a molded compression strut between the bushings and longo elements wrap around them to take tension loads.

Configuration 6 (Figures 11 and 17). Four filament-wound tubes form the MTS structure. A nonstructural leading edge weight provides chordwise balance. A spar longo is formed into two packs, one top and one bottom. They loop around the retention bolt bushing and fan out in the chordwise direction to cover the forward half of the blade chord. Additional broom longo material is added at the root end to perform the doubler function.



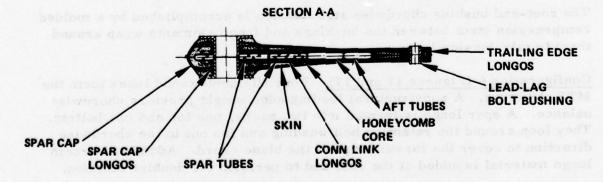


Figure 16. Blade root Configuration 5.

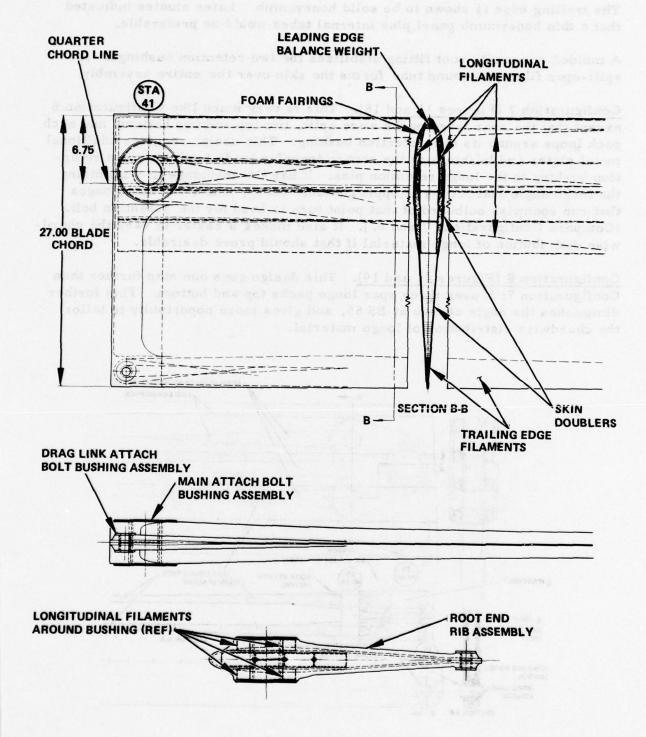


Figure 17. Blade root Configuration 6.

The trailing edge is shown to be solid honeycomb. Later studies indicated that a thin honeycomb panel plus internal tubes would be preferable.

A molded composite root fitting stabilizes the two retention bushings. A split-open filament-wound tube forms the skin over the entire assembly.

Configuration 7 (Figures 11 and 18). This is very much like Configuration 6 except that the spar longo packs were split, two top and two bottom, and each pack loops around its own retention bushing. This design requires additional metal plates and bushings at the root to transfer loads from the main retention bushing to the longo retention pins. It has the advantage of minimizing the longo angle that occurs at approximately BS 85, where the spar longos that run spanwise outboard of that point turn to head for the retention bolt. (Compare Configurations 7 and 6.). It also makes it easier to vary the chordwise distribution of longo material if that should prove desirable.

Configuration 8 (Figures 11 and 19). This design goes one step further than Configuration 7; it uses three spar longo packs top and bottom. This further diminishes the angle change at BS 85, and gives more opportunity to tailor the chordwise distribution of longo material.

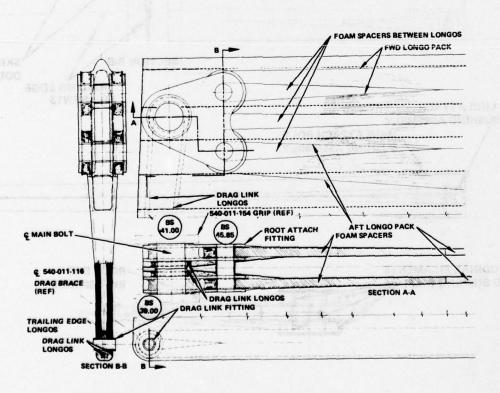


Figure 18. Blade root Configuration 7.

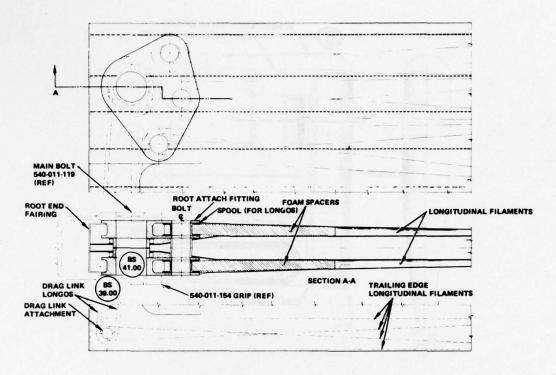


Figure 19. Blade root Configuration 8.

There is a small ballistic tolerance benefit near the blade root for Configurations 7 and 8, as opposed to Configuration 6, since the longos tie into multiple points.

Configuration 9 (Figures 11 and 20). The spar longo material is fabricated as three packs, each of which runs continuously from the blade tip, inboard around the root fitting, and back again to the tip. This arrangement allows chordwise tailorability of the longo material and avoids interruption of the longos in the region of the retention bolt bushing, as occurs in Configuration 4. A root-end metal forging is required to transfer loads from the longos into the retention bolt.

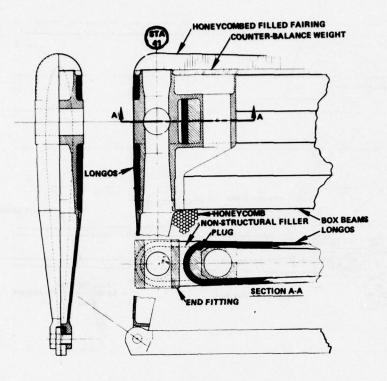


Figure 20. Blade root Configuration 9.

Blade Tip Configuration Descriptions

Configuration A (Figure 21). The four tip weights are distributed, one to each spar tube. The upper and lower contour of each weight is designed for a net fit within the blade structure. The outboard end of each weight is shaped much like the lip of a beverage bottle and forms part of the spar tube winding fixture, with the filaments wound around it to mechanically trap the weight among the fibers.

Each weight has a threaded hole through its length to accommodate adjustable weight elements. This feature is included in all depicted blade tip designs.

Configuration B (Figure 22). This configuration incorporates three wound-in weights as described for Configuration A. In addition, a contoured nose weight is pinmed to the leading edge.

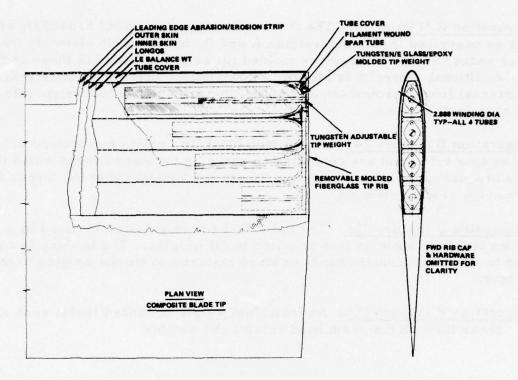


Figure 21. Blade tip Configuration A.

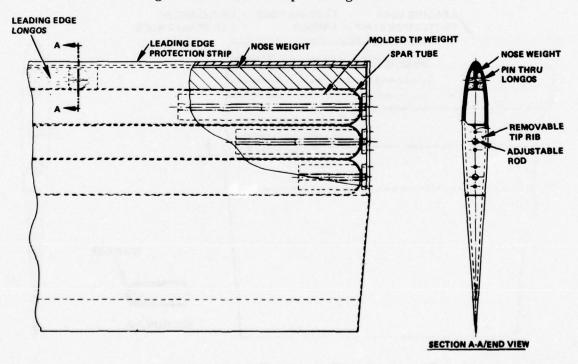


Figure 22. Blade tip Configuration B.

Configuration C (Figure 23). The three spar tubes are wound around tip elements as described for Configurations A and B, but these tip elements function only as anchor nuts. A one-piece molded tip weight is bolted to these anchor nuts. Additional restraint is attained by looping the upper and lower skin with internal longos around the end of the tip weight to key the weight into the blade (see Section A-A).

Configuration D (Figure 24). Three individual tip weights are located in line with the spar tubes and are contoured to serve as bushings around which the longos are wrapped. This provides a direct mechanical tie to the longos for optimum tip weight retention.

Configuration E (Figure 25). The individual tip weights are retained by a common bushing assembly that is bolted to all weights. The bushing is contoured to accept concentric bands of longo material to tie the weights to the structure.

Configuration F (Figure 26). An individual weight is bonded inside each spar tube. Shear through the resin bond retains the weights.

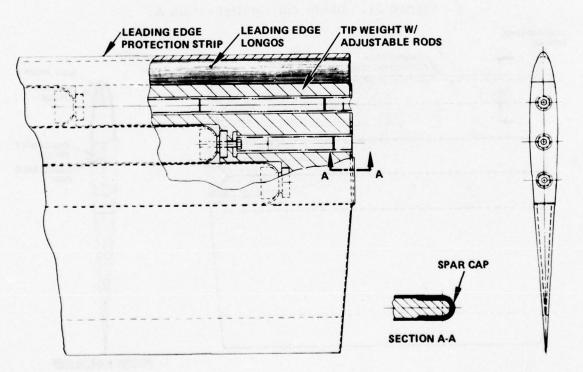


Figure 23. Blade tip Configuration C.

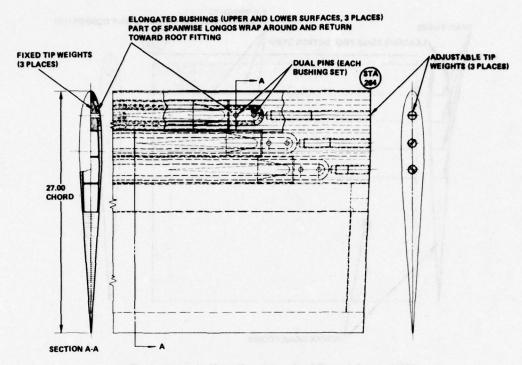


Figure 24. Blade tip Configuration D.

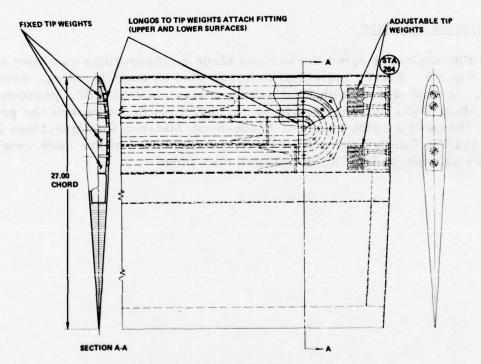


Figure 25. Blade tip Configuration E.

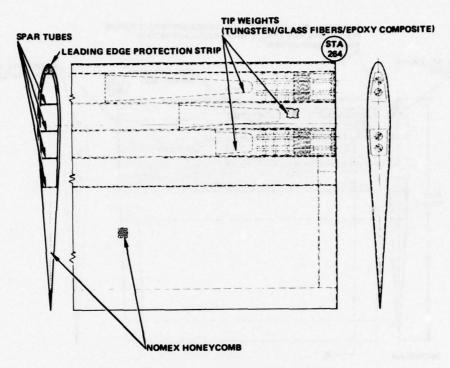


Figure 26. Blade tip Configuration F.

Configuration Selection

HH and FSI engineers rated the various blade configurations as shown in Tables 4 and 5. Eleven individual factors, plus an overall rating, were given to each. In cooperation with Eustis Directorate, USAAMRDL, personnel, a final configuration was selected to be carried through the rest of the program. This was a combination of Blade-Root/Midspan Configurations 1, 5, and 6, and Tip Configuration A -- later, an adaptation of the nose weight retention scheme in Tip Configuration B was added.

TABLE 4. BLADE ROOT CONFIGURATION RATING

Configuration

00.22809	1*	2	3	4	5*	6*	7	8	9
Structural Integrity	4	4	4	4	4	4	4	4	4
Low Cost	4	3	3	2	4	4	3	3	2
Ballistic Tolerance	1	4	4	3	4	3	3	3	4
Design Simplicity	4	3	3	3	3	3	3	3	3
Minimum Components	4	3	3	3	3	3	3	3	3
Development Risk	4	4	4	2 .	4	4	4	4	2
Radar Cross Section	4	4	4	4	4	4	4	4	4
Minimum Machining	4	4	4	2	4	4	3	3	2
Fits and Tolerance	4	4	4	3	4	4	3	3	3
Repairability	4	4	4	4	4	4	4	4	4
Fabrication Ease	4	3	3	2	3	3	3	3	2
Overall Rating	4	3	3	2	4	4	3	3	2

Excellent 4, Good 3, Fair 2, Poor 1

^{*}Selected for integration into the final design.

TABLE 5. TIP CONFIGURATION RATING

Configuration

	A *	B*	С	D	E	F
Structural Integrity	3	3	4	4	4	2
Low Cost	4	3	2	2	2	2
Ballistic Tolerance	2	2	4	3	3	1
Design Simplicity	3	3	2	2	2	4
Minimum Components	3	3	2	2	4	4
Development Risk	4	3	4	3	3	3
Radar Cross Section	3	3	3	3	3	3
Minimum Machining	4	4	4	2	2	3
Fits and Tolerance	4	4	4	4	4	4
Repairability	2	2	2	2	2	2
Fabrication Ease	4	3	2	2	2	2
Overall Rating	4	4	3	2	2	1

Excellent 4, Good 3, Fair 2, Poor 1

^{*}Selected for integration into the final design.

MANUFACTURING TECHNOLOGY DEVELOPMENT

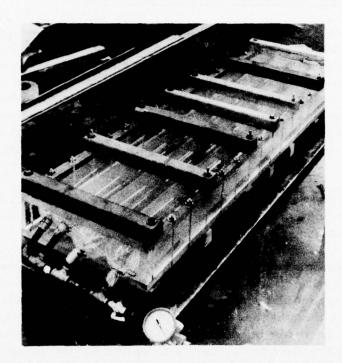
The MTS blade contract specified that FSI was to be the subcontractor for fabricating the blade. This company had developed the WFW process through several military and commercial programs and had reached a rather high level of sophistication. The WFW process was ready to use in the MTS blade, except for a few manufacturing details. The contract allowed for improving the WFW and assembly processes, and included time and funds for building as many as three full-size toolproofing blades while refining the overall technique. It was later determined that only two toolproofing blades were needed.

The manufacturing technology development effort began with rather simple fabrication tests and culminated in building full-scale MTS blades for laboratory and flight testing.

The MTS blade design requires several WFW spar tubes which are wound with circular cross sections and then deformed in the blade mold into approximately trapezoidal shapes with straight, vertical walls where they intersect. It was thought that this would happen automatically but, nevertheless, tests were made in which round tubes were placed into a mold and pressurized. In the first test, four thin-walled polyethylene tubes were inflated inside a rectangular box (Figure 27, top). Then WFW fiberglass tubes were inflated inside a mold and the tubes were cured (Figure 27, bottom). The tube intersections were straight and vertical, giving assurance of success for the actual blade.

The tip weight design calls for metal tip weights to be wound into two of the spar tubes. Again, the tubes are wound round and then forced into a trapezoidal shape in the blade mold. The tip weight has a trapezoidal cross section the same as the finished tube, and a circular neck into which the filaments are wound for mechanical entrapment. A tip weight was simulated by a wooden block and a tube was wound around it; then the tube was forced into a rectangular shape, and cured (Figure 28). This procedure was judged satisfactory.

These activities were followed by making a full-size fiberglass shell-type blade mold with proper chord and airfoil section, but only 4 feet long and with no twist (Figure 29). Two blade specimens were assembled and cured to evaluate the fabrication technique. The process was straightforward and gave confidence for proceeding with construction of the complete blade. One of these 4-foot specimens was ballistically tested against 23mm HEI-T projectiles. The ballistic test proved the rip-stopping function of the interwound filaments but showed that a plastic film material, used as a vacuum



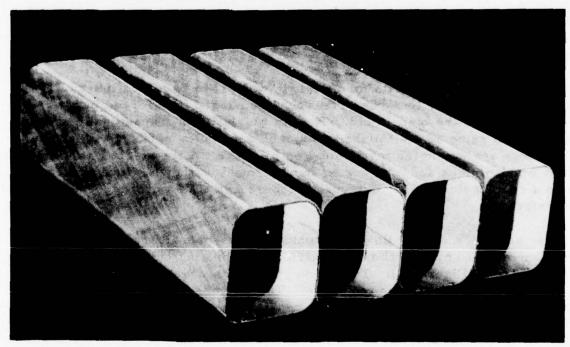


Figure 27. Spar tube technology demonstration.

diaphragm in the blade as a manufacturing aid, could not withstand ballistic shock loads. This finding led to a search that culminated in the selection of a film adhesive material held in a nylon matte carrier. It bonded well to the other materials in the blade and served satisfactorily as a vacuum diaphragm to hold the blade components in place in the mold.

Three manufacturing trials were made to establish methods for fabricating the spar cap which is a flattened, thick-walled tube. The first was a simple test that consisted of winding a short length of Kevlar-49 tube having a 0.072-inch-thick wall, and then flattening it to demonstrate that it could be compressed without wrinkling. The second test combined longos into the spar cap by winding two layers of helical filaments, laying on the longos, completing the helical wraps, and then flattening the tube. Both trials were satisfactory but the combined longo/helical tube design was discarded in favor of a design that wound each component separately. The third trial was for the purpose of winding the spar cap tube on a film adhesive mandrel, removing the film backing, and flattening the tube. The method that evolved and was used to build the spar caps for the blades required a solid metal mandrel with a close-fitting, inflated cover made from polyethylene film. That film was covered with adhesive film that had its backing sheet against the polyethylene. After the wet Kevlar filaments were wound over the adhesive film, the metal mandrel, polyethylene bag, and adhesive backing sheet were pulled out and the tube was easily flattened.

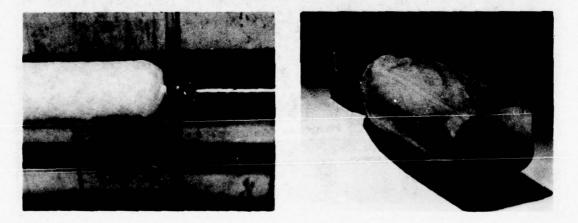


Figure 28. Spar tube tip weight technology demonstration.

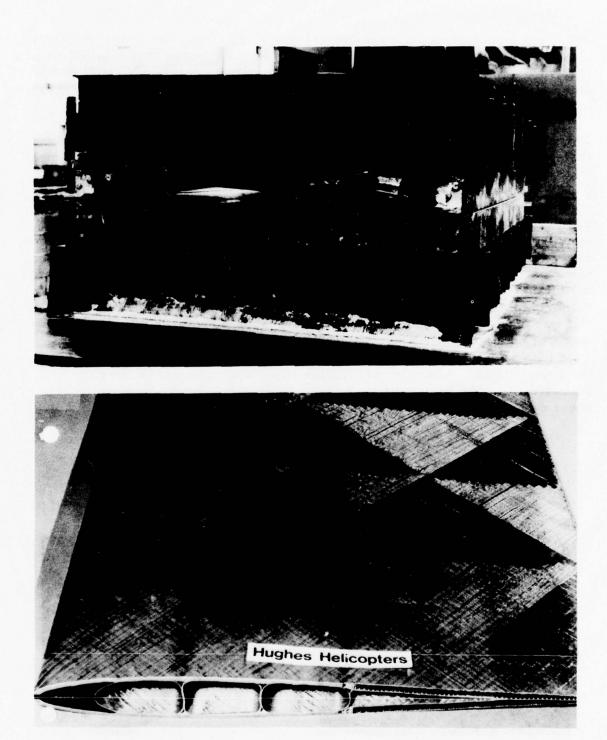


Figure 29. Four-foot mold and blade for co-cure process development.

The full-scale blade mold, which is shown open in Figure 30 and closed in Figure 31, was built to the contour of the 540 metal blade outboard of BS 85. Inboard of BS 85 the contour was altered to accommodate the root features of the MTS blade. This mold is a two-piece fiberglass shell that has two layers of graphite cloth molded into each mold half to serve as integral electric heaters. The shells are backed by square fiberglass tubes that distribute the mold pressure loads to a steel backup structure and minimize differential thermal stresses. Recesses formed into the mold surfaces serve to locate the metal blade root bushings and leading edge tip weight. Long threaded rods clamp the two mold halves together for curing the blade. Notched indexing plates at each end of the mold (Figure 32) align the spar tubes.

Two full-scale toolproofing blades (Figure 33), designated "A" and "B", were built to check out the procedure. These were complete in all aspects, except that "A" had wooden tip weights, and both "A" and "B" had aluminum blade root bushings. These blades showed up several factors in the production process that needed improvement including:

- a. Resin control
- b. Winding tension
- c. Spar tube diameter control
- d. Orientation of longo filaments
- e. Weight control
- f. Center of gravity location
- g. Pressure leaks during cure
- h. Spar tube location
- i. Blade surface treatment
- j. Vacuum diaphragm

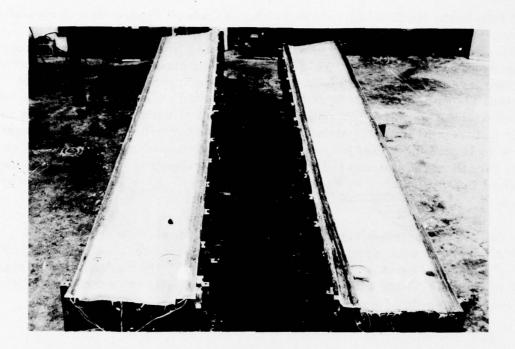


Figure 30. Open blade mold.

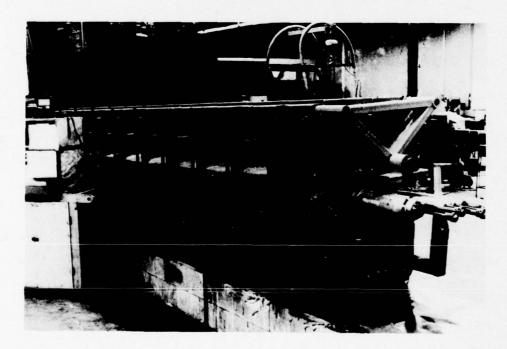


Figure 31. MTS blade mold.

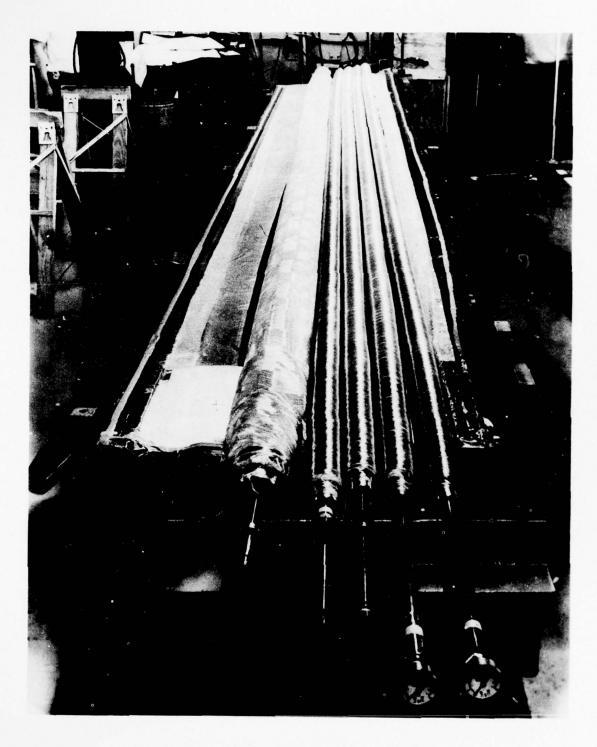


Figure 32. Blade mold indexing fixtures.

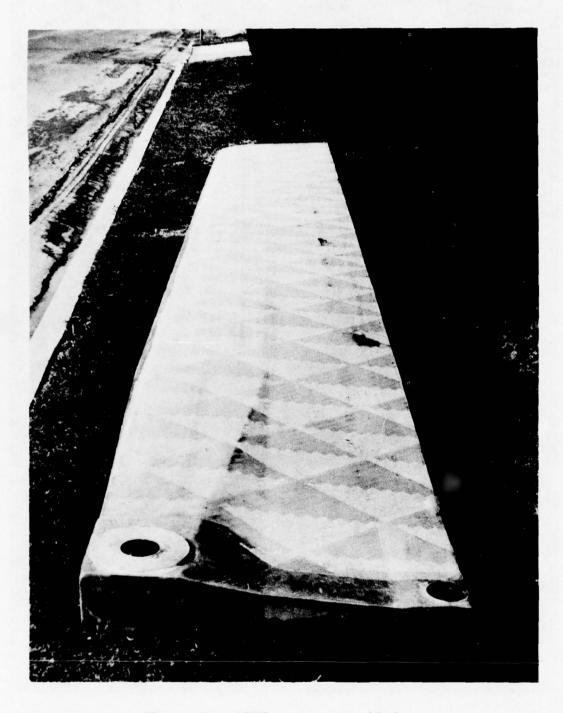


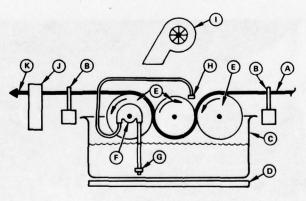
Figure 33. MTS toolproofing blade.

Resin Control and Winding Tension

The first two problem areas were interrelated. The WFW process leads dry filaments from spools through a resin impregnator (Figure 34) that thoroughly wets the filaments with a metered amount of resin, and delivers them in a uniform band to the component being wound. This band must be delivered with low tension in it. The dry filament rovings pass through a comb that keeps them aligned, and then between three heated rollers. From the rollers they go through another comb and through the winding eye. A systolic pump, driven by the final roller, pumps warmed resin onto the dry filaments as they pass over the rollers.

The resin is held at constant temperature to keep it at uniform viscosity. The rollers themselves are heated to aid in making the resin flow into each filament roving to thoroughly impregnate it. The winding eye collects the individual rovings, aligns them side-by-side in a uniform band, and dispenses them to be wound as tubular elements or longos.

The power to operate the impregnator comes from the machine that winds the blade components. It pulls the filaments through the impregnator, which turns the rollers; they, in turn, force resin into the rovings. This device requires a 4- to 6-pound tension in a 15-roving band; that force is compatible with winding the filament on the inflated plastic mandrels used in making the MTS blade.



- DRY ROVING BAND FROM SPOOLS OF FILAMENTS
- COMB TO ALIGN FILAMENTS RESIN RESERVOIR RESERVOIR HEATER
- IMPREGNATION ROLLER (3)
- SYSTOLIC PUMP
- PUMP INLET WITH METERING ORIFICE
- **RESIN DISPENSING OUTLET**
- HOT AIR BLOWER
- HOT AIR BLOWER WINDING EYE TO ALIGN FILAMENTS WET FILAMENT BAND TO WINDING MACHINE (4 TO 6 POUNDS TENSION)

Figure 34. Resin impregnator.

This impregnator maintains a constant ratio of resin weight to filament weight. It must be adjusted for the number of rovings being impregnated and the speed at which the filaments are drawn through it. An adjustable orifice in the pump's suction line meters the amount of resin being delivered. Resin impregnation is calibrated by first weighing a 60-foot-long band of dry rovings, and then weighing an equal-length band of wet rovings dispensed at the speed to be used in the WFW process. The orifice is adjusted until the dry- to wet-filament weight ratio is the specified value. As a further weight control measure, the winding mandrel is weighed before and after the winding process. The differential weight is compared with the calculated weight of the wound part (including the excess material that must be wound beyond each end of the actual part length). Agreement within ±3 percent is maintained.

Spar Tube Dimensional Control

Spar tube dimensional control is achieved by using the bladder fabrication tool shown in Figure 35. This takes a Tedlar film sheet, folds it, and bonds the edges to make a bladder whose circumference is precisely held. When the bladder is placed on the winding machine (Figure 36) its diameter is measured at several stations along its length to make sure it is within tolerance. After the tube is wound, the diameter is again measured for tolerance control.

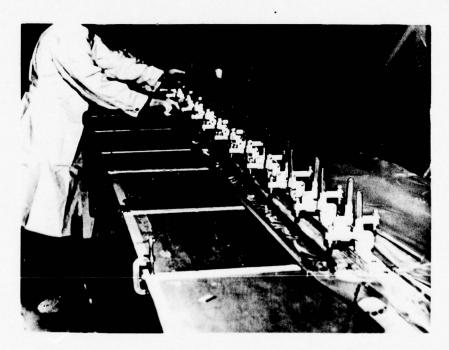


Figure 35. Bladder fabrication fixture.

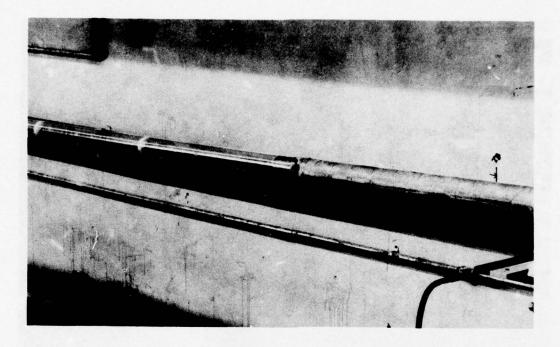


Figure 36. Inflated bladder for spar tube winding.

Orientation of Longo Filaments

Longo filament orientation was solved by the longo winding fixture shown in Figures 37 and 38. It has a hardback (one for each longo) pinned to the top of a rotating table which turns like a merry-go-round, at about 3 rpm. The fixture winds longos by pulling the rovings through the table-mounted resin impregnator seen in the background of Figure 37 and in the foreground of Figure 38, and wrapping them around pins at the ends of the hardbacks.

A fiberglass tray, seen at the far end of the hardback in Figure 37 and at the near end in Figure 38, is mounted on the hardback and the filaments are wound into it. The tray keeps the filaments straight at the crucial root end of the longo, aids in removing the longo from the hardback, and helps align the longo in the blade mold.

The longos are wound either directly on the stainless steel blade root bushing (spar longo and trailing edge longo) or on a sleeve portion of a fiberglass tray that slips over the bushing (broom and leading edge longo) and is bonded to it. In this manner, the filaments are never disturbed between the time they are wound and when they are placed in the mold. Special guides on the winding

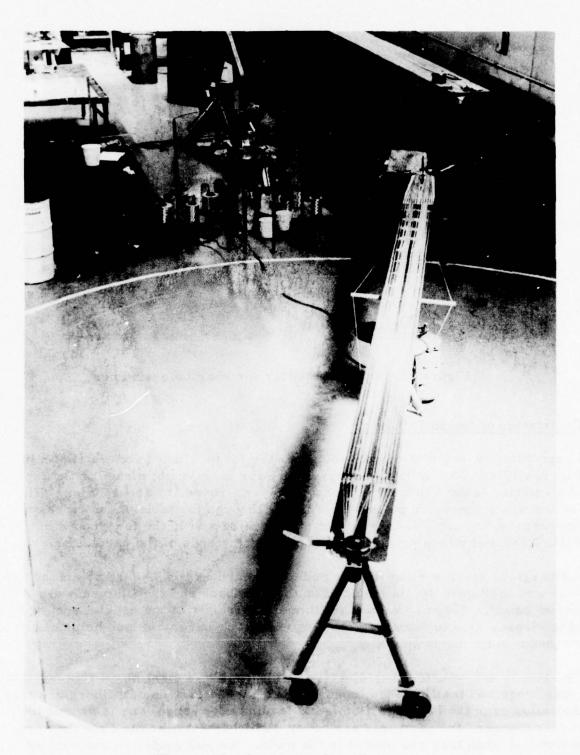


Figure 37. Longo winding fixture.

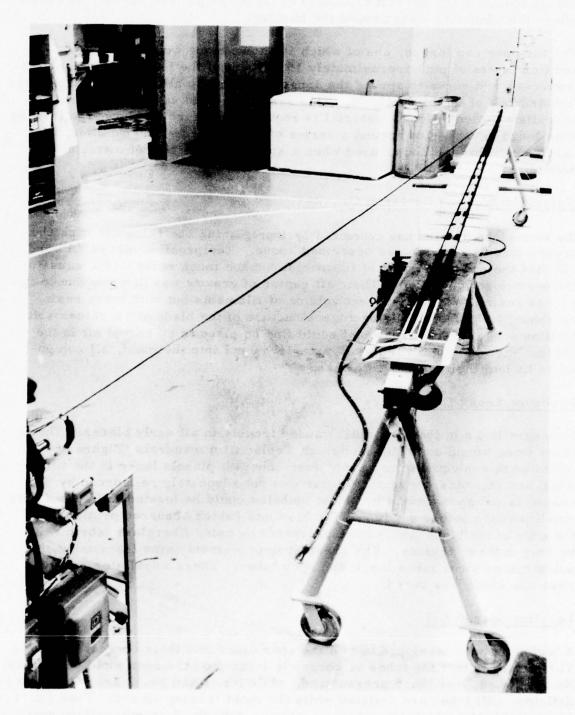


Figure 38. Trailing edge longo being wound.

fixture maintain the correct thickness of the longo pack in this critical area where the filaments wrap around the bushing.

For the spar cap longos, one of which is shown being wound in Figure 37, additional sets of pins approximately 15 percent of the length of the longo in from each end serve to spread the longo filaments to allow them to cover the forward half of the blade chord. This system is used where uniform spanwise distribution of longo material is required. Figure 38 shows the trailing edge longo being wound around a series of pins placed spanwise along the hardback. This method is used when a spanwise variation of material is needed.

Weight Control and Center of Gravity

The overweight problem was corrected by impregnating the filaments with the proper amount of resin, as described above. Toolproofing blades "A" and "B" had the proper amount of filaments, but too much resin -- the cause of the overweight condition. Their aft center of gravity was directly due to the excess resin. With the correct volume of filaments but with extra resin, combined with a solid leading edge structure of the blade and a rather soft trailing edge, the spar material could find no place to go except aft in the blade. When the right volume of material is put into the mold, all components fit into their proper locations.

Pressure Leaks During Cure

Pressure leaks in the spar tubes caused trouble in all early blades. These tubes were wound on 0.001-inch-thick Tedlar film mandrels (Figure 36) which were subjected to two problems: inherent pinhole leaks in the film itself and blowouts where the Tedlar was not adequately reinforced by filaments wrapped around it. Most pinholes could be located and sealed with small patches before winding. The blowouts (which occurred primarily at the ends of the blade mold) were prevented by using fiberglass fabric reinforcing in these regions. The greatest improvement came from using polyethylene inner tubes inside the spar tubes. These were later removed after the blade was cured.

Locating Spar Tubes

A technique was developed to tool the spar tubes into their correct locations. This requires that the tubes be correctly located on the open mold with tubes No. 3, No. 4, and No. 5 pressurized, while No. 1 and No. 2 are put in place deflated. All tubes are deflated while the mold is being closed. Then No. 4 is pressurized to lock the others in place. Tube No. 3 is pressurized next, followed by No. 1, No. 2, and No. 5 which are pressurized simultaneously.

Blade Surface Treatment

A blade surface treatment investigation was directed toward using Tedlar film as the outside surface of the blade skin. It was shown to be generally compatible with the blade fabrication process, but needed more development to perfect the process than could be accommodated in the present program. It is highly recommended that this process be developed for future blades because the Tedlar acts as a mold release, seals the blade against moisture, is an ultraviolet barrier to protect the resin, and comes in colors so that painting is not necessary.

Leading edge erosion protection material was selected from a radar reduction/leading edge erosion program, Reference 1.

Vacuum Diaphragm

The blade assembly technique requires that half of the blade material be placed in the top half of the mold, and half in the bottom. Then the top half-mold is turned over (with its blade material still in place) and positioned on the lower mold. To hold the WFW components on the upper mold while it is being turned upside down, a bondable vacuum diaphragm is used. This diaphragm must be impervious enough to maintain sufficient vacuum to prevent the WFW components from falling off the mold surface, and must be bondable to the WFW elements because it must remain in the blade. Several types of diaphragm material were investigated before Fiber Resin Corporation's FR-7035 film adhesive in a nylon matte carrier was chosen.

Radar-Absorbing Material

The technology related to incorporating radar-absorbing material, Reference 2, is discussed in Volume III.

- 1. Head, R. E., EROSION PROTECTION FOR THE AH-1G LOW RADAR CROSS-SECTION MAIN ROTOR BLADE, VOLUME I SAND AND RAIN EROSION EVALUATION, Hughes Helicopters, Division of Summa Corporation; USAAMRDL Technical Report 76-40A, Eustis Directorate, U.S. Army Air Mobility Research and Development Laboratory, Fort Eustis, Virginia, January 1977, AD A035961.
- 2. Head, R. E., EROSION PROTECTION FOR THE AH-1G LOW RADAR CROSS SECTION MAIN ROTOR BLADE, VOLUME II RADAR CROSS SECTION EVALUATION (U), Hughes Helicopters, Division of Summa Corporation; USAAMRDL Technical Report 76-40B, Eustis Directorate, U.S. Army Air Mobility Research and Development Laboratory, Fort Eustis, Virginia, January 1977 (S), AD C009381L.

SECTION II - DETAIL DESIGN

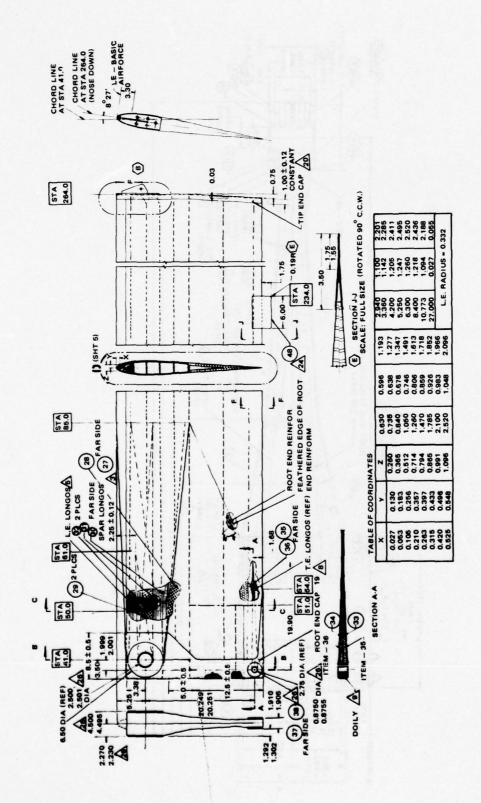
This section describes the detail design and analysis of the MTS blade. The candidate configurations designated during the preliminary design effort for integration were brought together in this phase into the final detail design of the blade. Throughout this process, close liaison was maintained between the tool designers and WFW manufacturing engineers to achieve optimum design/manufacturing integration. As a result, the MTS blade is a reliable structure that meets all the objectives set out for it at the beginning of the program.

DESCRIPTION OF THE MTS BLADE

The final MTS blade design details are shown in Figures 39 through 46. The blade has a 27-inch chord, a 226.5-inch span (BS 37.5 to BS 264.0), a linear twist of 0.45 degree per foot, and mounts interchangeably on the 540 hub of the AH-1G helicopter. The design of the blade can best be described by starting at its outside contour and working in. The description given here is in general terms. The MTS blade Process Specification in Volume II details the process of assembly.

The geometry of the blade is symmetrical, top and bottom. The internal structure is also symmetrical except for one feature which will be described below. The multi-tubular spar occupies the forward half of the chord, and the trailing edge structure occupies the rear half. The spar structure extends this far aft to disperse the structural elements and make them more tolerant of the 23mm HEI-T threat. The blade is covered by a three-ply Kevlar-49 skin, which is 0.018 inch thick and consists of a ±45-degree layer and a single 90-degree layer (see the angle nomenclature in Figure 2). The skin provides a portion of the blade torsion stiffness and a shear tie to the trailing edge longo.

The upper and lower spar longos are two packs of unidirectional Kevlar-49 filaments, each of which is continuous from the blade tip, runs inboard around the main bushing where the blade attaches to the hub, and back outboard to the tip. The spar longos are the primary members that provide flapwise stiffness; each spar longo in combination with its spar cap is independently capable of carrying all the centrifugal force in the blade. Outboard of BS 85, the spar longo is a band of filaments 11.75 inches wide and 0.044 inch deep. At the bushing this pack is 0.29 inch deep and 1.78 inches wide. At the inboard end where the bushing is located, the longo is wound into a preformed fiberglass tray that acts both as a guide for the filaments



Figur.: 39. MTS blade planform.

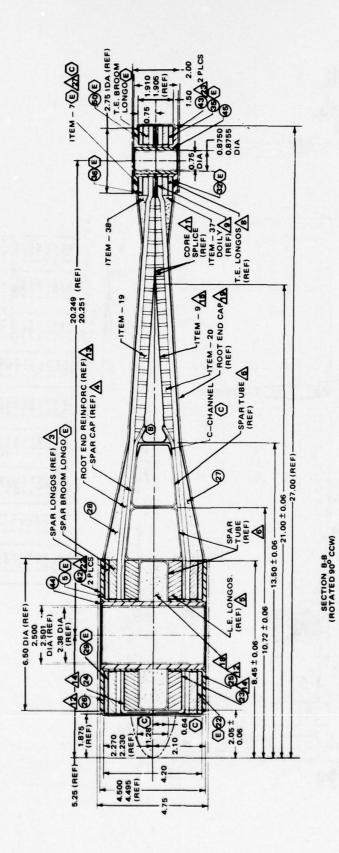
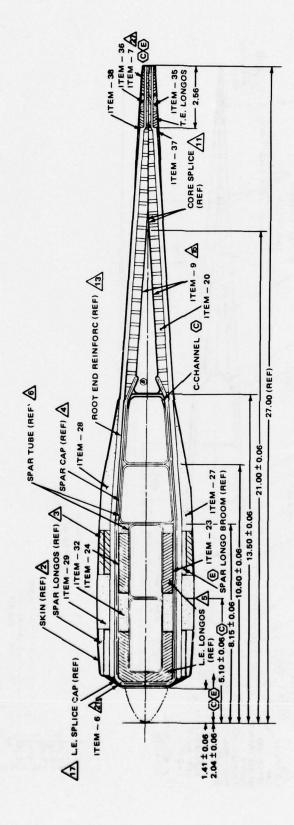


Figure 40. MTS blade section - BS 41.



SECTION C-C (ROTATED 90° CCW)

Figure 41. MTS blade section - BS 50.

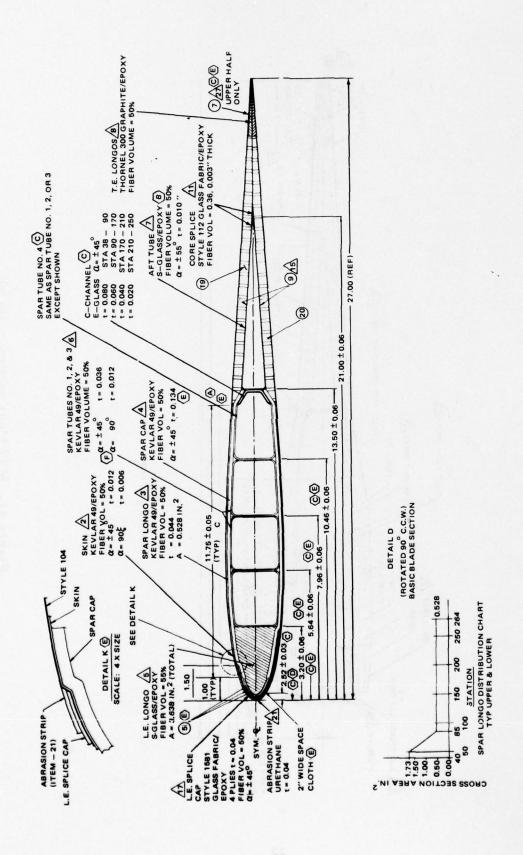


Figure 42. MTS blade section - BS 200.

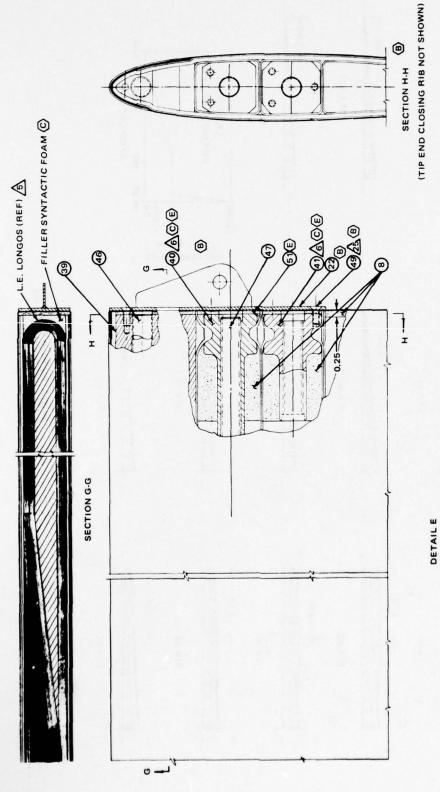


Figure 43. MTS blade tip section.

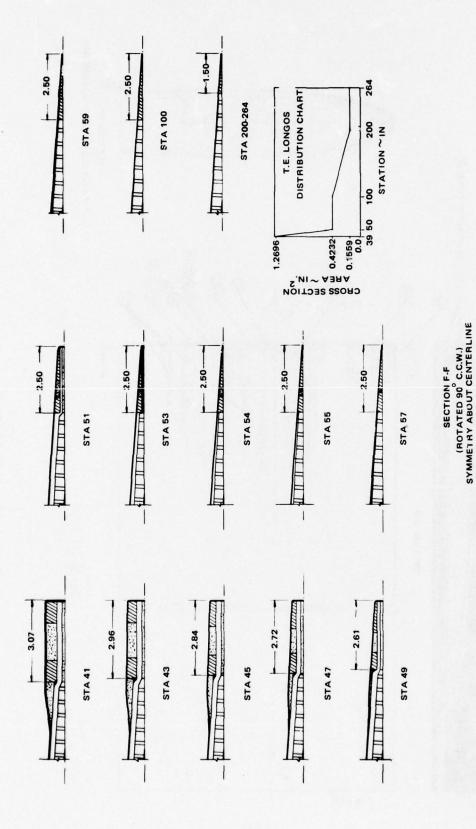


Figure 44. MTS blade trailing edge longo cross section.

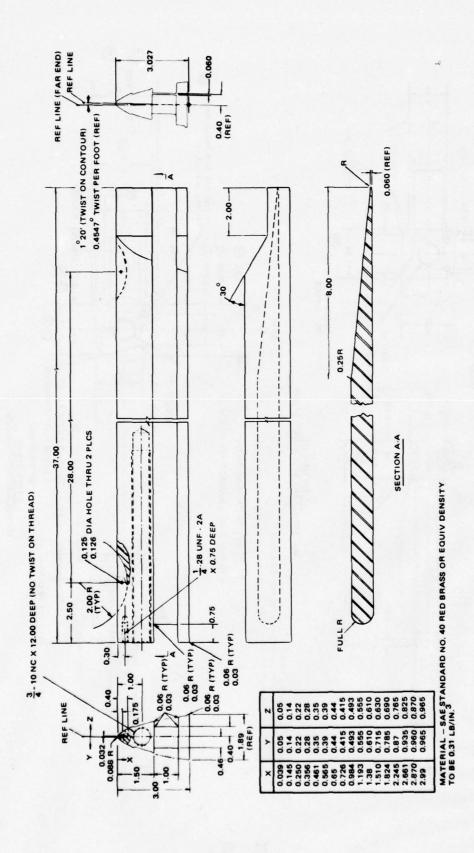


Figure 45. MTS blade leading edge tip weight.

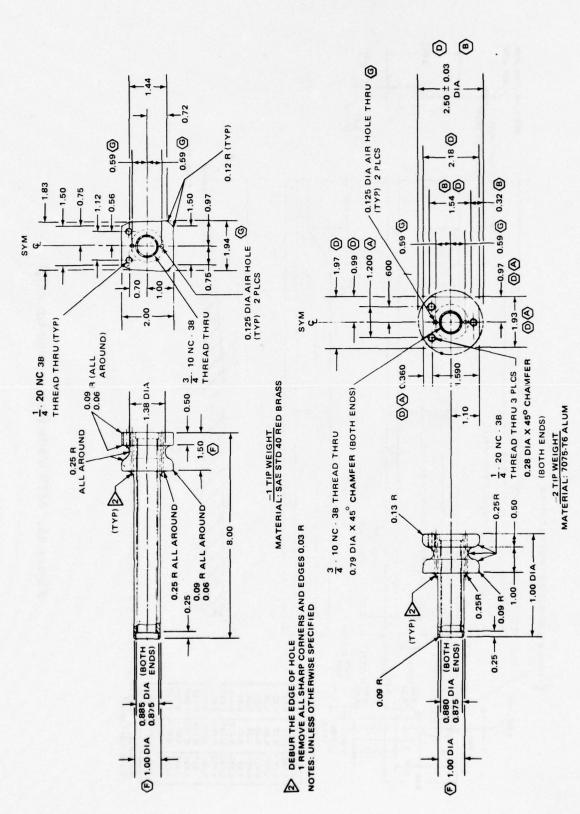


Figure 46. MTS blade spar tube tip weights.

and as a handling tool for moving the longo from the winding fixture to the blade mold. This tray, and all the other trays that will be described, is molded into the blade and becomes a permanent part of it.

The Kevlar-49 broom longo serves the same purpose that doublers serve in a metal blade: they increase stiffness and strength in the blade root area. These are unidirectional filaments that are step-tapered toward the root of the blade. One-fourth of the broom longos run from BS 85 inboard around the bushing and back out to BS 85. One-fourth of the longos are cut off at BS 74, one-fourth at BS 63, and the final fourth at BS 52. At the bushing the broom longo pack is 0.18 inch deep and 1.78 inches wide. The broom longo is wound into its own fiberglass tray.

The honeycomb panel that supports the aft skin is 3-pounds-per-cubic-foot, 1/8-inch cell Nomex, 3/8 inch thick. The leading and trailing edges are beveled. A single layer of Style 112 fiberglass fabric is bonded onto the side of the honeycomb away from the outside of the blade to stabilize the honeycomb and to protect the thin No. 5 spar tube from the sharp edges of the honeycomb.

The trailing edge (TE) longo is a unidirectional pack of Thornel-300 filaments that loop around the drag brace bushing at the inboard trailing edge of the blade. This longo, which provides chordwise bending stiffness, has a triangular cross section whose cross-sectional area decreases toward the tip of the blade as shown in Figure 44. A Thornel-300 TE broom longo adds reinforcement at the root. The cross-sectional area of this broom may be seen in Figure 44 inboard of BS 50. Both the full-length TE longo and TE broom longo have their own trays. A strip of 120-mesh aluminum screening woven from 4-mil wire is placed between the TE longo and the upper skin for lightning protection. It serves to conduct the lightning energy to the drag brace bushing from which it flows into the drag brace and hub.

The spar cap is a flattened tube wound at ±45 degrees from 11 layers of Kevlar-49, making it 0.132 inch thick. The spar tube is wound over a layer of film adhesive that remains inside the spar cap to assure a good bond when the tube is flattened. The spar cap extends from the nose of the airfoil where it butts against its partner in the other half of the blade, and runs aft to lap over the beveled leading edge of the honeycomb panel. The spar cap provides the major portion of the torsional stiffness. It has constant cross section from root to tip. A strip of RAM is wound into the spar cap at its leading edge.

The leading edge (LE) longo is a unidirectional pack of S-glass filaments that loop around the main retention bushing. This longo provides chordwise stiffness and has enough strength to carry all the centrifugal load by itself.

This longo, which is wound into a tray, has a constant cross section of 3.638 square inches inboard of BS 228. This longo is the only nonsymmetrical element in the blade: the lower LE longo stops at BS 228; 66 percent of the upper longo stops there, too. The remainder of the upper LE longo extends to the tip (BS 264) to form a loop around the grooved LE tip weight, tying the weight directly to the root bushing. A narrow strip of RAM is placed between the LE longo and the spar cap where they meet at the front of the blade.

The LE tip weight is a brass block that fills the forward portion of the blade (Figure 45). It has a spanwise groove through which the upper LE longos pass, and a threaded hole in the tip to accept the adjustable tungsten weights used to balance the blade.

The blade-root reinforcement is a layered pack of WFW S-glass broadgoods. It is 18 layers thick (0.180 inch) from the blade root to BS 51. Then it uniformly steps down three layers at a time until the tip of the final three layers is at BS 85. The filaments in all these layers are oriented at ±45 degrees to the blade span axis for torsional rigidity.

The doily, a hoop-wound ring of S-glass filaments 0.10 inch thick by 0.78 inch wide, is placed over the drag bushing to reinforce the fiberglass blade-root reinforcement for the chordwise loads that are induced in the blade by the drag link itself.

A film adhesive is used as a vacuum diaphragm to compact the skin, honey-comb, spar cap, and longos onto the mold. This film is bonded into the blade during the co-cure and becomes a permanent part of it.

The spar tubes are numbered one through five, counting aft from the nose of the blade. Numbers one through four are each wound from six layers of Kevlar-49 at ±45 degrees, with a final outer hoop winding.

The tube wall thickness is 0.048 inch. The No. 5 spar tube (the one under the honeycomb panels) consists of a single ±57-degree layer of S-glass (0.010 inch thick). All five tubes are wound on inflatable Tedlar mandrels that remain in the blade to serve as vapor barriers. The aft side of the No. 4 spar tube is reinforced with 2-inch-wide strips of filament-wound S-glass broadgoods, set on at ±45 degrees, which serve as the closing web for blade torsion loads. It is wound into the tube and consists of nine layers from the root to BS 85, six layers from BS 85 to BS 175, and three layers out to BS 220. The spar tubes contribute a small amount to the blade torsional stiffness, but more importantly serve as alternate load paths in case of ballistic damage. A primary function occurs during fabrication of the blade when these five tubes are inflated to pressurize the blade components during the co-cure cycle.

A brass tip weight is wound into the outboard end of the No. 1 spar tube, and an aluminum tip weight into No. 2. Figure 46 shows that these weights have a small diameter neck at the outboard end into which the filaments of the tube are wound for excellent mechanical entrapment. These weights are threaded to accept adjustable tungsten balance weights. Spar tubes No. 3, 4, and 5 do not have tip weights.

A number of cavities near the root end of the blade, such as the triangular regions between the longo filaments and the bushings and the space just aft of the spar broom longo and just forward of the TE broom longo, are filled with syntactic foam (glass microballoons and epoxy). The spar and the TE longo cavities are filled with milled E-glass fibers and epoxy for the added strength needed in the ground flapping mode. All these elements are cocured to form the basic blade.

When it is removed from the mold, the blade has approximately 2 feet of extra material on each end. This surplus is cut off, and the flashing is trimmed from the leading and trailing edges.

Note that in Figure 42 an indentation reaches 1.5 inches back from the leading edge on the top surface and 3.0 inches on the bottom. In this indentation there is first placed a strip of RAM and then three layers of ±45-degree filament-wound S-glass broadgoods. This material is cured in place in a secondary bonding operation using APCO 2434/2340 room-temperature curing resin. This still leaves an indentation around the nose of the airfoil that is later filled flush with a strip of polyurethane antierosion material, Reference 1.

One-quarter-inch styrofoam dams are inserted in the No. 3, 4, and 5 spar tubes, one-fourth inch in from the trimmed ends of the blade (root and tip); this one-quarter-inch space is filled with syntactic foam. The cavities around ends of the leading edge and No. 1 and 2 tip weights are filled flush with the tip with syntactic foam. Styrofoam dams are placed in the root ends of spar tubes No. 1 and 2, approximately 7 inches in from the root end. These spaces between the dams and root end are filled with milled E-glass/epoxy. The hardener used in this epoxy and in the syntactic foam cures at room temperature. After this material sets, a three-layer tip cap and a seven-layer root cap are hand molded in place, again with a room-temperature setting resin.

The blade is then stood up on its tip end, and syntactic foam is injected into the tip ends of spar tubes No. 1 and 2 to the depth of the tip weights to make them rigid with respect to the spar tube walls (Figure 43).

ANALYSES

Weight and Balance Analysis

The weight and balance analysis for the MTS blade was calculated from the density and volume of the components. The weight of each WFW component was determined before it was wound, and the weight of each detail part was controlled to within ±3 percent during the winding operation (see the weight inspection and verification process in Volume II).

The details of the weight and balance analysis are given in Appendix A. The important parameters are summarized in Table 6. The weight and chordwise center of gravity distributions along the span of the blade are plotted in Figures 47 and 48, respectively. Comparisons are given with the 540 metal blade characteristics.

Stress Analysis

The stress analysis of the MTS blade follows conventional practice with allowable loads being derived from the strength properties of the filaments and their combination with the resin matrix that supports them. These allowables are modified where necessary in light of the test data accumulated in the materials test program.

A search was made through a 540 blade flight loads report, Reference 3, to determine the maximum loads encountered. Because the MTS blade is designed to have similar weight, stiffness, and dynamic properties, it was assumed that these maximum loads would also apply to the MTS blade. Consequently, the MTS blade is designed to withstand all of these loads without ever going over the allowables - the definition of an infinite life design.

^{3.} Adaska, W. W., QUALIFICATION LOAD LEVEL SURVEY FOR IM-PROVED MAIN ROTOR BLADES ON THE MODEL AH-1G HELICOP-TER, Report 209-099-305, Bell Helicopter Company, Fort Worth, Texas, 5 June 1970.

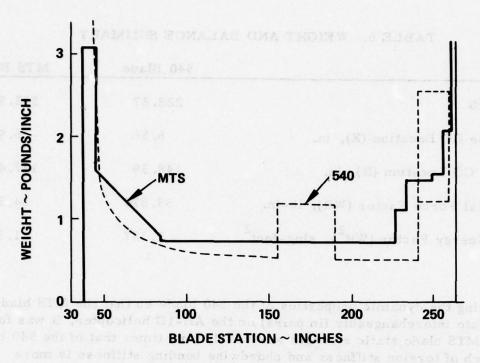


Figure 47. Spanwise weight distribution.

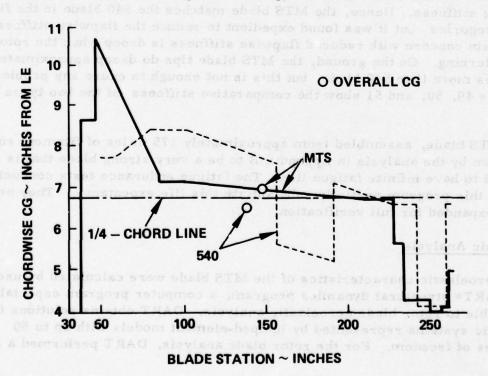


Figure 48. Spanwise center of gravity distribution.

TABLE 6. WEIGHT AND BALANCE SUMMARY

	540 Blade	MTS Blade
Weight, 1b	228.27	232.95
Chordwise CG Location (X), in.	6.56	6.94
Spanwise CG Location (R), in.	148.39	147.43
Centrifugal Force Factor (WR), 1b-in.	33,874	34,344
Kinetic Energy Factor (WR ²), slug-feet ²	1,387	1,395

In matching the dynamic properties of the 540 blade so that the MTS blade can operate interchangeably (in pairs) on the AH-1G helicopter, it was found that the MTS blade static strength was nearly four times that of the 540 blade. The match of torsion stiffness and chordwise bending stiffness is more important from a rotor dynamics point of view than the match of flapwise bending stiffness. Hence, the MTS blade matches the 540 blade in the first two categories, but it was found expedient to reduce the flapwise stiffness. The main concern with reduced flapwise stiffness is droop when the rotor is not turning. On the ground, the MTS blade tips do droop approximately 3 inches more than 540 blade, but this is not enough to cause any problem. Figures 49, 50, and 51 show the comparative stiffness of the two types of blade.

The MTS blade, assembled from approximately 175 miles of filament rovings, is shown by the analysis in Appendix B to be a very strong blade that is calculated to have infinite fatigue life. The fatigue endurance tests conducted during this program partially substantiate this life expentancy. They need to be expanded for full verification.

Dynamic Analysis

The aeroelastic characteristics of the MTS blade were calculated by use of the DART* structural dynamics program, a computer program especially adaptable to rotor blade aeroelastic analysis. DART obtains solutions for dynamic systems represented by lumped-element models with up to 80 degrees of freedom. For the rotor blade analysis, DART performed a fully

^{*}DART - Dynamic Analysis Research Tool

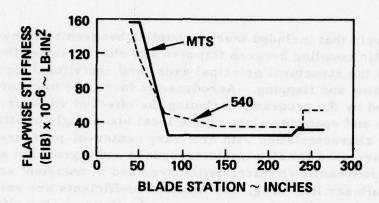


Figure 49. Flapwise bending stiffness comparison, MTS and 540 blades.

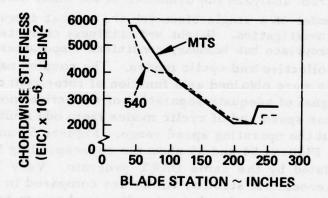


Figure 50. Chordwise bending stiffness comparison, MTS and 540 blades.

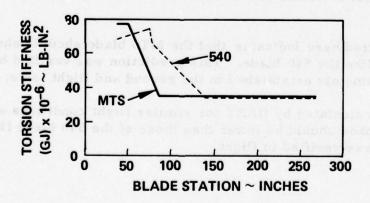


Figure 51. Torsion stiffness comparison, MTS and 540 blades.

coupled analysis that included inertia coupling between pitching and flapping motion, elastic coupling between flapwise and chordwise bending due to inclination of the structural principal axes, and centrifugal force coupling between pitching and flapping. Aerodynamic force and moment distributions are calculated by the program, including the effect of vibratory structural deformations and spanwise slope on the local blade angle of attack. Linear aerodynamic characteristics with arbitrary center-of-pressure and lift-curve slope are used for steady-stateresponse and eigenvalue solutions. Nonlinear aerodynamic characteristics are used in transient solutions in which the nonlinear lift, drag, and moment coefficients are entered as arbitrary functions of Mach number and angle of attack; the effects on lift and moment (including phase lag and hysteresis) due to dynamic stall and the effects of yawed flow on the maximum lift coefficient are accounted for.

The DART program analyzed the dynamics of the blade using an 11-station lumped-element model of a single blade for the natural frequency and linearized stability investigation. Weight and stiffness characteristics are listed in Table 7. Appropriate hub boundary conditions (impedances) were used to obtain both collective and cyclic modes. The coupled natural frequencies and mode shapes were obtained as a function of rotor rpm and collective pitch, with the goal of adequate separation of collective modes from even multiples of rotor speed and of cyclic modes from odd multiples of rotor speed throughout the operating speed range. Figures 52 and 53 are the MTS blade fan plots; Figures 54 and 55 show the corresponding 540 blade frequencies calculated by the same DART program. Very little difference can be seen. Aeroelastic stability limits are compared in Figure 56. The MTS blade first collective chordwise bending is shown to be very close to the stability boundary for the condition of no internal structural damping at or above the design rpm. A calculation assuming 5 percent structural damping showed that even this low level of internal damping makes the blade stable.

The data plotted here indicates that the MTS blade should behave in flight very nearly like the 540 blade. This prediction was verified by dynamics tests and ultimately established in the ground and flight tests.

Blade loads calculated by DART for similar flight conditions show that the MTS blade loads should be lower than those of the 540 blade (Figure 57). This thesis was verified in flight.

TABLE 7. MTS BLADE MASS AND STIFFNESS CHARACTERISTICS

BS (in.)	Flapwise EIF (106 lb-in ²)	Chordwise EIC (10 ⁶ lb-in ²)	Torsion GJ (10 ⁶ lb-in ²)	Neutral Axi NA (in. *)	cG (in. *)	Weight W (lb/in.)
41	156.0	5740	77.0	8.72	8.63	3.086
46	156.0	5740	77.0	8.72	8.63 and 10.67	3.086 and 1.594
52	156.0	5740	77.0	8.72	10.15	1.470
63	112.2	5123	63.0	8.65	9. 18	1.243
74	68. 5	4507	49.0	8.58	8.25	1.015
85	24.8	3890	35.0	8.51	7.29 and 7.13	0.788 and 0.730
96	1	3890		8.51	7.13	0.730
100		3890		8.51	7.11	0.730
107		3763	-0.01	8.39	7.08	0.729
118		3562		8.19	7.04	0.727
129		3362	2.0	8.00	6.99	0.725
140		3162		7.81	6. 95	0.723
151		2962	1020,04 - 4122	7.61	6.90	0.722
162		2762		7.42	6.87	0.720
173		2561	Usellos -	7.23	6.83	0.718
184		2361		7.03	6.80	0.716
195	15	2161		6.84	6.77	0.714
200		2070	0 850	6.75	6.75	0.713
206		2070	//	6.75	6.70	0.712
217		2070		6.75	6.70	0.710
228		2070	103/1	6.75	6.70 and 5.64	0.709 and 1.104
234		2760	JOHN /	4.21	5.64 and 4.30	1.104 and 1.465
239	849	2760	11/1	4.21	4.30	1.465
250		2760		4.21	4.30 and 4.05	1.465 and 1.537
257	18	2760	1	4.21	4.05 and 4.12	1.537 and 2.060
262	24.8	2760	35.0	4.21	4.12 and 5.00	2.060 and 3.125

^{*}Measured from leading edge

Mass Moment of Inertia (Including Hub)

Flapwise | about rotor center = 6,586 x 10⁶ lb-in²

Pitchwise, about quarter chord = 12,096 lb-in²

Twist

Root-to-Tip = -10° (-0.003788 degrees/inch)

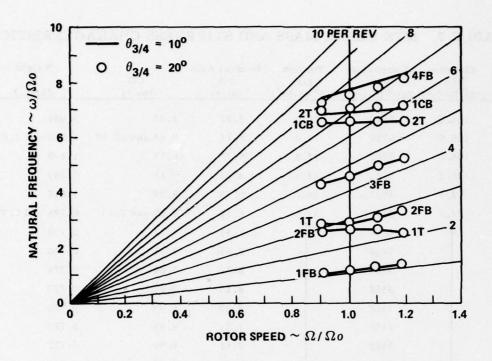


Figure 52. MTS blade - collective roots.

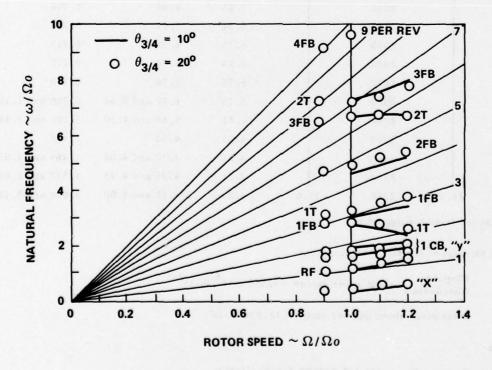


Figure 53. MTS blade - cyclic roots.

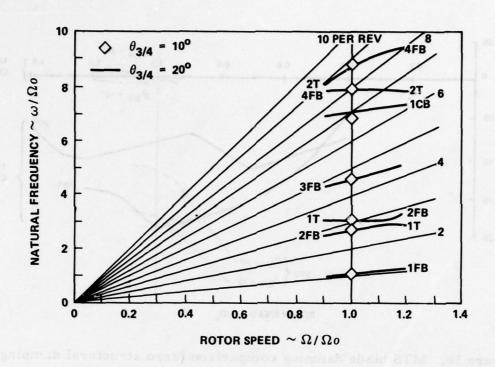


Figure 54. 540 blade - collective roots.

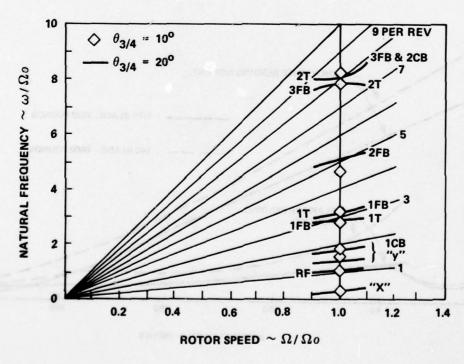


Figure 55. 540 blade - cyclic roots.

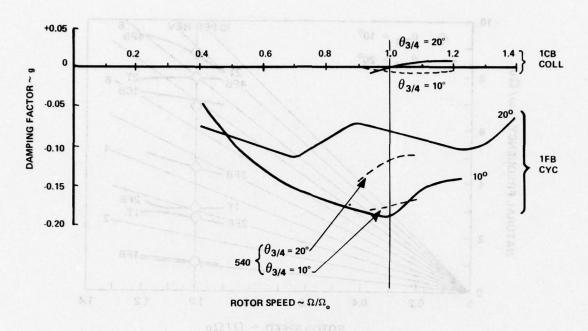


Figure 56. MTS blade damping comparison (zero structural damping).

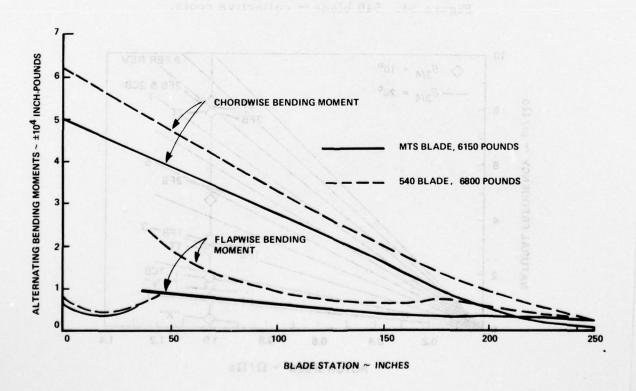


Figure 57. Calculated blade loads in level flight at 140 knots.

SECTION III - LABORATORY TESTS

The laboratory tests carried out on the full-scale MTS blade are described in this section. This test work demonstrated that the blade strength, stiffness, and dynamic properties were suitable for flight. The blades were built as complete, full-length blades. All blades except the flight test blades were cut into segments with the various segments being assigned to specific tests as indicated in Figure 58.

All eight MTS test blades were used in these structural tests. The stiffness of each blade was measured. S/N-001 and -002 were used for static test, fatigue test, radar test, ballistic test, and dynamic test (S/N-001 had metal weights clamped to its tip to give it the proper mass distribution). S/N-003 and -004 were used primarily for fatigue tests (although a portion of S/N-003 was used for a radar test in an allied program, Reference 2). The S/N-005 blade was subjected to 23mm HEI-T ballistic damage and then fatigue tested to demonstrate its fly-home ability. (An outboard segment of S/N-005 was also used in the referenced radar test.) The two flight test blades, S/N-006 and -007, were subjected to dynamic tests to establish their natural frequencies and mode shapes.

All structural load tests were conducted in HH's Structures Test Laboratory to establish that the static and fatigue strength, stiffness, and dynamic characteristics of the MTS blade were in agreement with the predicted values, and that the concept was ready for its ground and flight tests. For comparison, certain of the tests were duplicated for a pair of production metal (540) blades (NSN 1615-00-178-9680).

STIFFNESS TESTS

The first test for each MTS blade as it came off the production line was the measurement of its stiffness: flapwise, torsional, and chordwise. Each blade was supported in a cantilever mount by its two root attachment points, and its tip was stabilized at the quarter-chord point to eliminate unwanted cross deflections. Figure 59 shows the MTS blade undergoing these tests.

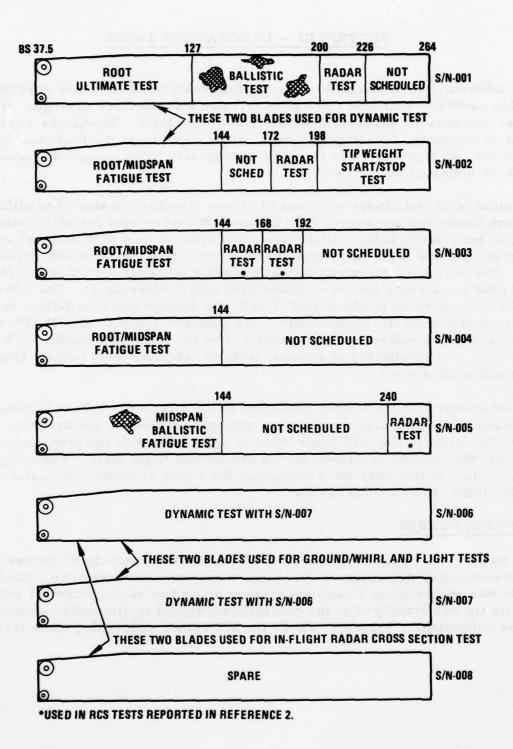
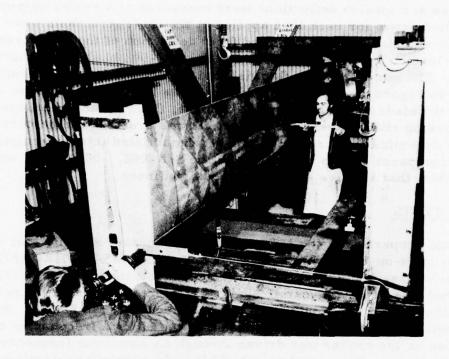
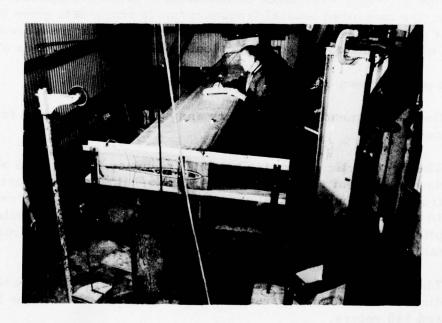


Figure 58. MTS blade structure test assignments.



Flapwise Measurement



Torsion Measurement

Figure 59. Blade stiffness tests.

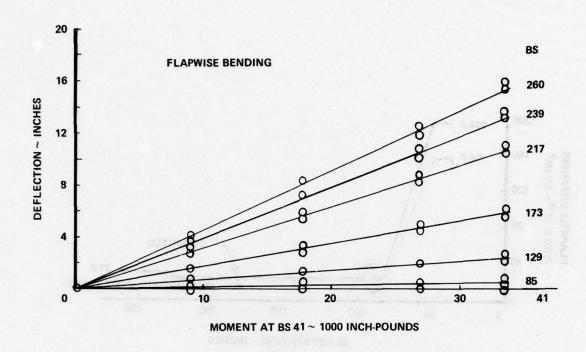
The flapwise and torsion deflections were measured at a series of points along the blade span for each load applied at the tip (corrections were made for the root-end motions that resulted from deflection of the cantilever support under load). Typical deflections for the S/N-002 blade are shown in Figure 60. The corresponding flapwise and torsion stiffness distributions are shown in Figure 61. The axial stiffness was too high to measure reliably along the blade span, but since the weight, flapwise and chordwise bending, and torsion stiffnesses were correct, it was presumed to be correct also. The dynamics tests reported below substantiated this presumption. Figure 62 compares the tip deflections of the S/N-002, -006, -007, and -008 blades to show that all have essentially equal stiffness.

DYNAMIC TESTS

The dynamic properties of the MTS blades were measured while they were mounted in pairs on an AH-1G main rotor hub (NSN 1615-00-918-9357). The blade-plus-hub assembly was suspended from a soft mount (Figure 63) and was vibrated by an electrodynamic shaker at selected points on the hub to induce collective and cyclic natural frequency modes in the blades. Suitably placed accelerometers (Figure 64) measured the natural frequencies and mode shapes as the shaker was driven through an automatic frequency sweep from 3 to 60 hertz. The complete set of blade frequency/acceleration sweep curves for the S/N-006, -007 blade combination is given in Appendix C. From these, the measured natural frequency/mode shape data given in Table 8 was deduced. This table also includes similar data measured for a pair of 540 blades, and corresponding calculated data for both kinds of blades.

The salient points shown by this comparison are:

- a. Good agreement between theory and experiment is shown for all modes.
- b. The first cyclic chordwise bending frequency for the MTS blade is down 6 percent relative to the 540 blade. However, the estimated frequency at normal rpm appears to be acceptable (1.54/rev at 10 degrees collective pitch and 1.35/rev at 20 degrees collective pitch). This is the most important single parameter for maintaining acceptable loads in a teetering rotor.
- c. The first cyclic coupled flapwise bending/torsion modes are predicted to be close to 3/rev at 100 percent rpm for both the MTS and 540 rotors.



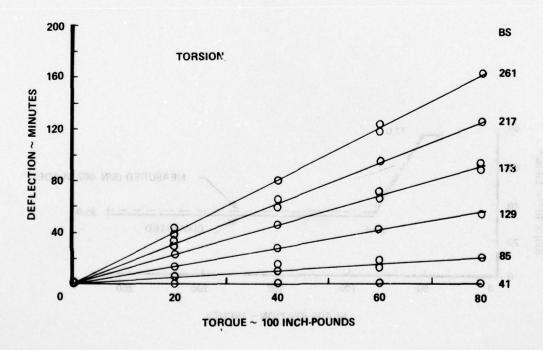
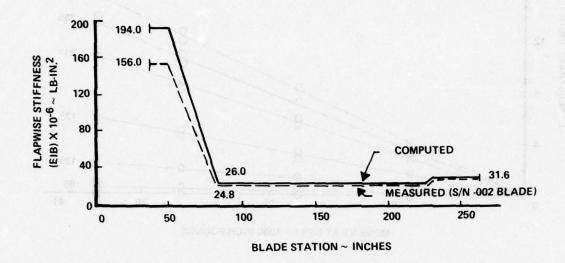


Figure 60. Flapwise and torsion stiffness - S/N-002 blade.



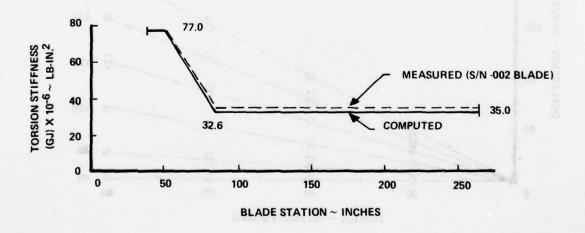


Figure 61. MTS blade spanwise stiffness distribution.

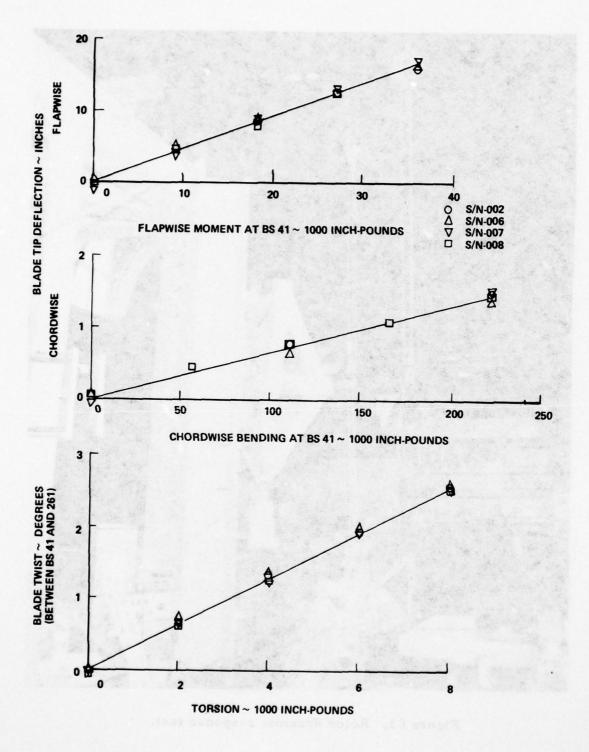


Figure 62. MTS blade stiffness comparison.

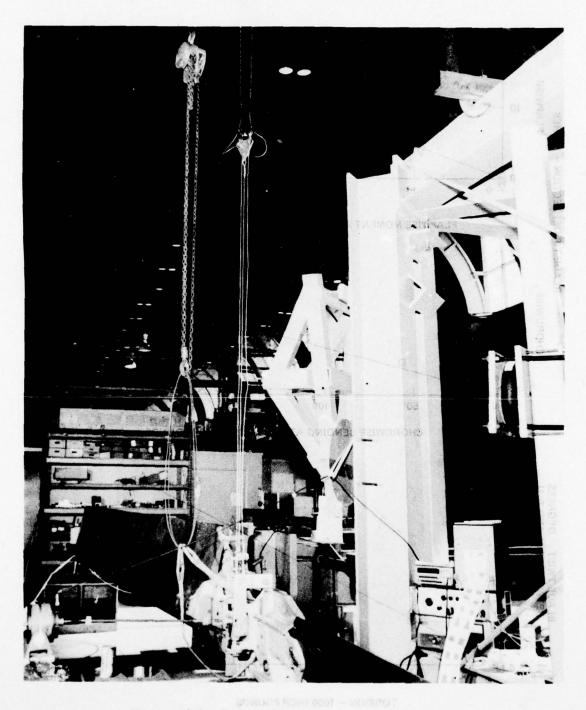


Figure 63. Rotor dynamic response test.

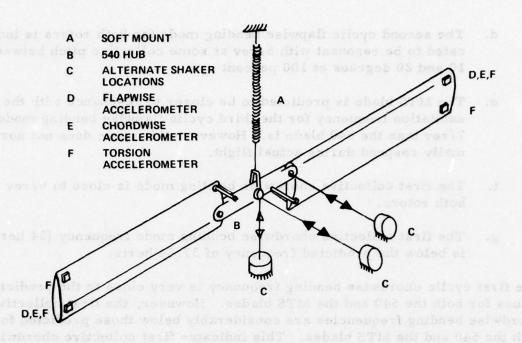


Figure 64. Dynamic test schematic.

TABLE 8. FREQUENCY COMPARISON - 540 ROTOR VERSUS MTS ROTOR

Mode*		540 Blades		S/N-006 and -007 MTS Blades	
Type	Boundary Condition	Experimental	Predicted	Experimental	Predicted
1FB	COLL	arl av 1.2 llos n	olen 1.3000e	ence with the sa	1.18
2FB	COLL	6.95	6.5	6.4	5.88
3FB	COLL	17.7	16.64	15.3	15.27
1 T	COLL	22.3	21.8	ATE STRENGT	22.45
1CB	COLL	33.0	39.90	34.0	37.56
4FB	COLL	38.2	33.47	bed 29.3 das	30.56
1FB	CYC	4.05	3.76	3.6	3.23
1CB	CYC	9.3	9.37	8.6	8.87
2FB	CYC	15.3	14.7	14.1	15.32
3FB	CYC	29.9	32.15	26.2	26.32
1T	CYC	31.0	33.2	000-030.0 st ad	31.78

^{*}FB: flapwise bending, CB: chordwise bending, T: torsion, COLL: collective mode, CYC: cyclic mode

- d. The second cyclic flapwise bending mode for both rotors is indicated to be resonant with 5/rev at some collective pitch between 10 and 20 degrees at 100 percent rpm.
- e. The MTS blade is predicted to be closer to resonance with the excitation frequency for the third cyclic flapwise bending mode at 7/rev than the 540 blade is. However, this mode does not normally respond during actual flight.
- f. The first collective chordwise bending mode is close to 6/rev for both rotors.
- g. The first collective chordwise bending mode frequency (34 hertz) is below the predicted frequency of 37.54 hertz.

The first cyclic chordwise bending frequency is very close to the predicted values for both the 540 and the MTS blades. However, the first collective chordwise bending frequencies are considerably below those predicted for both the 540 and the MTS blades. This indicates first collective chordwise bending operating frequencies at 100 percent rotor speed (324 rpm) close to 6/rev for the 540 blades (6.0/rev) and the MTS blades (6.2/rev). It is not considered desirable to have collective frequencies for a two-bladed rotor near an even integer multiple of the rotor speed, but apparently it is acceptable with the 540 blades. The MTS blades, being further from 6/rev, should be less critical.

Another effect of the first collective chordwise bending frequency observed for the inflight analysis of the MTS blade is the reduced damping at and above coalescence with the second torsion collective frequency. Reduction of the first collective chordwise bending frequency as in the MTS blade is beneficial in avoiding this coalescence.

ROOT ULTIMATE STRENGTH TEST

A test doubler was bonded onto the root-end segment of the S/N-001 blade, and this segment was tested in a 400,000-pound Baldwin Universal Test Machine (Figure 65) to measure its ultimate spanwise strength. The load at failure was 222,500 pounds, but the failure consisted of the test doubler delaminating from the blade, rather than a failure in the blade itself. An inspection of the blade structure showed no damage at this load level. The test load of 222,500 pounds is 23 percent above the design ultimate strength of 181,500 pounds at the root section blade station (BS 41), and 39 percent greater than the 150,000-pound ultimate load at the outboard end of the root doublers (BS 85).

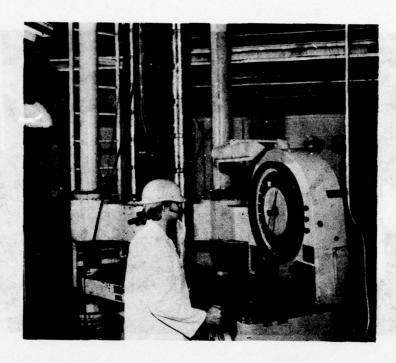


Figure 65. Root-end ultimate strength test (S/N-001 blade).

This test demonstrated that the MTS blade has more than adequate static strength. It also demonstrated the need for a better process for bonding the test doubler. Examination of the delamination, and subsequent tests, showed that bonding to cured Kevlar-49 is not satisfactory unless a fiberglass scrim cloth is placed over the Kevlar-49 before the Kevlar-49 doublers are bonded on. This process was used satisfactorily for the tip ground-air-ground cycle specimen and for the three root-end/midspan fatigue specimens, testing of which is described below.

GROUND-AIR-GROUND CYCLE TEST

The tip-end segment of the S/N-002 blade had a test doubler bonded to its inboard end. It was set up in the dynamic loading fixture shown in Figure 66 for the 1200-cycle ground-air-ground (GAG) test. (A 1200-cycle test was chosen to represent a factor of safety of 4 over the 300 actual start/stops that could be anticipated in the ground and flight test programs.)

ROOT/MIDSPAN FATIGUE TEST

A special fatigue test machine was developed for these tests. It is shown in its original configuration at the top of Figure 67, and as modified later at

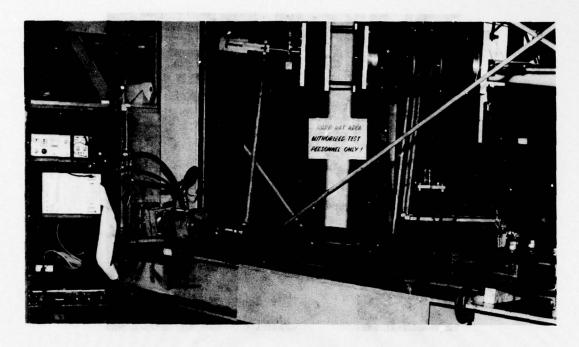


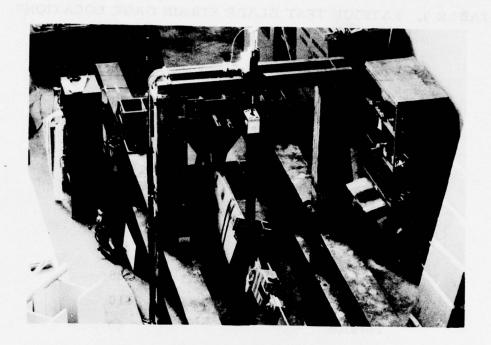
Figure 66. Ground-air-ground cycle test (S/N-002 blade).

the bottom of this figure. It was designed to permit testing the root end and the midspan region simultaneously, a new way of fatigue testing that avoids testing each section individually in two separate setups as in the usual case. The half-span blade was mounted as a cantilever beam at its root end and had doublers bonded on at its tip for introducing the simulated centrifugal force and the oscillating flap/chord/torsion fatigue force.

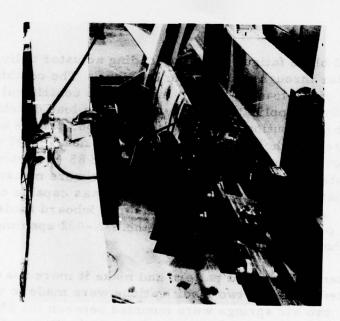
Strain gages on the blade, Table 9, measured blade loads. A hydraulic actuator applied the alternating load at a frequency near the flapwise bending natural frequency. This allowed chordwise bending moments to be introduced in proportion to the actuator force, and flapwise bending moments as a function of frequency. An offset weight aft of the trailing edge induced torsion from the flapwise input.

A desired alternating load level was established for the fatigue tests on the basis of 540 blade measured loads. These loads were imposed at a "weighted fatigue" level which equalled 1.3 times the maximum level flight loads, Reference 3, measured for the 540 blade. Two million cycles at this load level was established as the duration needed to give a 1.67 factor of safety for the 1,200,000 cycles to be expected at 2/rev during the 10-hour ground test and 20-hour flight test.

HUGHES HELICOPTERS CULVER CITY CALIF F/G 1/3
FLIGHT TEST OF A COMPOSITE MULTI-TUBULAR SPAR MAIN ROTOR BLADE --ETC(U) AD-A046 176 AUG 77 R E HEAD HH-76-281-VOL-1 DAAJ02-74-C-0055 USAAMRDL-TR-77-19A NL UNCLASSIFIED 2 OF 4 ADA046176



Initial Configuration - S/N-002 Blade Test



Final Configuration - S/N-003, -004, and -005 Blade Test
Figure 67. MTS blade fatigue test fixture.

TABLE 9. FATIGUE TEST BLADE STRAIN GAGE LOCATIONS

Mode	Blade Station (inches)
Flapwise Bending	48
	60
	85
	110
Chordwise Bending	Drag brace
	48
	60
	85
	110
Torsion	90

For the S/N-002 blade fatigue test, the loading actuator delivered its force to the blade collar through elastomeric bearings. The combination of blade stiffness, mass of the loading collar, mass of the centrifugal force mechanism, and the point of application of the alternating load developed a blade bending moment distribution as shown in Figure 68. There was a bending moment (flapwise and chordwise) inflection point near BS 97 which made it impossible to develop the desired moments at BS 85 (the inboard end of the blade midspan structure). The fatigue loads that were measured in this blade demonstrated that, inboard of BS 75, the blade was capable of carrying the required loads. A comparison of the measured inboard loads and blade spanwise structural properties indicated that the S/N-002 specimen had adequate strength throughout its length.

To modify the bending moment pattern and make it more nearly like the distribution expected in flight, two modifications were made to the fatigue test fixture. First, two air springs were mounted between the blade collar and the frame of the fixture. See the lower photograph, Figure 67. This changed the bending moment from that experienced by the S/N-002 blade (Figure 68) to the solid curves shown for S/N-003 in Figure 69. The S/N-003 blade was

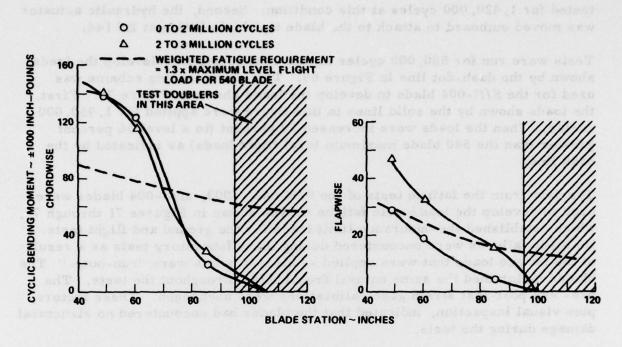


Figure 68. Fatigue test loading conditions - S/N-002 blade.

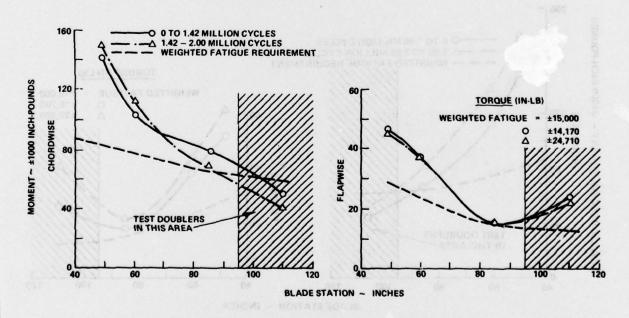


Figure 69. Fatigue test loading conditions - S/N-003 blade.

tested for 1,420,000 cycles at this condition. Second, the hydraulic actuator was moved outboard to attach to the blade tip clevis fitting at BS 144.

Tests were run for 580,000 cycles in this configuration to develop the loads shown by the dash-dot line in Figure 69. This same loading scheme was used for the S/N-004 blade to develop the loads shown in Figure 70. First, the loads shown by the solid lines in this figure were applied for 1,950,000 cycles. Then the loads were increased 20 percent (to a level 56 percent greater than the 540 blade maximum level flight loads) as indicated by the dash line.

The data i m the fatigue tests of the S/N-002, -003, and -004 blades were used to develop the load/cycle fatigue curves shown in Figures 71 through 78, which established the endurance limit loads for the ground and flight tests. No blade failures were encountered during these laboratory tests as a result of the fatigue loads that were applied -- all test points were "run-outs." The blades maintained the same natural frequencies throughout the tests. The pre- and post-test strain gage calibrations were unchanged. These factors, plus visual inspection, indicated that the blades had encountered no structural damage during the tests.

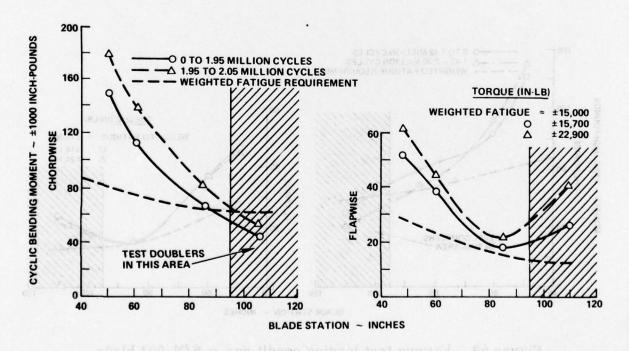


Figure 70. Fatigue test loading conditions - S/N-004 blade.

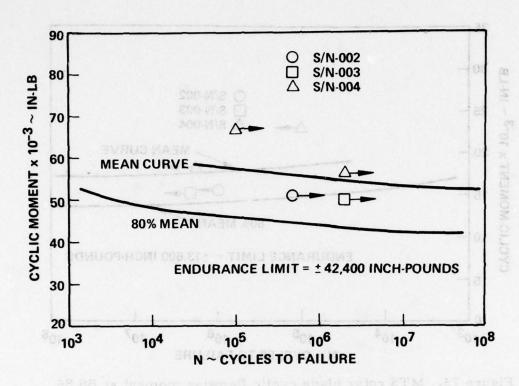


Figure 71. MTS rotor blade cyclic flapwise moment at BS 48.

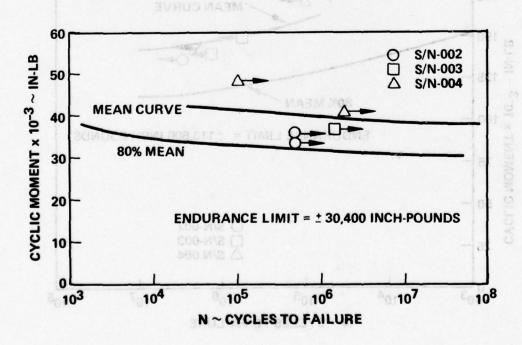


Figure 72. MTS rotor blade cyclic flapwise moment at BS 60.

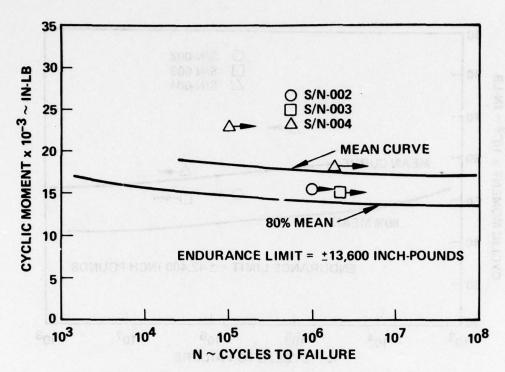


Figure 73. MTS rotor blade cyclic flapwise moment at BS 85.

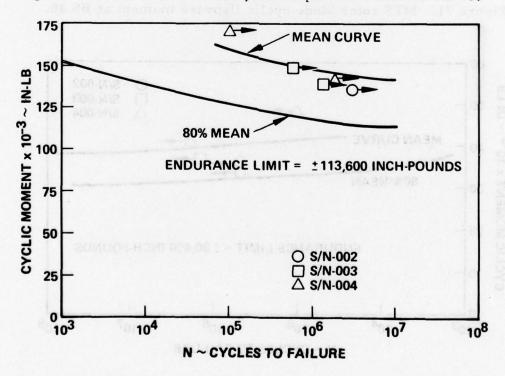


Figure 74. MTS rotor blade cyclic chordwise moment at BS 43.

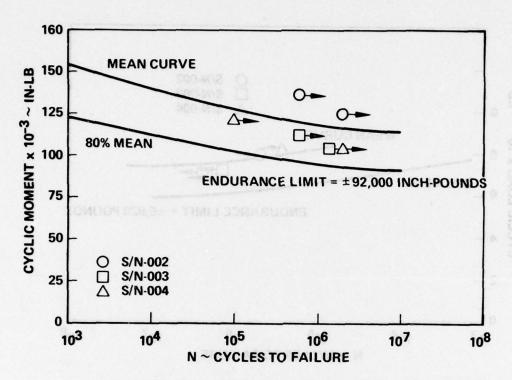


Figure 75. MTS rotor blade cyclic chordwise moment at BS 60.

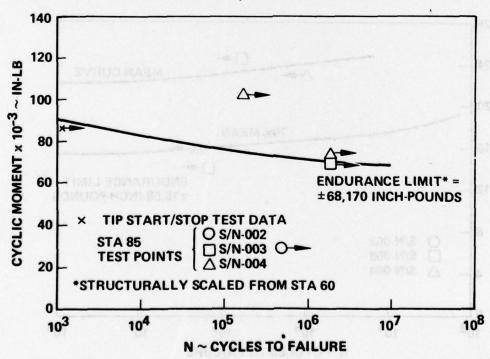


Figure 76. MTS rotor blade cyclic chordwise moment at BS 85.

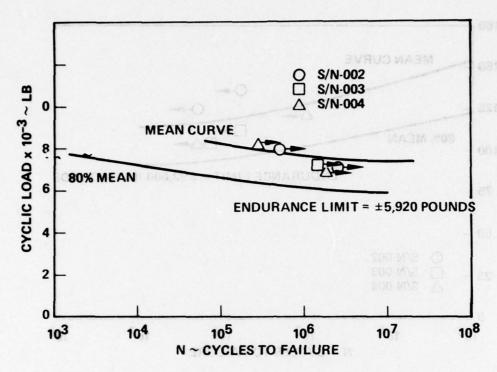


Figure 77. MTS rotor blade cyclic drag brace load.

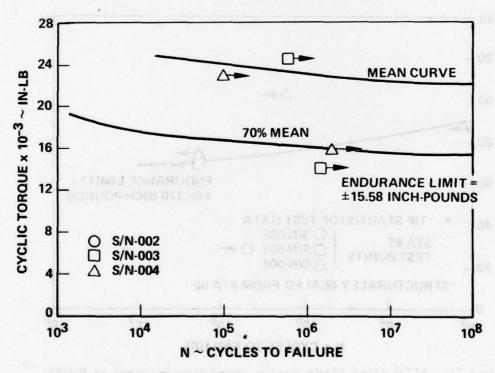


Figure 78. MTS rotor blade root-end cyclic torque.

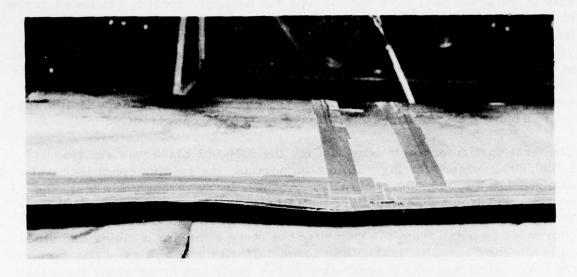
Because of the limited data (three specimens) the "run-out" test points were not considered to have established endurance limits. The Federal Aviation Administration (FAA) factor of 20 percent reduction in allowable loads when only three specimens have been tested was applied. Hence, the lower curves in Figures 71 through 78 are representative of the endurance limits for the limited flight tests of the current program only. Before expanded flight envelope tests or service evaluation tests, additional fatigue tests must be run at loads high enough to fail the blade and determine its true endurance limit. The MTS blade is calculated to have infinite fatigue life. Additional tests are expected to prove this to be the case, and that the endurance limits recommended for the current program are extremely conservative.

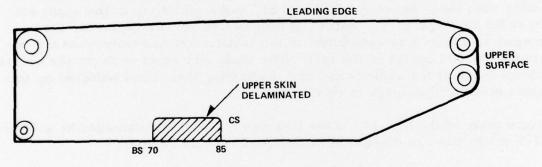
The first portion of the fatigue test for the S/N-002 blade was run for 2,000,000 cycles. During a follow-on portion, the loading conditions were changed for a 1,000,000-cycle test. About halfway through this test, the centrifugal force subassembly of the fatigue fixture broke, released the 90,000-pound centrifugal force instantaneously and subjected the blade to chordwise impulse from the weight of the strap attachment clevis and blade collar. The hydraulic shaker was turned off within 26 cycles. The damage the blade sustained was a separation of the upper and lower skins from the trailing edge longo between BS 60 and 85, and a small rip in the upper aft skin at BS 90 (Figure 79). After the fatigue fixture was repaired, the damage cimen was remounted in the test fixture and underwent the remain 0,000 cycles of the test. The blade continued to carry the beforeaccionads at the same frequency, indicating that it had suffered no important structural damage in this accident.

Fatigue tests of the S/N-005 blade that was ballistically damaged by a 23mm HEI-T projectile are discussed in Volume III of this report.

COMPOSITE BLADE REPAIR

The S/N-002 blade also demonstrated the efficiency of an aft-blade repair technique. Prior to the root fatigue test when the tip doubler was being bonded on, the aft portion of the blade in the region of the No. 5 spar tube was inadvertently collapsed by the vacuum used to hold the tip doubler in place while the resin cured. The blade was repaired (as shown in Figure 80) by cutting out the damaged area, inserting new honeycomb panels separated by a wedge of polyvinylchloride (PVC) foam, and bonding on an overlapping skin patch, top and bottom. This repair went through the entire 3,000,000-cycle fatigue test (including the test fixture accident described above) without difficulty, and demonstrated the efficiency of this repair technique.





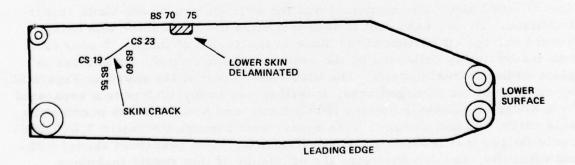
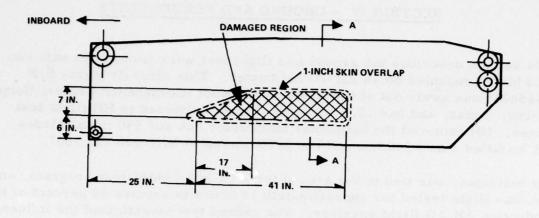


Figure 79. S/N-002 MTS blade damage resulting from fatigue fixture accident.



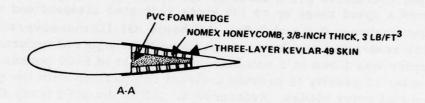


Figure 80. S/N-002 blade repair.

SECTION IV - GROUND AND FLIGHT TESTS

This section describes the ground and flight test work undertaken with two MTS blades mounted on an AH-1G helicopter. This aircraft (Army S/N 67-15683) was newly out of the Army Aero Depot Maintenance Center, Corpus Christi, Texas, and had 13.5 hours on it when delivered to HH flight test center. HH removed the helicopter main rotor hub and 540 metal blades and installed a new 540 hub and two MTS blades -- S/N-006 and -007.

The helicopter was tied to the ground for a 10-hour whirl-test program, and then was flight tested for approximately 15 hours to explore 80 percent of the production AH-1G flight envelope. The ground test investigated the influence of rotor rpm, collective pitch setting, and cyclic pitch inputs. The flight tests covered a speed range up to 136 knots indicated airspeed and vertical accelerations between 0.3 and 1.9g. All basic AH-1G maneuvers were flown in this restricted envelope except those that required ordnance firing. The helicopter was flown at a nominal gross weight of 8500 pounds and at a forward center of gravity to provide a direct comparison with the production (540) metal rotor blades, Reference 3. After the MTS blade flight test was completed, the 540 metal blades were reinstalled on the helicopter, and a short program was flown for a direct hub and mast loads comparison and for a pilot qualitative comparison of the two blade systems. The pilot reported a smoother ride with the MTS blades, but otherwise no significant differences in handling qualities. The rotor loads measured for the MTS blades were the same as or a little lower than those for the 540 blades.

INSTRUMENTATION

The instrumentation equipment listed in Table 10 was installed in the helicopter and on one of the MTS blades (S/N-007). Strain gage bridges were used to measure forces and moments, potentiometers measured positions, accelerometers measured accelerations, and transducers measured engine torque and airspeed. A 61-circuit slipring transferred signals out of the rotor and a 50-channel oscillograph recorded all data. An oscilloscope in the forward cockpit allowed the flight test engineer to monitor the alternating portion of five selectable load parameters (two at a time) during flight. In this way, he could have a real-time assessment of critical loads and did not have to wait for the oscillograph paper to be developed and analyzed. Control position

TABLE 10. INSTRUMENTATION LIST

Parameter			Galvanometer Frequency Response (Hz)
	D.C.	48	135
Rotor Blade Flapwise Bending Moment - MTS Blade (S/N-007) only	- BS	60	135
that to sealed bee bedriew as:	- BS	85*	135
	- BS	with the last the state of	135
	- BS	180	135
	- BS	Dallary or least at all	135
Rotor Blade Chordwise Bending	- BS	48	135
Moment - MTS Blade	- BS	45 85*	135
(S/N-007) only		environ anno.	
processors adally additionable stop		180*	135
Rotor Blade Torsion - MTS Blade (S/N-007) only	- BS	85	135
and months as a respective well-	- BS	180	135
Rotor Blade Drag Brace Axial Force			30
Rotor Blade Pitch Link Axial Load*			135
Hub Flexure Flapwise Bending Moment			30
Hub Flexure Chordwise Bending Momen		ni-1-1	
Rotor Mast Bending Moment - 0° (In li	ne with	n Blade)	135
Rotor Mast Bending Moment - 90°			135
Rotor Mast Torque			30
Accelerometer at CG - Low Frequency	Verti	cal	6
Lateral Control Actuator Axial Force			30
Lift Link Axial Force			30
Main Rotor Teeter Angle*			135
Engine Torque Pressure**			135 600
Lateral Stick Position**			600
Longitudinal Stick Position**			600
Collective Stick Position**			600
Pedal Position**			600
Rotor Aximuth Position			30
Accelerometer at CG - Vertical			30
Accelerometer at CG - Lateral			30
Accelerometer at CG - Longitudinal			30
Accelerometer at Pilot Seat - Vertical	**		30
Accelerometer at Pilot Seaf - Lateral	11		30
Accelerometer at Pilot Seat - Longitud	iinal		135
Indicated Airspeed			135

^{*} Selectable on cockpit monitor, two at a time. **Oscillograph and Cockpit Display.

indicators in the pilot's cockpit showed main rotor cyclic and collective pitch and tail rotor pitch. Figure 81 shows the special cockpit instrumentation and Figure 82 shows the oscillograph and its associated equipment located in the helicopter ammunition bay.

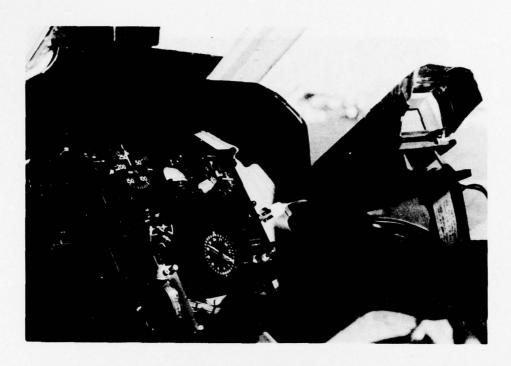
GROUND/WHIRL TESTS

The two MTS blades used for these tests were weighed and balanced individually, and made to match each other by adjusting the tip weights. The blades were mounted on a 540 hub and the whole assembly was balanced on a specially strengthened Army Balancing Kit (NSN 4920-00-572-0987). When the rotor was mounted on the helicopter, a Chadwick-Helmuth tracker/balancer (model 33A) was used to adjust the rotor track and balance. Minimum adjustments were needed and, once made during the ground tiedown test, did not have to be changed for the ground or flight tests. The flight test engineer, using the Chadwick-Helmuth strobe light blade tracker, reported that the blades tracked within 0.10 inch except for a few maneuvers in which one blade flew as much as 0.25 inch higher than its mate.

The helicopter was tied to a concrete pad as shown in Figure 83. The landing skids were clamped by U-bolts to a steel framework which in turn was bolted to the pad. This connection restrained the helicopter from moving horizontally and served to resist lateral, longitudinal, and directional moments. A large turnbuckle was the main lift tiedown link between the helicopter and the pad; it extended from an anchor buried in the concrete pad to a fitting in the helicopter directly below the lift link that connects the transmission to the airframe. A crossbar replaced the horizontal tail and its ends were tied to the ground by cables to restrain pitching moments. Lateral cables attached to the tail skid compensated for rotor torque. Torque compensation was aided by the pilot holding the two pedals in fore-and-aft alignment at all times. An arched steel bar over the cockpit was anchored to the basic steel framework under the helicopter. This was designed to give crew protection from a badly out of track rotor blade.

The ground tests gradually built up from low rpm and pitch conditions to larger and larger values until the rotor ran at maximum rated torque (50 psi) at design rpm (324) and was cycled through as much as 20 percent forward longitudinal cyclic pitch and 20 percent right lateral cyclic pitch. (Aft longitudinal and left lateral cyclic pitch were avoided because of the cable tiedown system that could not restrain the moments developed by these pitch inputs.)

The 10-hour ground test followed the schedule in Appendix D, Table D-1. All rotor loads were well below their endurance limits, as would be anticipated for a tiedown test of this type.



Forward Cockpit, Showing Oscilloscope Monitor



Aft Cockpit, Showing Control Angle Indicators
Figure 81. Special cockpit instrumentation.

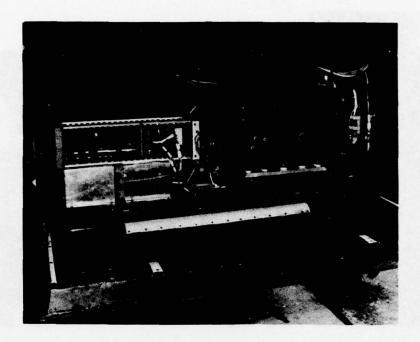


Figure 82. Oscillograph equipment in helicopter ammunition bay.

The data from the ground test is plotted in Figures 84 through 91. They show the mean loads for the various blade stations as functions of the mean lift link load; the spanwise distribution of mean flapwise bending moment, mean chordwise bending moment, and mean torsion moment; the cyclic blade loads at each station as a function of the resultant cyclic bending moment in the rotor mast; and the rotor mast cyclic bending moments in the plane of the rotor blade span axis with those in the plane perpendicular to the blade span axis. In these plots the MTS blade load limits and the maximum measured maneuvering loads (Reference 3) for the 540 rotor are tabulated to show that the MTS blade ground run loads are all well below any limits.

With the exception of one run, all the ground tests were made with the helicopter Stability/Control Augmentation System (SCAS) operating. The effect can be seen by comparing the data points shown as open symbols (SCAS "on") with those shown as solid symbols (SCAS "off"). SCAS in this helicopter includes not only the usual rate gyros but also a "feed-forward" cyclic stick position and stick rate augmentation circuit. With the helicopter tied to the ground, the gyros could not influence the control system, but the "feed-forward" function could. Figure 92 shows what typically happens in the tiedown mode with SCAS "on" and "off". With SCAS "on", as much as 12 percent more cyclic pitch input than called for by the control stick can be





Figure 83. Ground/whirl test installation.

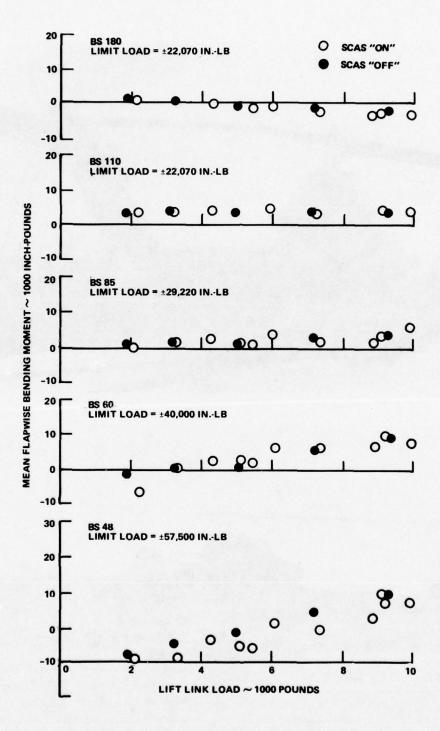


Figure 84. Mean flapwise bending moment versus lift link load, 324 rpm ground test.

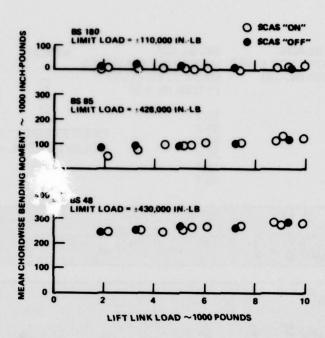


Figure 85. Mean chordwise bending moment versus lift link load, 324 rpm ground test.

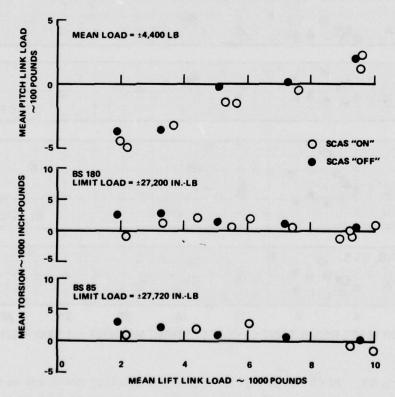


Figure 86. Mean pitch link load and mean torsion versus lift link load, 324 rpm ground test.

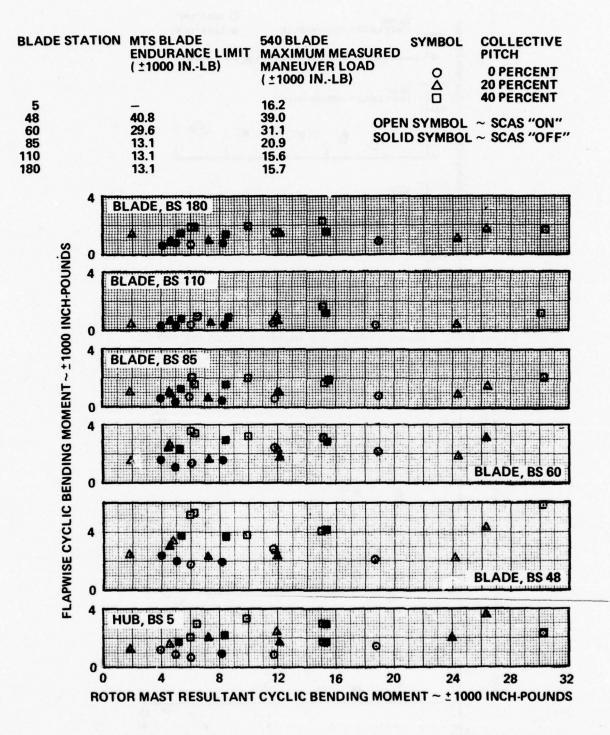


Figure 87. MTS blade cyclic flapwise bending moment versus rotor mast cyclic bending moment at 324 rpm.

BLADE STATION	MTS BLADE ENDURANCE LIMIT (±1000 INLB)	540 BLADE MAXIMUM MEASURED MANEUVER LOAD (±1000 INLB)	0	COLLECTIVE PITCH 0 PERCENT 20 PERCENT
8	<u>-</u>	175.3		40 PERCENT
48	116.4	153.0		
85	55.0	117.2		
180	31.8	43.7 OPEI		~ SCAS "ON" ~ SCAS "OFF"

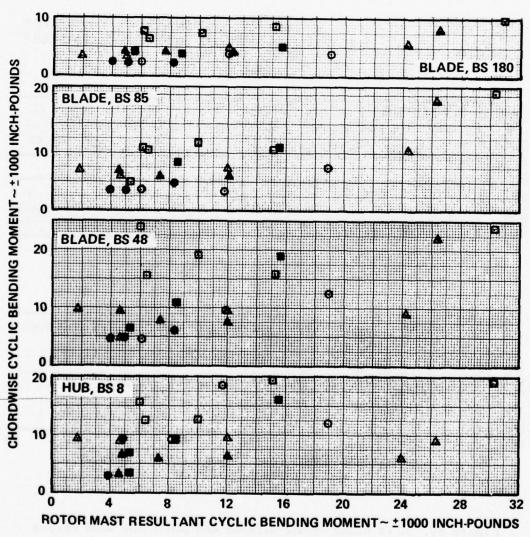
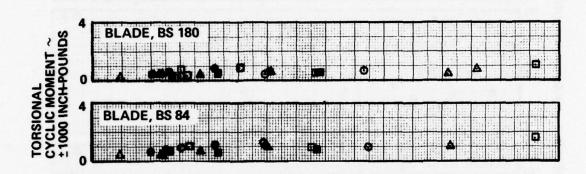


Figure 88. MTS blade cyclic chordwise bending moment versus rotor mast cyclic bending moment at 324 rpm.

BLADE STATION	MTS BLADE ENDURANCE LIMIT	540 BLADE MAXIMUM MEASURED MANEUVER LOAD	SYMBOL	COLLECTIVE PITCH 0 PERCENT
PITCH LINK	±1580 LB	±3150 LB	6	20 PERCENT 40 PERCENT
84	±14,700 INLB	±19,830 INLB		
180	±11,130 INLB			

OPEN SYMBOL ~ SCAS "ON" OPEN SYMBOL ~ SCAS "OFF"



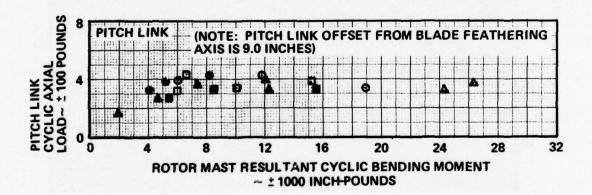


Figure 89. MTS blade cyclic torsion and pitch link load versus rotor mast bending moment at 324 rpm.

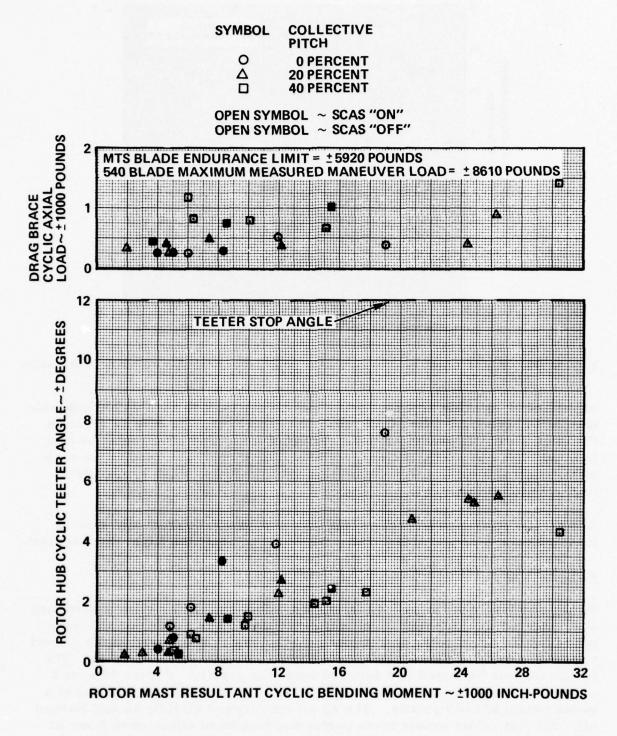


Figure 90. Drag brace load and teeter angle versus rotor mast bending moment at 324 rpm.

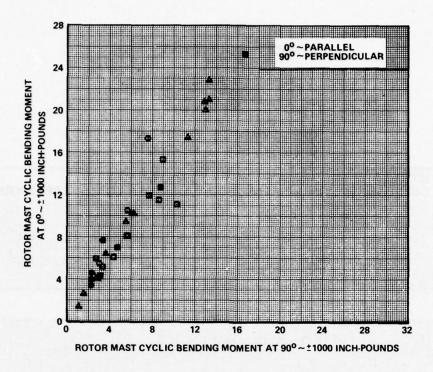


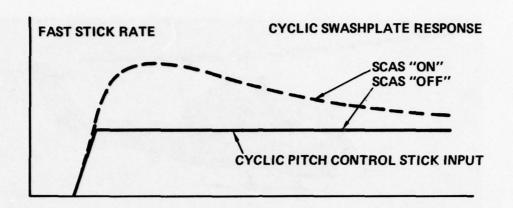
Figure 91. Rotor mast bending parallel and perpendicular to blade span axis.

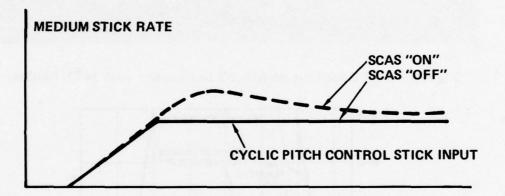
experienced, but this apparent overshoot bleeds back to zero within approximately 10 seconds. With SCAS "off", the control input is only as great as the stick input. In reading Figures 84 through 91, this effect must be kept in mind when comparing the open-symbol data which were read at the peak of the control input (stick position-plus-SCAS) and the solid-symbol data (control stick input only).

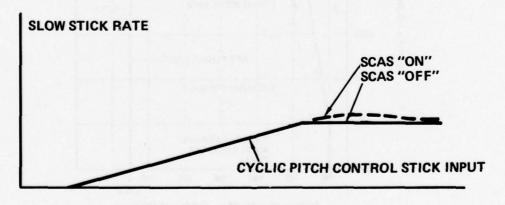
The ground tests showed that the MTS blades were free from any serious loads or dynamics problems, and were ready to begin the flight test program.

FLIGHT TEST

At the conclusion of the ground tests, the Safety of Flight Review Board met and approved the proposed flight test procedure. The helicopter was prepared for the flight tests by removing all tiedown fixtures used in the ground tests and returning the aircraft to its flight configuration, Figure 93. The helicopter was ballasted to a forward center of gravity. Figure 94 shows that the cg was at Fuselage Station (FS) 192.4 for takeoff with full fuel at a gross weight of 8685 pounds. The cg moved forward slightly as fuel burned off. All test points except those performed in ground effect were flown at







TIME

Figure 92. Schematic stability augmentation system response in helicopter tiedown mode.



Figure 93. Flight test of AH-IG helicopter with MTS blades.

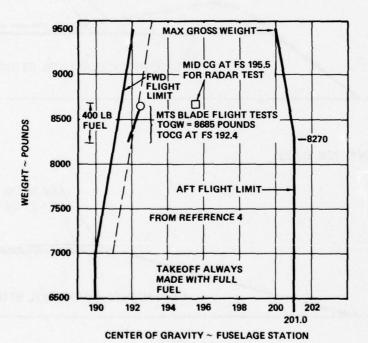


Figure 94. Center of gravity flight limits.

OPERATOR'S MANUAL, ARMY MODEL AH-1G HELICOPTER, Technical Manual 55-1520-221-10, Headquarters, Department of the Army, Washington, D.C., 12 December 1975, p. 7-6.

4000 feet pressure altitude. These conditions were chosen to expedite comparison with flight test data for the production metal (540) blades (Reference 3).

The flight tests were performed in a gradual buildup manner until 80 percent of the AH-1G flight envelope had been explored:

- a. 10 knots rearward to 136 knots forward
- b. 24 knots sideward flight
- c. Vertical accelerations between 0.3 and 1.9g

This required 21 flights whose test points are summarized in Appendix E, Table E-1. The airspeed/acceleration envelope that was explored in this program is shown in Figure 95.

A set of endurance limit loads for the MTS blade was established on the basis of the rotor blade fatigue tests, and on the hub, mast and controls information from the helicopter manufacturer. These limits are listed in Appendix E, Table E-2 along with 10-hour and 1-hour load limits. Appendix E, Table E-3 defines interaction equations that relate hub and mast

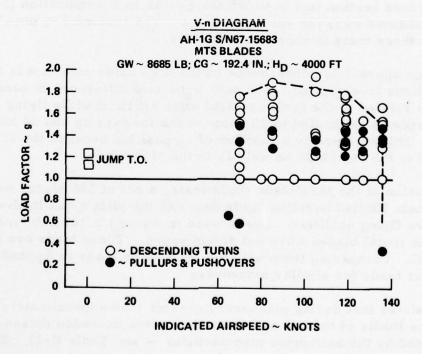


Figure 95. MTS blade V-n envelope - forward cg.

loads, and sets limits for these conditions. The MTS blade endurance limits were extremely conservative, but were exceeded during only 62 cycles in this test. The cumulative damage to the blade, actual cycles over endurance limit/allowable cycles over endurance limit = 0.0782, is insignificant.

The 50-channel oscillograph recorded the quantities listed in Table 10 during flight. The flight test engineer could monitor five of these in real time on the oscilloscope in his cockpit. Hub teeter angle was always shown on the scope. He could select any one of the other four: flapwise bending at BS 85, chordwise bending at BS 85 and at BS 180, and pitch link axial force. Usually he monitored chordwise bending at BS 85 because that was the blade parameter that ran nearest to the endurance limit.

A summary of the MTS blade loads is given in Figures 96 and 97 for level flight and for turns. The 540 blade loads, Reference 3, are superimposed for comparison. The loads are seen to be similar for the two types of blades, with the MTS blade loads being just a little lower. Appendix E lists all the MTS blade test data in tabular form and in plotted form. The loads reported here are the maximum loads encountered during the maneuvers-they did not necessarily occur at the maximum g condition, but usually during recovery.

Appendix F presents a tabulation of supplementary data taken in preparation for a radar cross section test in which the cg was in a midlocation (FS 195.5). All other conditions were the same as before. The limited V-g envelope investigated in these tests is shown in Figure 98.

There were no appreciable differences in the MTS blade rotor loads for the two cg conditions investigated. The only important difference in handling qualities was related to the cyclic control stick aft limit while flying rearward. The speed was limited to 10 knows at the forward cg and 24 knots at the mid-cg. This was purely a function of cg position because the 10-knot limit applied to the 540 blade as well as to the MTS blade.

At the conclusion of the MTS blade flight tests, a set of 540 blades was installed to obtain limited baseline loads data and the pilot's qualitative opinion of the relative flying qualities. Loads were measured in the hub, mast, and controls—the metal blades were not strain gaged. These loads are tabulated in Appendix G. Comparing them with the MTS blade loads in Appendix E shows similar loads for similar maneuvers.

Appendix E shows that during maneuvers greater than approximately 1.6g the endurance limits of the hub and mast were often exceeded (based on limits provided by the helicopter manufacturer — see Table E-2). These

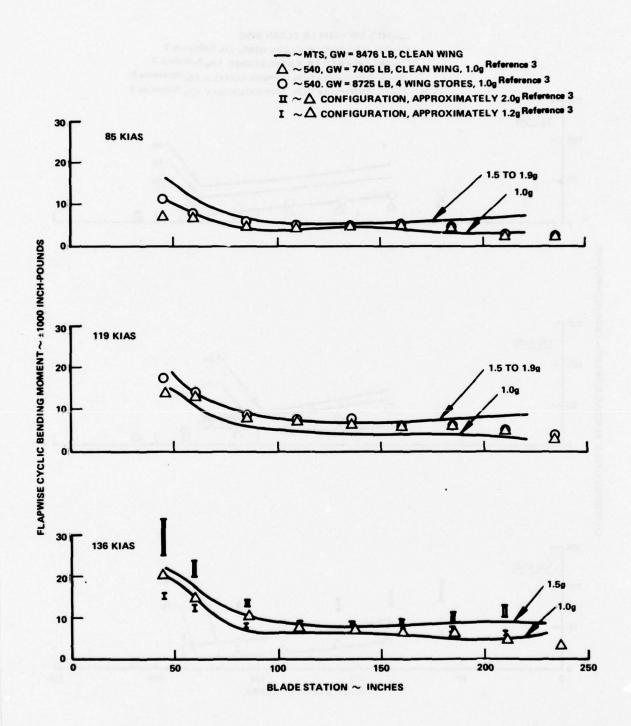


Figure 96. Flapwise bending moment comparison, MTS versus 540, CG ≈ FS 192.4.

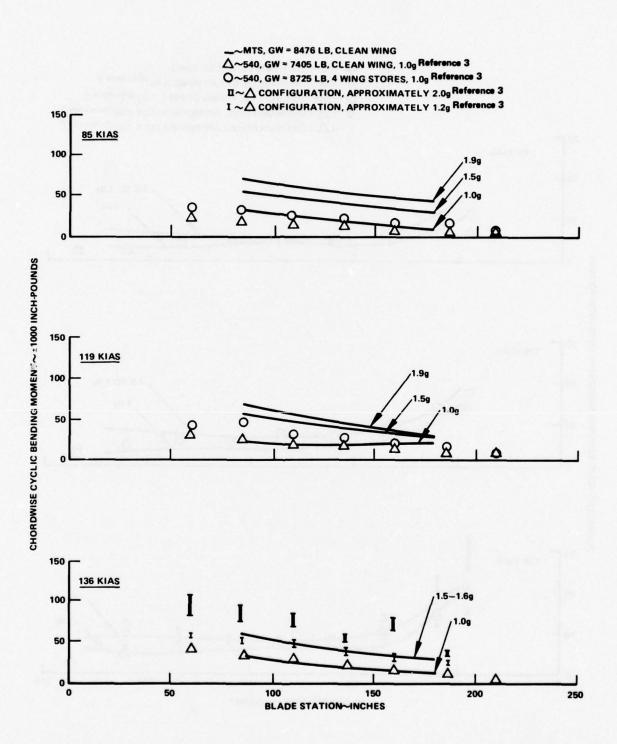


Figure 97. Chordwise bending moment comparison, MTS versus 540, CG ≈ FS 192.4.

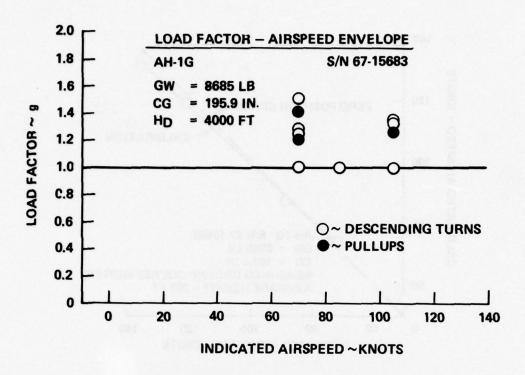


Figure 98. MTS blade V-n envelope - mid-cg.

tests conducted with the metal blades showed the same mast/hub loads, so it was concluded that the basic helicopter configuration induces damaging load cycles during moderate maneuvers.

It required 3.5 hours of ground/flight time to track and balance the 540 blades as compared with approximately 1.5 hours for each of the S/N-006/-007 and S/N-006/-008 MTS blade pairs. The latter combination was flown at the very end of the program to qualify these two blades for a radar cross section test to be performed later. In neither case was it necessary to bend the trim tabs of the MTS blade to achieve satisfactory track -- it was necessary for the metal blades. An airspeed calibration was flown with the 540 blades. It is shown in Figure 99 and applies equally to the MTS and 540 blade tests.

A comparison was made between the hovering efficiencies of the two types of blade by hovering in ground effect with the skids 2 feet off the ground. Figure 100 compares the hovering power coefficient/thrust coefficient (CQ/CT) ratio for the MTS and 540 blades. The power coefficient is based on main rotor mast torsion and the thrust coefficient on gross weight. Within the accuracy of the test conditions, there is no appreciable difference.

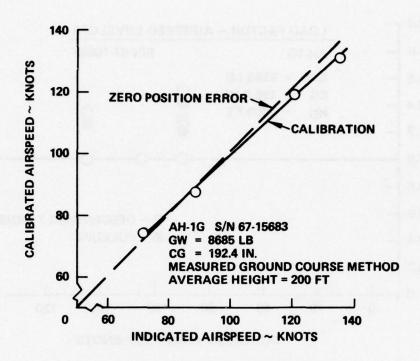


Figure 99. Airspeed calibration.

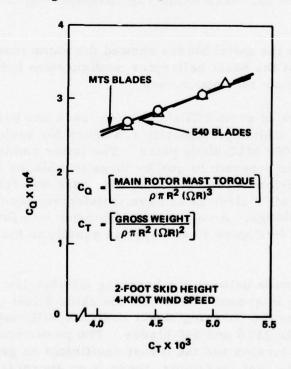


Figure 100. In ground effect (IGE) hover performance comparison - MTS versus 540 blades.

BLADE STRUCTURAL INTEGRITY

Two times during the flight test program there was a question whether the stiffness of the blade had changed significantly. The first was after Flight Number 8 whan an orange stripe was noticed on the top of the tail rotor drive shaft cover approximately in line with the orange-painted tip of the MTS blade. The second time was after the last flight when some blade surface imperfections (discussed below) were found on the S/N-007 blade. Flapwise stiffness checks were made, and no significant change was apparent either time.

The orange stripe was determined to have occurred on the ground during a hub teeter angle calibration check. Nevertheless, three 1/4-inch dowels (with their tips 6, 12, and 18 inches above the driveshaft cover) were mounted on the tail boom to indicate a close rotor approach by breaking off. None was ever broken, and the chase pilot reported that the tip of the main rotor was never seen to fly lower than the center of the tail rotor.

A procedure for inspecting the MTS blades after every ground run or flight consisted of a visual inspection of each blade and a coin-tap test of the areas shown by shading in Figure 101. Occasional surface imperfections were discovered by tapping from time to time, but were determined by HH, FSI, and Government personnel to be inconsequential with respect to safety of flight. Their appearance pointed to a case of locally insufficient bonding pressure during the resin cure cycle. In all future blades, adequate pressurization will be applied to prevent reoccurrence.

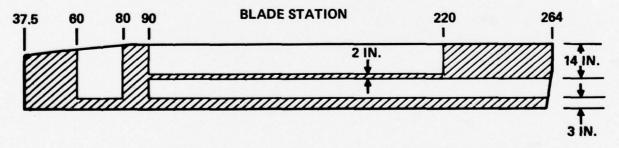


Figure 101. MTS blade tapping inspection areas.

CONCLUSION

The MTS blade program met all its goals. The design concepts integrated with the technology for fabricating the rather complex multi-tubular spar structure by the WFW, co-cure process were developed to the point where they can be reliably applied to a variety of aircraft structural components in addition to main rotor blades. The MTS blade was shown to fly like the metal blade it was designed to replace, proving that replacing a metal blade by a composite one can be routine. Its ruggedness permits it to survive severe damage (including the small explosive round threat). Tests show it to have a smaller radar cross section than the metal blade. Its leading edge erosion strip is replaceable in the field so the blade need not be discarded because of erosion damage. The stiffness, weight, and twist of the MTS type of blade, while required to match the 540 blade in this program, are readily tailorable to achieve optimum dynamics and performance. Its calculated 3600-hour fatigue life, resistance to damage, and repairability make for a longer service life than the metal blade.

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APPENDIX A

WEIGHT AND BALANCE ANALYSIS

MTS MAIN ROTOR BLADE ASSEMBLY - WEIGHT AND MASS PROPERTIES

INTRODUCTION

Design of the MTS Main Rotor Blade Assembly was developed in cooperation between Hughes Helicopters and Fiber Science, Inc. A basic requirement was to closely duplicate the mass properties of the Bell (PN 540-011-250) blade.

DISCUSSION

The weight and mass properties calculations included in this report were determined from drawings and material specifications furnished by Fiber Science. Preliminary estimates were performed to compare the mass properties of this design with the Bell blade resulting in some adjustments to the design. The report includes a comparison of the final actual MTS blade and the Bell 540 blade.

DRAWING REFERENCE

Fiber Science, Inc.

503-001	MTS Blade Assembly (Sheet 1 through 7)
503-003	Tracking Tab - MTS Blade
503-004	Bushing - Fwd Attach Fitting, MTS Blade
503-005	Bushing - Aft Attach Fitting, MTS Blade
503-007	Sleeve - Fwd Attach Fitting, MTS Blade
503-008	Sleeve - Aft Attach Fitting, MTS Blade
503-017	Nose Tip Weight, MTS Blade
503-020	Tip Weight - Adjustable, MTS Blade
503-022	Tip Weights, MTS Blade

TABLE A-1. MTS MAIN ROTOR BLADE ASSEMBLY, MASS PROPERTIES SUMMARY

Description	Hughes MTS Blade	Bell 540 Blade
Total Blade Weight (lb)	232.95	228.27
R (R Sta cg)(inches)	147.43	148.39
X (C Sta cg)(inches)	6.94	6.56
X (percent of chord)	25.7	24.3
WR (lb-in.)	34, 344	33, 874
WX (lb-in.)	1616.1	1497.8
WRR (lb-in. 2)	6, 464, 130	6, 426, 052
WRR (slug-ft ²)	1,395	1,387
WRX (1b-in. ²)	209, 414	196, 580
Σ WRX/ Σ WR .	6.10	5.80
Radius (feet)	22.0	22.0
Chord (inches)	27.0	27.0
Pitch Axis (percent of chord)	25.0	25.0

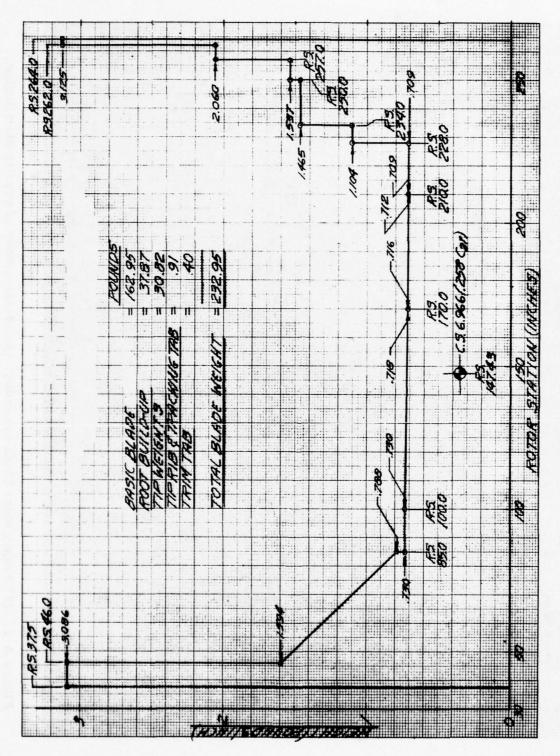


Figure A-1. MTS main rotor blade assembly, radial weight distribution.

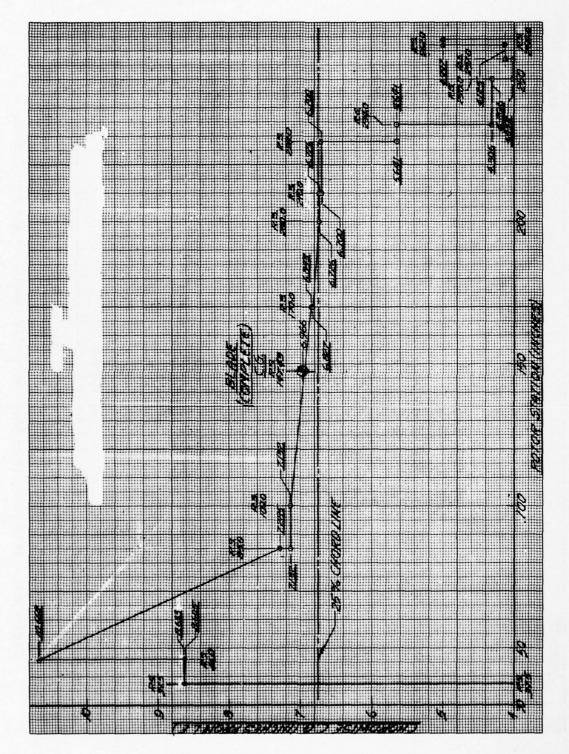
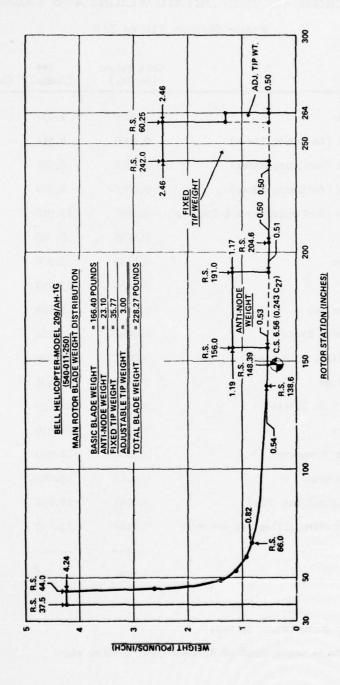


Figure A-2. MTS main rotor blade assembly, chordwise center of gravity distribution.



Radial blade weight distribution - Bell (PN 540-011-250). Figure A-3.

TABLE A-1. MTS MAIN ROTOR BLADE ASSEMBLY, TYPICAL BLADE CROSS SECTION DETAIL WEIGHT AND BALANCE

Rotor Station 210 to 228

	Unit Weight (Lb/In.)	X** (In c hes)	WX (Lb-In/In.)
L.E. Member	0.2469	2.052	0.5066
Tube No. 1 (Including Liner)	0.0200	4.511	0.0902
Tube No. 2 (Including Liner)	0.0200	6.891	0.1378
Tube No. 3 (Including Liner)	0.0200	8.984	0.1797
Tube No. 4 (Including Liner & Doubler)	0.0227	12.018	0.2728
Spar Caps	0.1826	6.729	1,2288
Spar Longos	0.0489	7.000	0.3423
Skin	0.0463	13.450	0.6227
L.E. Splice Cap	0.0145	1.160	0.0168
L.E. Abrasion Strip	0.0091	1.162	0.0106
Aft Tube (Including Liner)	0.0141	17.028	0.2401
Aft Honeycomb	0.0144	19.191	0.2706
Honeycomb T.E. Splice	0.0018	22.250	0.0401
T.E. Longos	0.0097	26.010	0.2523
Lightening Arrester	0.0006	26.000	0.0156
Vacuum Diaphram	0.0112	13.240	0.1483
Adhesive (Final Assembly)	0.0143	15.042	0.2151
Paint (Including filler and primer)	0.0119	13.450	0.1601
TOTAL	0.7090	6.700*	4.7505

^{* 24.8%} of Chord (27.00 inches)

^{**}X - Chordwise measurement of distance from leading edge.

TABLE A-2.

MTS MAIN ROTOR BLADE ASSEMBLY,
BLADE SPANWISE DISTRIBUTION

SHEET!							
*/17	R	WR	WRR	C	wc	WCC	WCR
1.54275	37.75	58 - 24	2198.5	8 . 631	13.32	114.9	502.7
1.54275	39 . 25	59.01	2257.1	8.630	13.31	114.9	509.2
1.54275	39 . 75	59 . 78	2316.5	3 . 623	13.31	114.3	515.8
1.54275	39.25	60.55	2376.7	8.626	13.31	114.8	522.4
1.54275	39 • 75	61.32	2437.6	8 . 625	13.31	114.8	528.7
1.54275	40.25	62-10	2499.4	9.623	13.30	114.7	535.5
1.54275	40.75	62.97	2561.8	3.621	13.30	114.7	542.0
1.54275	41.25	63.64	2625 1	3.620	13.30	114.6	543 . 6
1.54275	41.75	64.41	2689.1	8.619	13.30	114.6	555.1
1.54275	42.25	65 • 19	2753.9	3.617	13.29	114.5	561.6
1.54275	42.75	65.95	2919.5	3.615	13.29	114.5	568 • 2
1.54275	43.25	66.72	2935.3	8.613	13.29	114.5	574.7
1.54275	43.75	67.50	2952.9	9.612	13.29	114.4	531.2
1.54275	44.25	69 . 27	3020-8	3.610	13.29	114.4	587.8
1.54275	44.75	69 • 04	3089.5	8.608	13.23	114.3	594.3
1.54275	45.25	69.31	3159.9	8.607	13.29	114.3	600.8
1.54275 WEIGHT (Lbs.)	45.75	70 • 53	3229 • 1	8.605	13.29	114.2	607.3
26.23	41.75	1095	45872	3.613	226.03	1948	9436

TABLE A-2. (Continued)

MTS MAIN ROTOR BLADE ASSEMBLY,

BLADE SPANWISE DISTRIBUTION

JAKET &	2						
#/IN	R	WR	WRR	С	wc	WCC	WCR
1.58337	46.50	73.63	3423.6	10.581	16.75	177.3	779 - 1
1.56271	47.50	74.23	3525.9	10.495	16.40	172.1	779.0
1.54205	49.50	74.79	3627.3	10.409	16.05	167.0	778 . 4
1.52138	49.50	75.31	3727.8	10.321	15.70	162.1	777.3
1.50072	50.50	75 • 79	3827.2	10-234	15.36	157.2	775.6
1 - 49 006	51.50	76.22	3925.5	10-148	15.02	152.4	773.5
1 • 459 40	52.50	76.62	4022.5	10.061	14.68	147.7	770-9
1 • 439 74	53.50	76.97	4118 • 0	9.974	14.35	143.1	767.7
1 418 08	54.50	77 • 29	4212.0	9.887	14.02	138 • 6	764-1
1.39742	55.50	77.56	4304.4	9.801	13.70	134.2	760-1
1.37675	56.50	77.79	4394.9	9.714	13.37	129.9	755.6
1.35609	57.50	77.99	4483.6	9.627	13.06	125.7	750.7
1.33543	58.50	78 • 12	4570.2	9.540	12.74	121.5	745.3
1.31477	59.50	78 • 23	4654.6	9.454	12.43	117.5	739 • 5
1.29411	60-50	79 • 29	4736.8	9 • 367	12.12	113.5	733-4
1.27345	61.50	78 32	4916.5	9.230	11.82	109.7	726.5
1.25278	62.50	78 - 30	4993.7	9.193	11.52	105.9	719.8
1.23212	63.50	78 . 24	4968.2	9.107	11.22	102.2	712.5
1.21146	64.50	79 - 14	5040.0	9.020	10.93	98.6	704.8
1 • 19 09 0	65.50	78 • 00	5108.8	9.933	10.64	95.0	696.8
1.17014	66.50	77.81	5174.6	8.846	10.35	91.6	688 - 4
1 - 14948	67.50	77.59	5237.3	8.760	10.07	88.2	679 • 7
1.12992	69 - 50	77.32	5296.7	8.673	9.79	94.9	670.6
1.10915	69.50	77.02	5352.7	8 • 58 6	9.51	81.7	661.3
1 • 03 749	70.50	76 • 67	5405 1	3 • 499	9.24	79 • 6	651.6
1.06693	71.50	76.28	5453.9	8.413	9.97	75.5	641.7
1.04617	72.50	75.95	5498 • 9	9.326	8.71	72.5	631.5
1.02551	73.50	75.37	5540.0	8 • 239	8 • 45	69 • 6	621.0
1 • 00485	74.50	74.36	5577 • 1	9.152	8 • 19	66.8	610.3
•98418	75.50	74-31	5610-1	8 • 066	7.94	64.0	599 • 3
.96352	76.50	73.71	5639 . 9	7.979	7.69	61.3	588 • 1
.94286	77.50	73.07	5663.1	7.992	7.44	58 • 7	576.7
.95550	79.50	72.39	5682.8	7.805	7.20	56.2	565.1
.90154	79.50	71.67	5697.9	7.719	6196	53.7	553.2
•88088	30.50	70.91	5708 • 3	7.632	6.72	51.3	541.2
•86022	81.50	70-11	5713-8	7.545	6.49	49.0	529 • 0
•83955	82.50	69 • 26	5714-2	7 - 458	6.26	46.7	516.6
-8 1889	83.50	68 • 39	5709 • 5	7.372	6.04	44.5	504-1
79823 WEIGHT	8.4.50	67 • 45	5699.6	7 • 28 5	5.52	42.4	491.4
(Lbs.)							
46.44	63.30	2940	191756	9.124	423.72	39 08	26332

TABLE A-2. (Continued)

MTS MAIN ROTOR BLADE ASSEMBLY, BLADE SPANWISE DISTRIBUTION

SHEET	3						
#/IN	R	WR	WRR	C	wC	WCC	WCR
.72990	85.50	62.40	5335.0	7.132	5.20	37.1	445.0
. 72990	86.50	63-13	5460.5	7.132	5.20	37.1	450.2
. 72980	87.50	63.86	5587.5	7.132	5.20	37.1	455 . 4
. 72980	98.50	64.59	5716.0	7.132	5.20	37.1	460.6
• 72990	89.50	65.32	58 45 • 9	7.132	5.20	37.1	465.8
. 72980	90.50	66.05	5977.2	7.132	5.20	37-1	471.0
. 72980	91.50	66.79	6110-1	7.132	5.20	37.1	476.3
. 72950	92.50	67.51	6244.4	7.132	5.20	37.1	481.5
. 72990	93.50	68 - 24	6390-1	7.132	5.20	37.1	486.7
• 72980	94.50	69.97	6517.3	7.132	5.20	37-1	491.9
.72930	95.50	69.70	6656•0	7.132	5.20	37.1	497.1
. 72990	96.50	70.43	6796-1	7.132	5.20	37.1	502.3
. 7.2980	97.50	71-16	6937.7	7.132	5.20	37.1	507.5
. 72980	99.50	71.89.	7090.7	7.132	5.20	37.1	512.7
.72930 WEIGHT (Lbs.)	99+50	72.62	7225•2	7.132	5•20	37.1	517-9
10.95	92.50	1013	9-33-70	7.132	78 . 07	557	7222

TABLE A-2. (Continued)

MTS MAIN ROTOR BLADE ASSEMBLY, BLADE SPANWISE DISTRIBUTION

SHEET	-1						
#/IN	R	WR	WRR	C	WC .	WCC	WCR
. 729 72	100.50	73.34	7370-3	7.129	5.20	37.1	522.7
. 72955	101.50	74.05	7516.0	7.124	5.20	37.0	527.5
. 729 39	102.50	74.76	7663-1	7.120	5.19	37.0	532.3
	103.50	75.47	7811.6	7.116	5.19	36.9	537-1
. 729 05	104.50	76.19	7961.5	7.112	5.19	36.9	541.3
.72889	105.50	76.90	9112.7	7-109	5 • 19	36.8	546.6
.72872	106.5C	77.61	8265 • 4	7.104	5 • 19	36.8	551.3
• 72956	107.50	79.32	8419.4	7.100	5.17	36.7	556 • 1
• 728 39	108.50	79.03	8574.8	7.096	5.17	36.7	560.8
• 728 23	109.50	79.74	8731.6	7.092	5.16	36.6	565.5
• 728 06	110.50	50.45	8889.8	7.088	5.16	36.6	570.2
. 72789	111.50	81.16	9049 . 4	7.034	5.16	36.5	575.0
.72773	112.50	81.87	9210.3	7.080	5.15	36.5	579.7
.72756	113.50	\$2.58	9372.6	7.076	5.15	36.4	584.3
•72740	114-50	83.29	9536.4	7.072	5.14	36 • 4	589.0
• 72723	115.50	84.00	9701.4	7.068	5.14	36.3	593.7
.72707	116.50	84.70	9867.9	7.064	5.14	36.3	598 . 4
. 72690	117.50	85.41	10035.8	7.060	5.13	36.2	603.0
.72673	118.50	86.12	10205.0	7.056	5.13	36.2	607.7
• 72657	119.50	36.82	10375.6	7.052	5.12	36 • 1	612.3
.72640	120.50	87.53	10547.6	7.048	5.12	36.1	616.9
.72624	121.50	88.24	10720.9	7.044	5.12	36.0	621.6
. 72607	122.50	88.94	10995.6	7.040	5.11	36.0	626.2
. 72591	123.50	89.65	11071.7	7.036	5.11	35.9	630.8
• 72574	124.50	90.35	11249.2	7.032	5.10	35.9	635.4
.72557	125.50	91.06	11428 • 0	7.028	5.10	35.8	640.0
. 7.2541	126.50	91.76	11609 • 2	7.024	5.10	35.8	644.6
. 72524	127.50	92.47	11789 • 7	7.020	5 • 09	35.7	649 • 2
• 72508	128.50	93.17	11972.7	7.016	5.09	35.7	653.7
• 7249 1	129.50	93.88	12156.9	7.012	5 • 08	35.6	658 • 3
.72475	130-50	94.59	12342.6	7.009	5 • 08	35.6	662.9
. 72458	131.50	95.29	12529 • 6	7.004	5 • 09	35.5	667.4
.72441	132.50	95.98	12719.0	7.000	5.07	35.5	671.9
. 72425	133.50	96.69	12907.7	6.996	5.07	35.5	676.5
• 72409	134.50	97.39	13099 • 8	6.993	5.06	35 • 4	681.0
.72392	135.50	95.09	13291.3	6.989	5.06	35.4	685.5
. 72375	136.50	99 . 79	13495 - 1	6.985	5.06	35 - 3	690.0
• 72359	137-50	99.49	13690-3	6.981	5.05	35.3	694.5
• 72342	138 - 50	100-19	13976.8	6.977	5.05	35.2	699 • 0
• 72325	139.50	100.89	14074-7	6.973	5.04	35.2	703.5

TABLE A-2. (Continued) MTS MAIN ROTOR BLADE ASSEMBLY, BLADE SPANWISE DISTRIBUTION

SHEET	-5						
*/17	R	WR	WRR	C	WC	WCC	WCR
. 72309	140-50	101.59	14273.9	6.969	5.04	35.1	708 • 0
.72292	141.50	102.29	14474.5	6.965	5.03	35 - 1	712.4
.72276	142.50	102.99	14676.5	6.961	5.03	35.0	716.9
. 72259	143.50	103.69	14879.8	6.957	5.03	35.0	721.3
• 72243	144-50	104-39	15084-4	6.953	5.02	34.9	725.8
.72226	145.50	105.09	15290.4	6.949	5.02	34.9	730-2
• 72209	146.50	105.79	15497.8	6.945	5.01	34.8	734.7
.72193	147.50	106.48	15706.5	6.941	5.01	34.8	739 • 1
.72176	148.50	107-19	15916.5	6.937	5.01	34.7	743.5
.72160	149.50	107.88	16127.9	6.933	5.00	34.7	747.9
.72143	150-50	109 - 58	16340-6	6.929	5.00	34.6	752.3
.72127	151.50	109.27	16554.7	6.925	4.99	34.6	756.7
.72110	152.50	109.97	16770-1	6.921	4.99	34.5	761 - 1
.72093	153.50	110.66	16986.8	6.917	4.99	34.5	765.4
•72077	154-50	111.36	17204.9	6.913	4.95	34.4	769 • 8
.72060	155.50	112.05	17424.4	6.909	4.98	34.4	774.2
.72044	156.50	112.75	17645 1	6.905	4.97	34.3	778 . 5
.72027	157.50	113.44	17867.2	6.901	4.97	34.3	782.8
.72011	158 - 50	114-14	18090.7	6.997	4.97	34.3	787-2
• 71994	159 • 50	114.83	18315.5	6.893	4.96	34.2	791.5
.71977	160-50	115.52	18541.6	6.889	4.96	34.2	795.8
.71961	161.50	116.22	19769 • 0	6.885	4.95	34-1	800.1
.71944	162.50	116.91	19997.8	6.881	4.95	34.1	804.4
.71928	163.50	117.60	19227.9	6.377	4.95	34.0	808.7
•71911	164.50	118 • 29	19459 • 3	6.873	4.94	34-0	813.0
.71895	165.50	118.99	19692-1	6.869	4.94	33.9	817.3
• 71878	166.50	119.68	19926.2	6.865	4.93	33.9	321.6
.71961	167-50	120.37	20161.6	6.861	4.93	33.8	825.8
.71845	169.50	121.06	20395 • 4	6.857	4.93	33.8	830-1
• 71929 WEIGHT	169.50	121.75	20636-4	6.853	4.92	33.7	834.3
(Lbs.)							
50.69	134.91	69 37	943054	6.991	354.30	2477	47715

TABLE A-2. (Continued)

MTS MAIN ROTOR BLADE ASSEMBLY, BLADE SPANWISE DISTRIBUTION

SHEET	-6						
*/IN	R	WR	WRR	С	WC	wcc	WCR
.71564	170.50	122.02	20803.7	6.924	4.88	33.3	832.6
.71551	171.50	122.71	21044.6	6.820	4.88	33.3	836.9
•71538	172.50	123.40	21286.9	6.817	4.88	33.2	841.2
.71525	173.50	124-10	21530.5	6.914	4.87	33.2	845.5
.71512	174.50	124.79	21775-4	6.910	4.87	33.2	849.8
.71499		125-48	22021-7	6.807	4.87	33-1	954-1
•71486	176.50		22269 • 3	6.303	4.86	33.1	858 • 4
•71473	177.50		22513 • 3	6.900	4.86	33.0	862.7
	178.50		22768 • 6	6.797	4.86	33.0	867.0
•71447	179.50	128 • 25	53050•5	6.793	4.85	33.0	871.2
.71434	130.50	129.94	23273.2	6.790	4.85	32.9	875.5
.71421	191.50	129.63	23527.5	6.787	4.85	32.9	879.7
•71409	152.50	130.32	23783.2	6.783	4.94	32.9	884.0
•71395	183.50	131.01	24040 1	6.790	4.84	32.8	855.2
•71392	194-50	131.70	24298 • 4	6.777	4.84	32.8	892.5
•71369	185.50	132.39	24558 • 1	6.773	4.83	32.7	896.7
•71356	196.50	133.08	24919.0	6.770	4.93	32.7	900.9
.71343	197.50	133.77	25081.3	6.766	4.83	32.7	905.1
•71330	198 - 50	134.46	25345.0	6.763	4.52	32.6	909.3
•71317	189.50	135-14	25609 • 9	6.760	4.82	32.6	913.5
• 71304	190.50		25576.2	6.756	4.82	32.5	917.7
.71291	191.50		26143.8	6.753	4.81	32.5	921.9
•71278	192.50		26412.8	6.750	4.81	32.5	926.1
•71265		137.90	26683.0	6.746	4.81	32.4	930.3
•71252	194.50	138 • 58	26954.6	6.743	4.80	32.4	934.4
.71239	195.50	139.27	27227.5	6.739	4.80	32.4	938 • 6
•71226	196.50	139.96	27501.8	6.736	4.80	32.3	942.8
•71213	197.50	140.64	27777.3	6.733	4.79	32.3	946.9
•71200	198 • 50	141.33	28054.2	6.729	4.79	35.5	951.1
•71137 WEIGHT (Lbs.)	199.50	142.02	28 332 • 4	6.726	4.79	32.2	955•2
21.41	194.99	3961	734339	6.775	145.07	983	26930

TABLE A-2. (Continued)
MTS MAIN ROTOR BLADE ASSEMBLY,

BLADE SPANWISE DISTRIBUTION

JHEET T

#/IN WR WRR C WC WCC WCR 4.79 ·71180 200·50 142·72 28614·5 6.726 32.2 959.9 6.726 •71190 201-50 143-43 25900.7 4.79 32.2 964.7 29188 . 2 32.2 •71180 202-50 144-14 6.726 4.79 969.5 .71190 203.50 144.85 29477.2 6.726 4.79 32.2 974.3 .71180 204.50 145.56 29767.7 6.726 4.79 32.2 979.1 •71180 205-50 146-27 30059 . 5 6.726 4.79 32.2 983.8 .71180 206.50 146.99 30352.8 6.726 4.79 32.2 988 . 6 .71190 207.50 147.70 30647.4 6.726 4.79 32.2 993.4 •71180 208 • 50 148 • 41 30943.5 4.79 998.2 6.726 32.2 .71130 209.50 149.12 4.79 31241.1 6.726 32.2 1003.0 WEIGHT (Lbs.) 7.12 205.00 1459 299193 6.726 47.88 322 9815 #/IN R WR WRR C WC WCC WCR .70900 210-50 149-24 4.75 31.8 999.9 31416.0 6.700 .70900 211.50 149.95 31715.2 6.700 4.75 31.8 1004.7 6.700 4.75 ·70900 212·50 150·66 32015.8 31.8 1009.4 .70900 213.50 151.37 32317.8 6.700 4.75 31.8 1014.2 ·70900 214·50 152·08 4.75 31.8 1018.9 32621.3 6.700 4.75 31.8 1023.7 ·70900 215·50 152·79 32926.1 6.700 .70900 216.50 153.50 33232.4 6.700 4.75 31.8 1028.4 .70900 217.50 154.21 33540 • 1 6.700 4.75 31.8 1033.2 .70900 219.50 154.92 33949 . 3 6.700 4.75 31.8 1037.9 .70900 219.50 155.63 4.75 31.8 1042.7 34159.8 6.700 ·70900 220·50 156·33 34471.8 6.700 4.75 31.8 1047.4 4.75 31.8 1052.2 .70900 221.50 157.04 34795.1 6.700 •70900 222-50 157-75 35099.9 6.700 4.75 31.8 1056.9 31.8 1061.7 ·70900 223·50 158·46 6.700 4.75 35416.1 .70900 224.50 159.17 35733.8 4.75 31.8 1066.4 6.700 31.8 1071.2 31.8 1075.9 4.75 ·70900 225·50 159·35 36052.5 6.700 4.75 •70900 226-50 160-59 36373.3 6.700 31.8 1080.7 ·70900 227·50 161·30 36695.2 6.700 4.75 WEIGHT (Lbs.) 12.76 219.00 2795 612422 6.700 85.51 573 18726

TABLE A-2. (Continued) MTS MAIN ROTOR BLADE ASSEMBLY, BLADE SPANWISE DISTRIBUTION

SHEET	8							
*/18	P	WR	WRR	С	WC	WCC	WCR	
1.10400	229.50	252.26	57642.3	5.641	6.23	35 • 1	1423.0	
1.10400	229.50	253.37	58148 . 0	5.641	6.23	35 • 1	1429.2	
1.10400	230.50	254.47	58655.8	5.641	6.23	35 • 1	1435.5	
1.10400	231.50	255 - 59	59165.8	5.641	6.23	35 • 1	1441.7	
1.10400	232.50	256 . 69	59673 - 1	5.641	6.23	35 • 1	1447.9	
1.10400 WEIGHT (Lbs.)	233.50	257 • 78	60198•6	5.641	6.23	35•1	1454•2	
6.62	231.00	1530	353483	5.641	37.37	211	8632	
*/IV	R	WR	WRR	c	WC	WCC	WCR	
1.46460	234.50	343.45	90539 • 7	4.306	6.31	27.2	1478 . 9	
1.46460	235.50	344.91	31227.1	4.306	6.31	27.2	1485.2	
1.46460	236.50	346.39	81918 . 4	4.306	6.31	27.2	1491.5	
1.46460	237.50	347.84	32612.6	4.306	6.31	27.2	1497.8	
1.46460	239.50	349.31	33309 • 7	4.306	6.31	27.2	1504.1	
1.46460	239.50	350.77	34009.8	4.306	5.31	27.2	1510.4	
1.46460	240.50	352.24	94712.3	4.306	6.31	27.2	1516.7	
1.46460	241.50	353.70	95419.3	4.306	6.31	27.2	1523.0	
1.46460	242.50	355-17	36127.6	4.306	6.31	27.2	1529.3	
1.46460	243.50	356.63	8 68 39 • 4	4.306	6.31	27.2	1535.6	
1.46460	244.50	358 • 09	87554.2	4.306	6.31	27.2	1542.0	
1.46460	245.50	359 - 56	38271.3	4.306	6.31	27.2	1548 . 3	
1.46460	246.50	361.02	93992.4	4.306	6.31	27.2	1554.6	
1.46460	247.50	362.49	39715.9	4.306	6.31	27.2	1560.9	
1.46460			90442.3	4.306	6.31	27.2	1567.2	
1.46460 WEIGHT (Lbs.)	249 • 50	365.42	91171•7	4.306	6.31	27.2	1573.5	
	242.00	5671	1372863	4.306	100-91	434	24419	

TABLE A-2. (Concluded) MTS MAIN ROTOR BLADE ASSEMBLY, BLADE SPANWISE DISTRIBUTION

SWEET	9						
#/IN	R	WR	WHR	C	wc	WCC	WCR
1.53700	250.50	385.02	96447-1	4.052	6.23	25.2	1560-1
1.53700			97213.7	4.052	6.23	25.2	1566.3
1.53700		385 • 09	97993.4	4.052	6.23	25.2	1572.6
1.53700		-	98771.1	4.052	6.23	25.2	1579 • 3
1.53700			99551.9	4.052	6.23	25.2	1535.0
1.33760	234.30	3,1011	,,,,,,,,,	4.032	0.23	2302	137300
1.53700	255.50	392.70	100335.7	4.052	6.23	25.2	1591.2
1.53700			101122.7	4.052	6.23	100	1597.5
WEIGHT	2000	0,					
(Lbs.)							
	253.50	2727	691441	4.052	43.60	177	11051
••••	200-00						
#/IV	R	WR	WRR	С	WC	WCC	WCR
2.05990	257.50	530-40	136577.6	4.125	8.50	35.0	2187.9
2.05990	258 - 50	532.46	137640.5	4.125	3.50	35.0	2196.4
2.05980	259.50	534-52	139707.4	4.125	8.50	35.0	2204.9
2.05980	260.50	536 - 58	139778 . 5	4.125	8.50	35.0	2213.4
2.05980	261.50	539 . 64	140953.8	4.125	8.50	35.0	2221.9
WEIGHT							
(Lbs.)							
10.30	259.50	2673	69 3553	4.125	42.48	175	11024
#/IN	R	WR	WRR	С	WC	WCC	WCR
3.12490	262.50	320.26	215318 • 3	4.997	15.61		4098 • 8
	263.50	923.39	216961.9	4.997	15.61	78 • 0	4114.5
WEIGHT							
(Lbs.)							
6.25	263.00	1644	432290	4.997	31.23	156	8213
WEIGHT							
(Lbs.)							
232.95	147.43	34344	6464130	6.9381	616-14	11921	209414

APPENDIX B

STRUCTURAL DATA FOR MTS ROTOR BLADE FOR AH-1G HELICOPTER

REPORT TITLE	MTS Main Rotor Blade Assy, Stru	ctural Analys	is Report	_ REPORT NO	150-S-1001
PREPARED BY	D. H. Mancill	12/76	SUBJECT	MODEL NO.	
CHECKED BY			MTS Blade		

TABLE B-1. SUMMARY — STATIC MINIMUM MARGINS OF SAFETY

ITEM	LOAD CONDITION	MARGIN OF SAFETY
Blade Root End		
Main Pin Joint	Bearing on chopped E-glass/epoxy	.77
Aft Drag Brace Attach Point	Bearing on chopped E-glass/epoxy	.99
"FEP"		
Film Vacuum Bondable Material	Bond shear	.96
Basic Blade Section	e terro	at me
Leading Edge Longos	Tension	3.38
Spar Tube	Tension	1.80
Outer Skin Spar Cap	Shear	1.10
Spar	Shear	.95
Outer Skin	Tension	2.35
C-Channel	Shear	2.30
Aft Tube	Tension	3.00
Trailing Edge Longos	Buckling	.58
Blade Tip		
Nose Tip Weight Attach	Tension in L.E. longos	.92
Middle Tip Weight Attach	Tension in spar tube	.79

REPORT TITLE	MTS Main Rotor Blade Assy, Structural Analys	is Report	REPORT NO.	150-S-1001
PREPARED BY	D. H. Mancill 12/76	SUBJECT	MODEL NO	
CHECKED BY _		MTS Blade		

INTRODUCTION

This report contains the structural data for the MTS rotor blade for the AH-1G helicopter.

Section 1 presents computed and measured MTS blade physical properties.

Section 2 contains the static blade loads and stress analysis.

Section 3 presents the blade L-N fatigue curves.

Section 4 contains a comparative tip deflection study of the MTS blade and model 540 metal blade.

The Appendix contains computer output from the "BOX" program

REPORT TITLE	MTS Main Rotor Blade Assy, Structural Analysi	s Report	REPORT NO.	150-S-1001
PREPARED BY _	D.H. Mancill 12/76	SUBJECT	MODEL NO.	
CHECKED BY		MTS Blade		

COMPUTED AND MEASURED BLADE PHYSICAL PROPERTIES

The blade bending and axial stiffness properties were calculated by Hughes' section properties computer program utilizing laminate elastic properties generated by the "PROP" computer program. Blade torsional stiffness was calculated by Hughes' "BOX" computer program. Again "PROP" program supplied the laminate elastic properties (shear modulus). These calculated stiffnesses are compared to measured results obtained in full-scale blade stiffness tests.

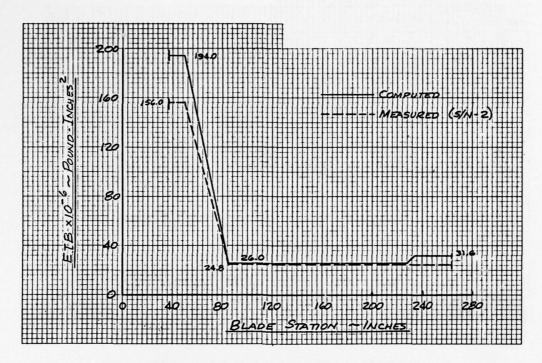


Figure B-1. MTS blade beamwise stiffness.

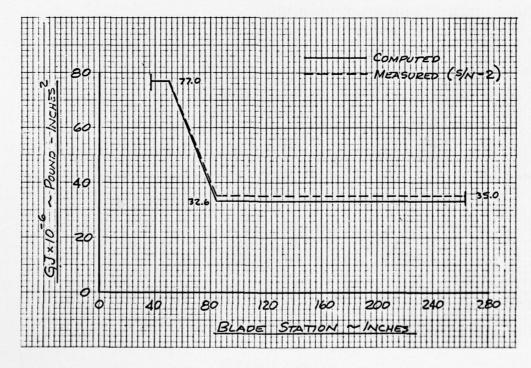


Figure B-2. MTS blade torsional stiffness.

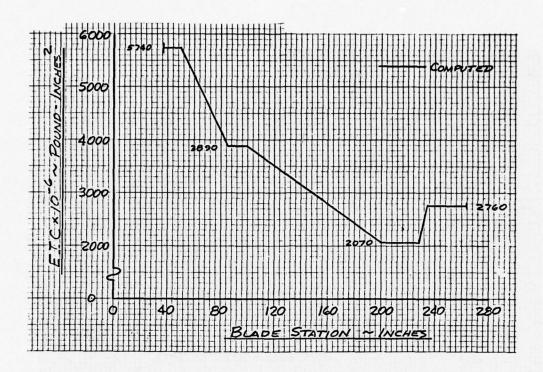


Figure B-3. MTS blade chordwise stiffness.

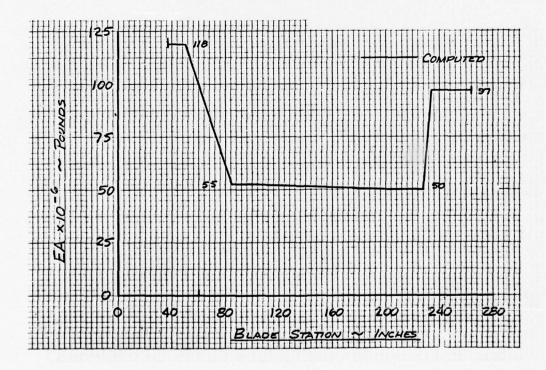


Figure B-4. MTS blade axial stiffness.

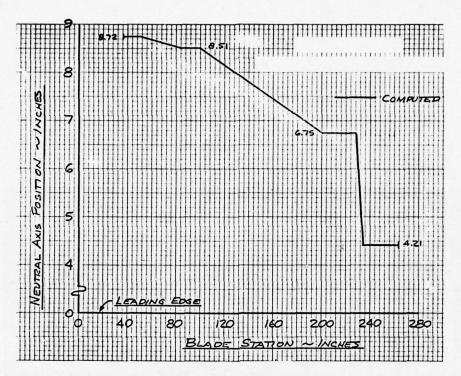


Figure B-5. MTS blade neutral axis position.

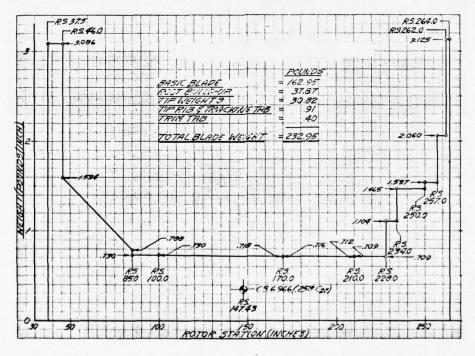


Figure B-6. MTS main rotor blade assembly, radial weight distribution.

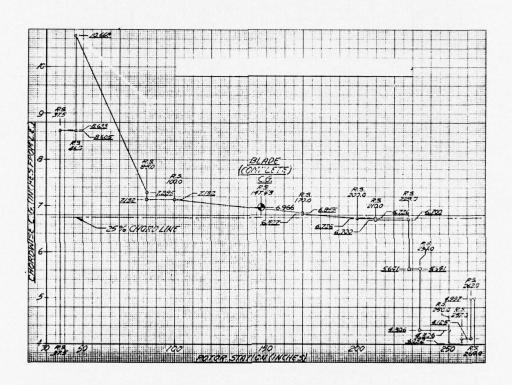


Figure B-7. MTS main rotor blade assembly, chordwise center of gravity distribution.

REPORT TITLE MTS Mai	n Rotor B	Blade Assy, Stru	ctural Analys	is Report	REPORT NO. 150-S-1001
PREPARED BY	D. 1	H. Mancill	12/76	SUBJECT	MODEL NO
CHECKED BY				MTS Blade	

STATIC BLADE LOADS AND STRESS ANALYSIS

This section contains the static load determination and structural analysis of the MTS blade for the AH-1G helicopter. The load requirements for the MTS blade are in all cases equal to the model 540 metal blade.

The loading conditions 1 thru 4 (see page 156) are identical to the conditions in Bell's stress report (Ref. 3 page 2.02). In addition, the MTS blade is checked for ground flapping and rotor starting.

All loads are limit loads unless otherwise noted. The ultimate factor is 1.5. The margin of safety is based on either yield or ultimate allowables depending on which is more critical.

The strength of the laminates was computed by the "PROP" computer program (computer output shown in Appendix). Experimental evaluation of the computed laminate strength was accomplished by tubular coupon tests. In addition, "Fan Belt" type of coupons were tested to evaluate the strength of unidirectional fibers/epoxy that wrap around bushings. This type of construction is used at the tip and root end of the blade.

The strength of the root end and blade tip is further substantiated (experimentally) by the root-end ultimate pull test and tip-end start/stop test.

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REPORT TITLE			REPORT NO. 150-5-1001
PREPARED BY O. MANCILL	DEC 3, 76	SUBJECT	MODEL NO.
CHECKED BY		MTS P	LADE

DESIGN STATIC LOADING CONDITIONS FOR THE MTS BLADE

THE CRITICAL STATIC LOADING CONDITIONS ARE SHOWN BELOW. CONDITIONS I THROUGH 4 ARE IDENTICAL TO THE MODEL 540 METAL BLADE CONDITIONS SHOWN IN THE BELL STRESS REPORT (REF 3, PAGE 2.02). GROUND FLAPPING AND MAIN ROTOR STARTING ARE ADDITIONAL CONDITIONS.

CONDITION	Mco IN-LB	RPM	HELICOPTER VERTICAL G'S	BLADE VERTICAL G'S
to the second	+450000	280	+3.5	-
2	-250000	280	+3.5	-
3	+450000	356	-0.5	-
4	-250000	356	-0.5	-
GROUND FLAPPING	_	0	1.0	2.67
MAIN ROTOR STARTING	72000	0	1.0	1.0

M .. IS THE CHORD BENDING MOMENT PER BLADE AT THE & OF THE ROTOR.

GROSS WEIGHT = 6600 LB

SIGN CONVENTION

FLAPWISE BENDING MOMENT - POSITIVE DENOTES TENSION IN THE COWER SIDE OF BLADE.

CHORDWISE BENDING MOMENT - POSITIVE DENOTES

TORSION MOMENT - POSITIVE DENOTES NOSE UP.

AXIAL WAOS - POSITIVE DENOTES TENSION.

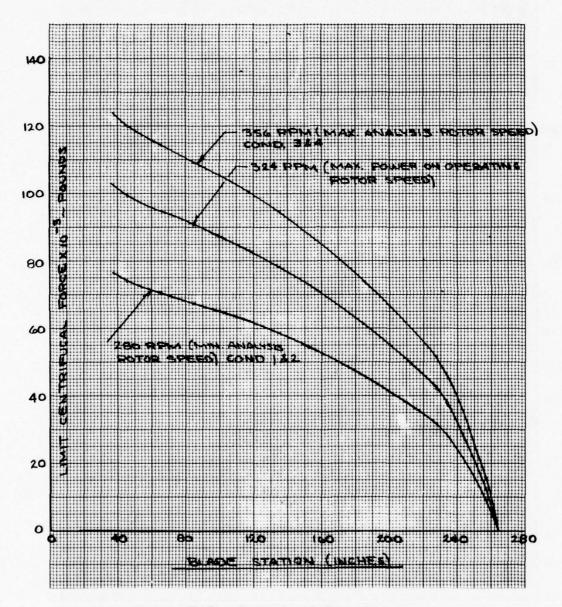


Figure B-8. Centrifugal force curves.

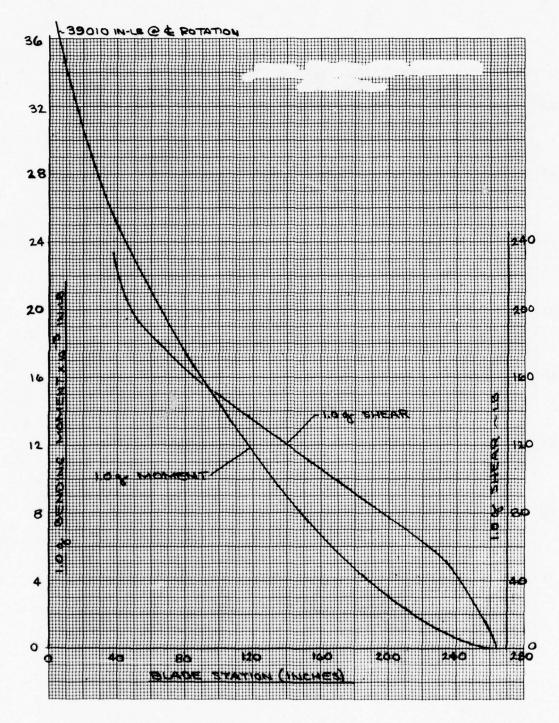


Figure B-9. 1.0g shear and moment curves.

REPORT T	ITLE							REPORT NO. 1	50-5-	1001
PREPARE	ON D. N	MICIL		OCT 14	1,76	SUBJE	CT .	MODEL NO		
CHECKED	87					MTS	BLAR	>€		
	TA	ABLE					ORCE DING M		. 0	
ATZ	AR	WIMON	ΔV	V	AM	м	ACF		PIFUGA	
3	27				2	59001	280 RPM	RPM	RPM	RPM
264				0		0		0	0	0
262	2.0	3.125	6.25	6.25	6.25	6.25	3661	3661	4902	5918
	5.0	2.06	10.3	16.55	57	63.25	5953	9/-14	12870	
257	7.0	1.537	10.76		153.5		6075			
250	16	1.465	23.44	27.31	624.5	216.8	12634		21010	
234	6	1.104	6.624	50.75	324.4	841.2	3408	20320	37920	45780
228	18	.709	12.76	57.37	1148	1166	6224	31730	42490	5129
210	10	,712	7.12	70.13	736.9	2314	3251	31960	50830	61360
200			10.70	77.25		3051	4588	41210	55180	6662
185	15	.713		87.95	1239	4290		45790	61310	7402
170	15	,715	10.72	98.67	1400	5690		50030	66990	8088
152.5	17.5	,720	12.60	111.27	1837	7527	4525	54560	73050	88200
135	17.5	.722	12.64	123.91	2058	9585	4047		78460	
117.5	17.5	.726	12.70		2280	11865	3571			
	17.5	.728	12.74	136.61	2502		3086		83260	
100	15	.730	10.95	149.35	2320	14367	2256		87380	105490
85	19.5	.990	19.30	160.30	3314	16687	3235	67520	90410	109150
65.5	19.5	1.392	27.14	179.6	3767	20000	3370	70750	94730	114370
46	8.5	3.086	26.23	206.74	1869	23768		74120	99250	119820
37.5	0.3	3.006	16.23	232.97		15637	4459	76560	102500	12376
AM	= VAY	AR }	∆ CF	$= \frac{\Delta V}{38}$	r { 28	30 211	= 2.	2273	ΔV R	280 RPM

REPORT TITLE			REPORT NO. 150-5-1001
PREPARED BY O. MANCILL	NOV 3 76	SUBJECT	MODEL NO.
CHECKED BY		MTS R	CAPE

TABLE B-3. ROTOR HUB 1.0g BENDING MOMENT AND SHEAR

ATE	AR	WE/INCH	ΔV	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	AM	STAN
39.6				225		25100
	13.2	6.875	90.75		3569	
26.4				315.75		28670
	13.2	6.900	91.08		4769	
13.2	A Charles			406.83		33440
	13.2	3.326	43.50		5660	
0	10.00			450.73		39010

REPORT TITLE

PREPARED BY D MANCILL NOV 19.76 SUBJECT MODEL NO.

CHECKED BY MTS BLADE

DRAG BRACE AND BLADE BOLT LOADS

STA
41.0

PMBX

PMBY

17.76

1.553

6.94

6.75

CENTRIFUGAL FORCE MOMENT ARM ABOUT THE MAIN BOLT

MCDRAG

147.43

FROM SIMILAR TRIANGLESS

CE ATE

STA 37.5

$$\frac{CF_{ARM} - 1.50}{41} = \frac{6.94 - 6.75}{147.43}$$
 % $CF_{ARM} = 1.553$

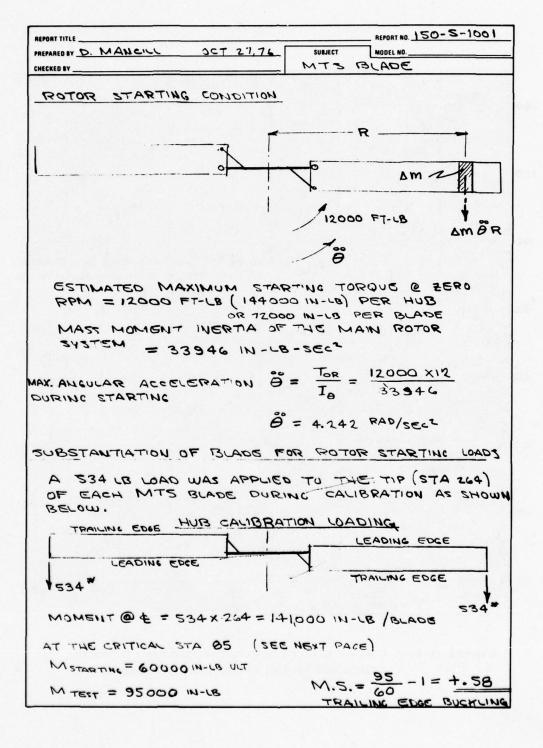
Medrae IS THE CHORD MOMENT DUE TO AIRLOAD DRAG.

MOMENT ABOUT THE MAIN BLACE BOLT

DRAG BRACE LOAD

PS IT THE SHEAR WAD DUE TO AIRLGAD DRAG.

REPORT TITLE							_ REPORT NO	120-2-	1001
	D. MAN	CILL	NOV	19,76	St	UBJECT	MODEL NO		
CHECKED BY _					_ ~	ITSE	BLADE	L	
DRAG	3 BRA	ICE AN	40 BC	ADE B	مرح لا	ZOAC	CONT'E	<u>></u> .	
		J JOA							
		C.F.							
P	MBY =	P3 -	POB.	SIN 35	5°				
P	WB =	Pmex	Pm	BY					
	DRAG	BRACE	(2)	(3)	BOLT	LOADS	_(LIMI	7)	
COND.	RPM	C.F.	Mc	Ps	MMB			PMBY	
COND.		STA 37.5	IN-LB	r 8	IM-LB	LB	LB	LB	CB -
1	280	76560	357000	2272	238100	-13410	87480	10060	88060
2	280	76560	195000	-1262	-313900	17670	62170	-11520	63230
3	356	123760	357000	2272	164800	-9279	131310	7660	131530
4	356	123760	-192000	-1262	-387200	21300	106420	-13630	107290
START-	0	0	55070	378	55070	-3100	2524	-1422	2897
2 F	REF 3	PAGE , PAGE	2.15						
	Ps =	(5.05)	× 10 ⁻³) 1	Mco					
									TO A TO SELECT



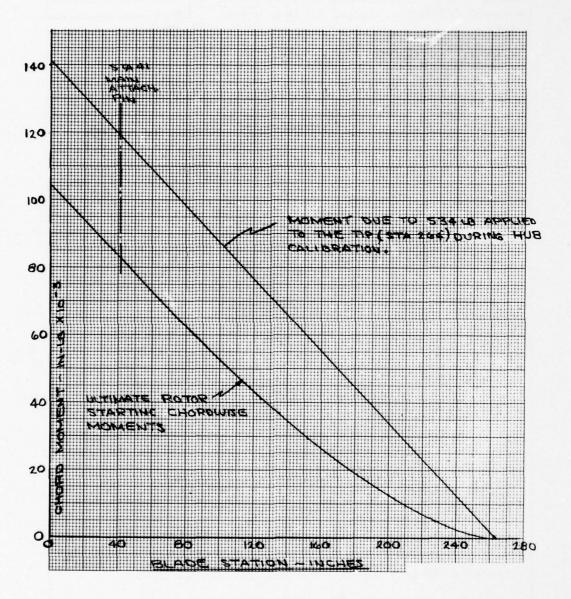
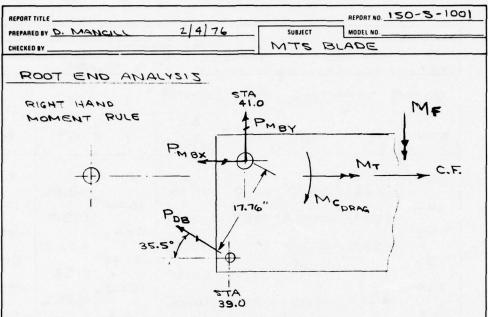


Figure B-10. Ultimate rotor starting chordwise moment compared to hub calibration loading.

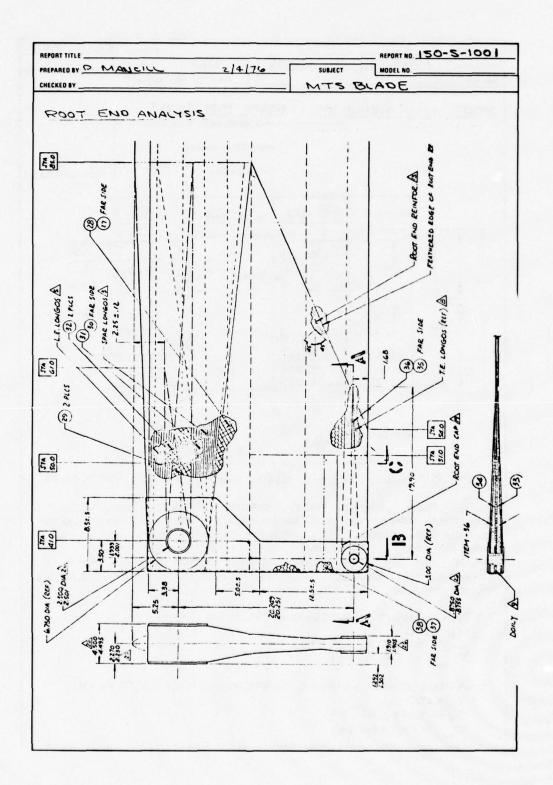
PREPARED BY	. IARHCIC	00.7	47,16	SUBJE	CT MODE	The state of the s	3-1001
CHECKED BY				_ M	5 130	ADE	
ROTO	R STAI	8.7.116 C	OADS ((LIMIT)		Alexander	
STA	R	mΔ	Am R2	۵۷ 8 مم	v	ΔM	M
264	263	.01619	1120	18,06	0	18.06	0
262	259.5	.02668	1797	29.31	18.06	163.7	18.0
257	253.5	.02788	1792	29,98	47.43	436.9	182
250	242	.06073	3557	62.34	77.41	1738	619
234	231	.01716	915.7	16.82	139.8	889.2	3240
210	219	.03306	1586	30.71	187.3	3095	634
200	205	.01845	775.4	16.04	203.3	1953	829
185	192.5	.02772	1027	22.64	226	3220	1151
170	177.5	.03264		22,33	246.9	4516	1506
152.5	A STATE OF THE STA	,03275		19.97	269.2	4886	1958
135	126.25	03290	524.4	17.62	285.2	5215	2446
117.5	108.75	,03301	390.4	15.23	306.8	5502	3518
85	92.5	.02837	242.7	11.13	333.2	4914	4009
65.5		.0500	283.1	15,96	349.1	6652	4675
46	1	,07031	218.5	16.63	365.7	6969	5372
37.5	41.75	.06795		12.03	377.8	3160	5688
0	ESTIM	ATED!	225	50.90	428.7	13122	72000
		Σ	16973	1	W= V	AV AR	

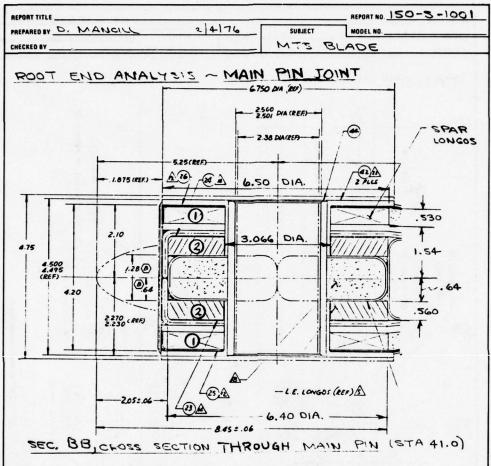


THE ROOT END ATTACHMENT OF THE BLADE UTILIZES A TWO PIN ATTACHMENT SCHEME SHOWN ABOVE. THE FORWARD PIN JOINT RESISTS THE MAJOR PORTION OF CENTRIFUGAL FORCE, FLAP BENDING MOMENT, TORSIONAL MOMENT, AND SHEAR LOADS. THE AFT PIN IS ATTACHED TO A DRAG BRACE AND WITH THE FWD PIN RESISTS THE CHORDWISE BENDING MOMENT.

LIMIT LOADS (REF. 3)

CONDITION		2	3	4	GROUNDING	ROTOR
MCDRAG IN-LB	357000	-195000	357000	-192000	0	55070
C.F. STA 37.5 LB	76560	76560	123760	123760	0	0
MMB IN-LB	238100	-313900	164800	-387200	0	55070
PDB LB	-13410	17670	-9279	21300	0	-3100
PMBX LB	87480	62170	131310	106420	0	2524
PMBY LB	10060	-11520	7660	-13630	0	-1422
PMB LB	88060	63230	131230	107290	0	2897
MF, IN-LB	62500	62500	-18000	-18000	-66800	-25000
My IN-LS		-39600 PITCH				222





THE SPAR LONGOS AND LEADING EDGE CONGOS
DRAPED ARGUND THE FORWARD PIN, ARE DESIGNED
TO CARRY TENSILE LOADINGS. COMPRESSION LOAD
CAPABILITY IS PROVIDED BY CHOPPED E-GLASS/
EPOXY INSIDE THE LOOP OF THE SPAR LONGOS AND
SYNTACTIC FOAM INSIDE THE LOOP OF THE LEADING
EDGE LONGOS.

SPAR LONGOS MATERIAL: HEVLAR / EPOXY

Vt = .50

Ex = 9.735 × 10 +6 PS1

Fxtu = 162,500 PS1

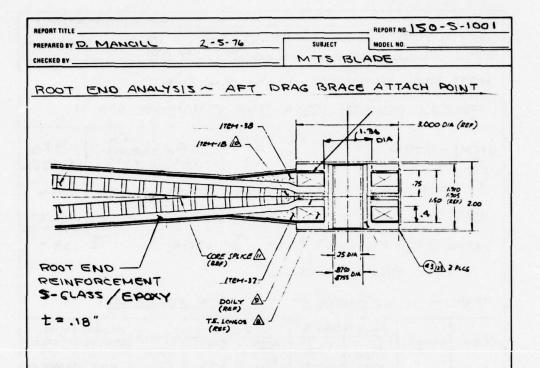
LEADING EDGE LONGOS MATERIAL ? S-GLASS/EPOXY

Vf=.55

Ex = 7.141 × 10 +6 PS |

Fxtu = 178750 PS |

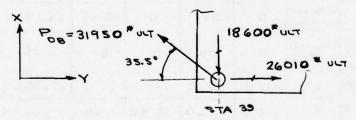
REPORT TITLE						REPORT	vo. 150-3	1001
	O. MANC	الد	2-5-		SUBJECT MTS R	MODEL N	0	
CHECKED BY					10113	CALL		
ROOT	END	ANAL	4515 ~	MAIN	BIN 20	THIC		
<u> 350</u>	TION P	ROPE	RTIES	e the	PIN	HOLE,	STA 4	.1
ITEM NO.	ITEN	4	E _X	A	E	AX BE	I B AM-	EIB
0	SPAR I	011605	9.735	3.64	35.	44 1	1.94	116.2
@	L.E. LO	NEOS	7.141	3.73	+ 26.0	06 3	3.258	23.27
TOTAL	FT_ =	139	5 X10+6 #-	IN2	S 62.1	0	Σ	139.5
			62.10 MARY AT		MAIN !	PIN JOI	NT	
			ZOAOJ	f ,	ULT KS	. 1	100 100 100	. MIN.
ITEM	COMO.	PMB	Me	DUE TO	DUE	TOTAL		MARCI
		KIPS		PMB	MB	2 4 4 4		SAFETY
		132.1	-	20.7		34.44		
SPAR LONGOS	4	160.9	- 27.0	25.22	3,96	29.18	(2)	+2.75
	GROUND FLAPPING	(3)0	- 99.7	٥	15.17	15.17		
HOPPED E-GLASS EPOXY	GROUND FLAPPING (3)		- 99.7	٥	-16.99	- 16.99	30.0	+.77
LEADING	١	132.1	93.75	15.19	5.76	20.95	142.7	+5.79
ONEOS	4	160.5	-27.0	18.50	1.66			13.15
70 181 2., B.	ADDITION ACTION OF LONGING CO.	TRIF S UL- DWAB RE W S BA ROUND 1605	THE ROC UGLAL O T. DESIGN T. DESIGN T. DESIGN TEAPPIN TO FLAPPIN LUG AND HE STRE TO CONSE	F 222, WITH SOUCEO AROUND HUGHES HE LOAD THE LENGTH	SOO LE OUT FA SINCE A BU TESTIN OS ARE OWER OF THE	SS, (CON NLURE THE UN SHING. NG REACTO CHOPPE SYNT	APAREI SO BY SO BY	ETIONAL ETION THE UPPE LASS



MAXIMUM DRAC BRACE LOAD = 21300 * LIMIT COND. 4

REF R 188

OR 31950 * ULT

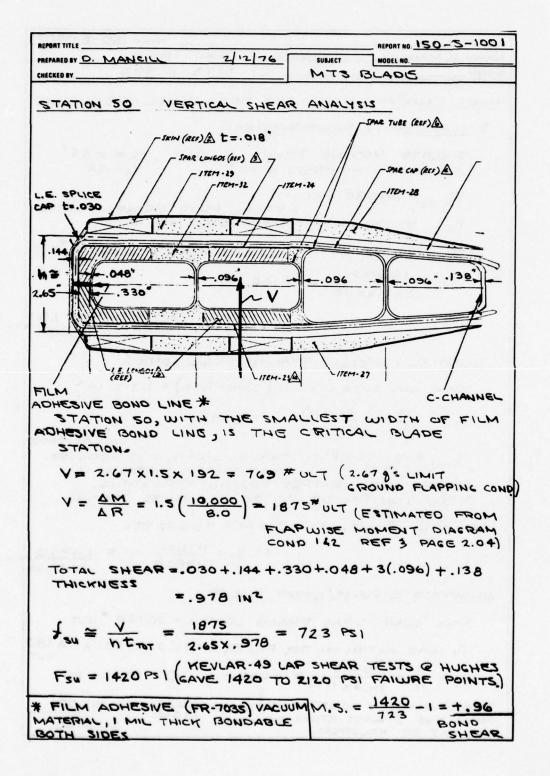


THE AXIAL LOAD IN THE X-DIRECTION IS CARRIED
BY THE S-GLASS/EPOXY REINFORCEMENT; THE TENSION
LOAD IN THE Y-DIRECTION IS CARRIED BY THORNEL 300/
EPOXY TRAILING EDGE LONGOS WHICH ARE DRAPED
AROUND THE PIN; AND THE COMPRESSION LOAD IN
THE Y-DIRECTION IS CARRIED BY CHOPPED E-GLASS/
EPOXY FILLER INSIDE THE LOOP OF THE TRAILING
EDGE LONGOS AND THE 5-GLASS/EPOXY RENFORCEMENT.

REPORT NO. 150-3-1001 PREPARED BY D. MANCILL 2-6-76 SUBJECT MTS BLADE ROOT END ANALYSIS - AFT DRAG BRACE ATTACH POINT S-CLASS/EPOXY REINFORCEMENT S-CLASS ROVING FERRO 5-1014; & = ±45° V4=.50 Fx TU = 40030 PSI 7 FX CU = 29600 PSI APPENDIX. REF PG 67 FOR 3.50" EFFECTIVE WIDTH AND P=-18600 ULT $f_c = \frac{18600}{2 \times 3.5 \times .18} = 14760 \text{ PSI}$ $M.S. = \frac{29600}{14760} - 1 = +1.01$ THORNEL 300/EPOXY TRAILING EDGE LONGOS TOTAL LUG AREA = 2x.40[3.00-1.36] = 1.312 IN2 $f_{ty} = \frac{P}{A} = \frac{26010}{1.312} = 19800PS1$ FROM APPENDIX FXTU = 162,500 PSI THIS ALLOWABLE IS REDUCED SINCE THE UMDIRECTIONAL FIBERS ARE WRAPPED AROUND A BUSHING. REDUCTION FACTOR BASED ON HUBBES TESTING REDUCED Fxtu = .73x 162, 500 = 118 600 PSI M.S. = 118600 -1 = LARGE TENSION CHOPPED E-GLASS/EPOXY FILLER MAX. COMP. DRAG BRACE LOAD = - 20120 "ULT 30 LOAD ACTING ON THE FILLER = 20120 COS 35.5 = -16380 $f_c = \frac{P}{A} = \frac{16380}{2 \times .4 \times 1.36} = 15060 \, PS$ THIS ANALYSIS IS CONSERVATIVE M.S. = 30,000 -1 = + .99

SINCE THE 5-GLASS EPOXY REINFORCE.

HAS NOT BE INCLUDED.



REPORT TITLE			REPORT NO. 150-5-1001
PREPARED BY D. MANCILL	2/3/76	SUBJECT	MODEL NO
CHECKED BY		MTS B	LADE

BLADE STATION 85

STATION 85 IS THE CRITICAL BASIC BLADE SECTION SINCE OUTBOARD OF THIS SECTION THE LOADS ARE LESS AND INBOARD, THE STRESSES ARE LESS (DUE TO LARGE INCREASES IN BOTH FLAPWISE AND CHORDWISE SECTION MODULI).

LIMIT LOADS @ STA 85

CONDITION	1	2	3	4
LIMIT C'S	+3.5	+3.5	-0.5	-0.5
LOADS RPM	280	280	356	356
CENTRIFUGAL FORCE - LBS	67400	67400	109,000	109,000
FLAPINISE MOMENT	21000	21000	-29200	-29200
CHORDWISE MOMENT	401700	-260	489040	85040
TORSION MOMENT	-35000	-32000	-35000	-35000

NOTES:

- (1) REFERENCE 2 (LIMIT LOAD ANALYSIS) FOR CHORDWISE MOMENT AND COND. ILZ FLAPWISE MOMENT.
- (2) REFERENCE I (MEASURED FLIGHT LOADS) FOR COND. 3 & 4 FLADWISE MOMENTS. MEASURED FLIGHT LOADS WERE FOUND TO EXCEED LIMIT LOADS FOR THESE PARTICULAR CONDITIONS.
- (3) LOAD SIGN WHYENTON:

FLAPWISE MOMENT - POSITIVE DENOTES TENSION

CHORDWISE MOMENT - POSITIVE DENOTES TENSION IN LEADING EDGE OF BLADE.

TORSION MOMENT - POSITIVE DENOTES NOSE UP.

(4) MODEL 540 CHORD LOADS MODIFIED ON WEXT PAGE SECTION PROPERTIES @ STA 85 FOR MTS BLADE.

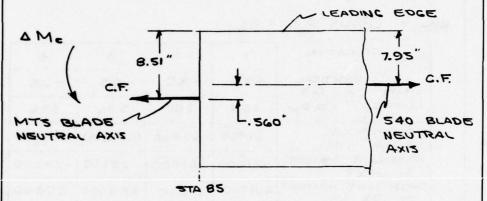
AXIAL STIFFNESS, EA = 55.0 XIO+6 LBS-IN2
FLAPWISE STIFFNESS, EI = 24.8 XIO+6 LBS-IN2
CHORDWISE STIFFNESS, EI = 3890 XIO+6 LBS-IN2

PREPARED BY D. MANCILL 9/15/76 SUBJECT MODEL NO.

CHECKED BY MTS BLADE

BLADE STATION 85

THE CHORDWISE MOMENT FROM REFERENCE ? (UMIT LOAD 540 BLADE ANALYSIS) MUST BE MODIFIED TO ACCOUNT FOR THE :560 INCH AFT. SHIFT OF THE NEUTRAL AXIS.



1 Mc = .560 C.F.

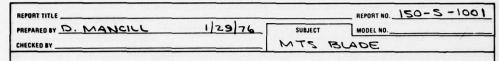
CONDITION LIMIT LOADS	1	2	3	4
CENTRIFUGAL	67400	67400	109000	000001
1 Mc	37740	37740	61040	61040
Mc 540	364000	-38000	428 000	24000
Mc MTS	401700	- 260	489040	85040

REPARED BY	MINIMUM	SAFETY	4. S. L	3.38 Tension	-	6.10 SHEAR	O 0.95	2.35 TENSION	2.30 S SHEAR 4	3.00 TENSON	BLA	MODEL NO. 2)-5-
	TS.	रुष	1	10700	11540	14880	10470	10500	31120	10630	1	1	STACHETA	
	5e.	PSI	1	1090	3574	LL89	5244	2480	9288	2083	1	1	-	2 45
740	Th. 3	PSI	178750	018771	15440	12540	39930	25320	36300	22410	162500	162500	0	£)(}
CRITICAL	407 PC	500	32420	40580	9087	467B	17550	7554	6919	2600	9034 47970	40770	ALLOWABLE BINING TENT	(Ftu -
AT THE	WISE DING	10 00 E	11200	6750	1512	1200	2000	-231	-236	-256	- 9034	-10 450 40770	THE	Fou = / (Ft - ft) (Fau)
> W	CHOROWISE BENDING	NCHES	8.316	5.01	5.01	7.510	3.660	4.290	4.290	4.2	18.99	18.43	STRENGTH; (2) THE	
u	NE	28 UCT	0	12610	2820	1961	0899	2845	2220	13 40	STTS	0		নি ব
BLADE	BENDING	NCHES	0	1.00	1.0	59.	1.26	1.0	.7S	.50	61.	0	BLE TENSILE SHEAR IS	Feu & fsu
1	8		4	00	Ø	J	a	W	T	J	I	н	1	1
	JASH		(0	6	8	60	4	4	4	<	+	NING	THE
	1187		LEADING	LONGOS	SPAR	SPAR CAP	SPAR	SHIN	C-CHANNEL	AFT	TRAILING	Longos	(1) THE ALLOW	F'tu=

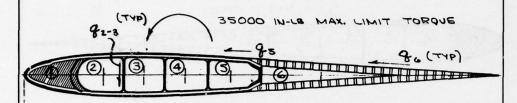
Francis, P.H. and Ko, W.L., SURVEY OF THE LITERATURE ON STRENGTH CHARACTERIZA-TION OF FIBER REINFORCED COMPOSITE MATERIALS; AFOSR Scientific Report, AFOSR-TR-71-2437, November 1970.

PREPARED BY	MANC	اسر		7	121	76		SUBJE		=	L NO.	50-	3-1	001
1		IL N	APPENDIX	178750		26 600	13970		45090	25990	37970	22450	162500	
Sas	t	STRESS	MAX. 356 RPM	14150		3170	1677	0.65)	3260	3330	3010	34150	
STATION	LIMIT	C.F. ST	FATIGUE 324 RPM	11640		2626	1390	0 0	4 0 0	2700	2758	2493	78790	
W H		E×	×10-6	7.141		1.601	.845	086		1.643	619-1	1.521	17.23	
ш	36.5	P. M. P.		4	00	00	υ		0	Ш	Ц	J	I	н
	CENTRIFUGAL FORCE STRESSES			S-GLASS/EPOXY	FIBER VOL = 55%	MEVLAR 49/EPOXY 6 PLIES OF ±45°, ZPLIES OF 90°	MEVIAR 49/EDOXY	KEVLAR 49/EPOXY	30 PLIES OF	N 4	E-GLASS/EPOXY	S-GLASS/EPOXY	THORNEL 300 CRAPHITE/), A 04 3
		Nut.		LEADING	LONGOS	SPAR TUBE	WIER SKIN,			DUTER SHIN	C-CHANNEL	AFT TUBE	FRAILING	Longos

REPORT TITLE			REPORT NO. 150-5-1001							
PREPARED BY	MANCILL 1/29/76	SUBJECT	MODEL NO.							
CHECKED BY		MTS B	CADE							
WEB 3-4 (TYP) (1) WEB 3 (TYP) (1)										
	WEB SUMMARY									
WEB	MATERIAL		THICK NESS							
ı	KEVLAR 49/ \24 PLIES OF EPOXY \ 3 PLIES O	± 45° F 90°	.162							
1-2	S-CLASS/EPOXY LONGOS		.20 (ASUMED)							
2	KEVLAR 49/ 8 PLIES O EPOXY S PLIES	OF 90°	. 254							
2-3	HEVLAR 49/ 12 PLIES OF	F ±45°	<i>360</i> .							
3	SAME AS 2	. 9 %	.254							
3-4	SAME 2-3		.096							
4	SAME AS 2	15000	.254							
4-5	SAME AS 2-3	1	.096							
5	SAME AS 2		.254							
5-6	E-CLASS CHANNEL &=		.080.							
6	MEVLAR 49/ 2 PLIES OF EPOXY	±45°	.018							
	AFT TUBE S-CLASS &	= ± 55°	.010							
(2) u										



STATION 85 TORSION ANALYSIS CONT'O.



THE MAXIMUM MEASURED TORQUE (BASED ON PITCH LINK WAD RATIOED TO STA. 85) IS

35000 IN-LBS REFERENCE 2,
PAGE 222, COND 71. BASED ON THIS TORQUE, THE SHEAR FLOWS WERE CALCULATED BY THE HUGHET COMPUTER PROGRAM "BOX" (SEE APPENDIX, p. 195)

SUMMARY OF SHEAR STRESSES

				~ 300	
WEB	UET	t	+5u	F54 */102	fsu/Fsu
1	#/WCH	.162	#/1W2 6877	15580	.441
1-2	217.9	,20	1090	10970	.0994
2	1332	,254	5244	11290	.464
2-3	19.25	.096	200	12217	.0164
3	1313	.254	5169	11290	.458
3-4	161.2	,096	1679	12217	.137
4	1151	.254	4531	11290	.401
4-5	343.1	.096	3574	12217	.293
5	808.4	.254	3183	11290	.282
5-6	743	.080	9288	31720	.293
SKIN	44.62	.018	2480	11000	.225
TUBE	20.83	.010	2083	34600	.0602

REPORT TITLE	-0.00			REPORT NO. 150-5-1001
PREPARED BY	D. Mancill	2-9-76	SUBJECT	MODEL NO.
CHECKED BY			MTS	BLADE

BLADE TIP

The tip weights are attached to the blade by a combination of both bond shear and mechanical locking. The two load paths are as follows:

1. NOSE TIP WEIGHT

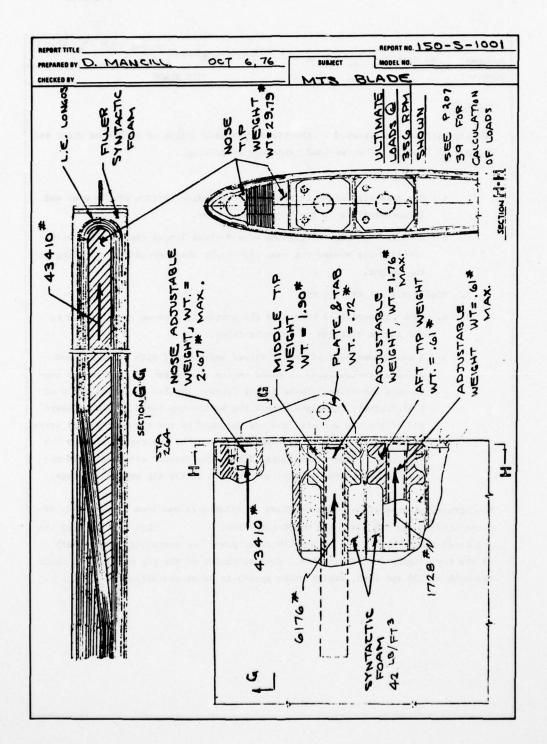
- a. The nose tip weight is bonded to the inside surface of the spar and forward surface of the forward spar tube.
- b. A continuous band of leading edge S-glass longos (impregnated with resin) wraps around the nose tip weight thus mechanically locking in the weight.

2. Middle and aft tip weights

- a. Each tip weight is bonded to the syntactic foam which is bonded to the inside surfaces of the spar tubes.
- b. A continuous band of Kevlar fibers impregnated with wet resin and under a tension force is wound on the tip weight fitting in one continuous operation. These Kevlar fibers, applied at a wrap angle of ± 45 degrees, interlace around the bottle-top shape of the outboard end of the tip weights, and are followed by the circumferential wraps, resulting in an effective mechanical lock of the tip fitting to the spar tube. Under centrifugal force, the elastic deformation of the ± 45° wraps is to contract and tighten on the tip weight fittings.

The structural strength of these methods of attachment has been successfully demonstrated by the MTS blade tip start-stop test. This test applied the simulated centrifugal force of 324 RPM (max. power on operating rotor speed) to the tip weights for 1200 cycles. Substantiation of the tip weight attachment strength at 356 rpm (max. design rotor speed) is presented herein.

BEST AVAILABLE COPY



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PREPARED BY D. MANCILL 007	- 7 76 F	CH01557	MODEL NO.	5-3-1001
	1,10	SUBJECT		
HECKED 8Y	L	MTS E	SCADE	
BLADE TIP				
LOADS				
MAXIMUM DESIGN RO	TOR SPE	033	356 RF	m 7
MAXIMUM POWER ON	OPERA			4.
ROTOR SPEED			324 RF	>M)
$cF = \frac{w}{\delta} r$	ພ້			
CENTRIFUGA	LOAT	05 ~LB		
	WEIGHT	[r	CF	CF
ITEM SEED NOW	LB	INCHES	LIMIT	ULTIMATE
			324 RPM	356 RPM
NOSE TIP WEIGHT PLUS	29.79	246.77		10110
2.67 CB. OF ADJUSTABLE WT.	2.67	257.50	23970	4'5410
MIDDLE TIP WEIGHT				
PLUS 1.76 LB OF ADJ.	4.38	261.12	3410	6176
WT. AND . TZLO PLATE				
AND TAB		2.22	795	
AFT TIP WEIGHT PLUS	122	262.26	954	1728
. GILB OF ADJUSTABLE	1	~62.20	334	1120
<u>w.</u> .		EV - Ft - Na		Jak I
NOSE TIP WEIGHT ATTA	CHMENT			
.068 R				
1 1 49	Ţ	PAPRIED =	43410	ULT
1 - 1 :	1.00			
1.50	-t.	TOTAL BOY		= 222 IN2
		AMER -	6.0 1 3 1	
3.00	,	P _ 4	3410 .	*
100 1	y year	A - 2	$\frac{3410}{22} = 1$	VERAGE
1.				SHEAR
				STRESS
	Fsu	= 1000 5	751	
1 1 1 1				
i is	,710,	M.S. =	196-1=	LARGE
			190	BOND
-40	x			SHEAR
1.89	# ASSUN	IES ALL -	THE LOAD	

REPORT NO. 150-5-1001 PREPARED BY D. MANCILL OCT 7.76 MODEL NO. SUBJECT MTS BLADE CHECKED BY _ BLADE TIP NOSE TIP WEIGHT ATTACHMENT CONT'D. THIS LOAD - L.E. LONGOS PATH ASSUMES 21705 ALL THE LOAD IS CARRIED BY 43410 " ULT THE LEADING FILLER EDGE LONGOS . SYNTACTIC 21705# FOAM AREA OF THE L.E. LONGOS WHICH WRAPS AROUND THE WEIGHT = 1.0 x . 32 = . 32 102 $f_{tu} = \frac{P}{2A} = \frac{43410}{2 \times 32} = 67830 PS1$ V4=.55 FOR 5-CLASS LONGOS FW = 178750 PSI THIS ALLOWABLE WILL BE REDUCED SINCE THE FIBERS ARE WRAPPED AROUND THE WEIGHT. REDUCTION FACTOR IS BASED ON HUGHES TESTING (RET 7). REDUCED Fty = .73 x 178 750 = 130,500 PSI M.S. = 130,500 -1 = +.92 L.E. TENSION

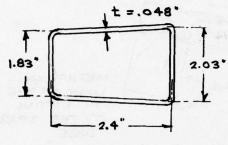
REPORT NO. 150-5-1001 PREPARED BY D. MANCILL OCT 8, 76 SUBJECT MODEL NO. MT3 BLADE BLADE TIP MIDDLE TIP WEIGHT ATTACHMENT MAX. TEETER ANGLE SPAP TUBE-6176* MECHANICAL LOCK OF THE TIP FITTING SYNTACTIC TO THE SPAR FOAM 42 CO/FT3 TUBE. THIS LOADING CONDITION ASSUMES THAT THE BLADE IS AGAINST THE UP TEETERING STOP (120) AND 13 ROTATING AT 356 RPM. SHEAR LOAD = Ps = 6116 SIN 12 = 1284 * ULT THE BEARING STRESS ON THE SYNTACTIC FOAM $J_{BRy} = \frac{P}{A} + \frac{MC}{I} = \frac{1284}{1 \times 2.5} + \frac{1284 \times 1.25 \times 1.25 \times 12}{1.0(2.5)^3}$ fory = 2054 PS1 TYPICAL COMPRESSION STRENGTH = 9500 PSI USE A STRENGTH REDUCTION FACTOR OF 2 $M. S. = \frac{9500}{2 \times 2054} - 1 = 1.31$ BEARING ON THE

SYNTACTIC FOAM

REPORT TITLE REPORT NO. 150-5-1001
PREPARED BY D. MANCILL OCT 8,76 SUBJECT MODEL NO.
CHECKED BY MTS BLADE

MIDDLE TIP WEIGHT ATTACHMENT CONT'D.

TENSION STRESS AT SECTION AA OF THE SPAR TUBE. THIS ANALYSIS CONSERVATIVELY ASSUMES NO LOAD TRANSFER THROUGH THE SYNTACTIC FORM.



SECTION AA

SPAR TUBE KEVLAR 49 /EPOXY

6 PLIES OF ±450

Fty = 26600 PSI

P = 6176 # ULT AREA = .4157 IN2

$$S_{tu} = \frac{P}{A} = \frac{6176}{.4157} = 14860 PS1$$

 $M.S. = \frac{26600}{14860} - 1 = \pm \frac{.79}{.79}$ TENSION IN SPAR TUBE

AFT TIP WEIGHT ATTACHMENT

PAPPLIED = 1728 # ULT AFT TIP WEIGHT LOAD

PAPPLIES = 6176 # ULT MIDDLE TIP WEIGHT LOAD

THE AFT TIP WEIGHT ATTACHMENT IS LESS CRITICAL THAN THE MIDDLE SINCE THE STRENGTH. OF BOTH ATTACHMENT STRUCTURES ARE IDENTICAL AND THE AFT LOAD IS 28% OF THE MIDDLE ATTACHMENT LOAD.

REPORT TITLE	MTS Main Rotor Blade Assy, Structural Analys	sis Report	REPORT NO	150-8-1001
PREPARED BY	D. H. Mancill 12/76	SUBJECT	MODEL NO.	
CHECKED BY	The second secon	MTS Blade		

BLADE L-N FATIGUE CURVES

The results of the Hughes' bench testing of three (3) MTS full-scale blade assemblies were used to develop the L-N curves in this report. This laboratory testing applied simultaneously cyclic fapwise, chordwise, and torsional moments as well as steady chordwise moment and centrifugal force to the blade assemblies. To account for scatter in fatigue data, the mean L-N curves were reduced statistically by the following factors to yield the design curves for life calculations:

L-N Curve Reduction Factors

Number of Fatigue Test Specimens	Reduction to Mean L-N Curve	Blade Loading Item
2	70%	Root End Torque
3	80%	Remaining Items

It should be noted that run-out points were conservatively assumed to be failures to generate the L-N curves (i.e. there were \underline{no} fatigue failures in this blade fatigue test program).

See Figures 72 through 78.

REPORT TITLE	MTS Main Rotor Blade Assy, Structural Analysis	Report	MEPORT NO	150-8-1001
PREPARED BY	D. H. Mancill 12/76	SUBJECT	MODEL NO	
CHECKED BY _	CONTRACTOR	MTS Blade		

COMPARATIVE TIP DEFLECTION STUDY OF THE MTS AND 540 METAL BLADES

Review of the deflection curves on the next page indicates that:

- 1. Above 60 RPM the MTS blade and the metal 540 blade have practically the same deflection.
- 2. Below 60 RPM the MTS blade has gradually increasing deflection (up to 20% at zero RPM).

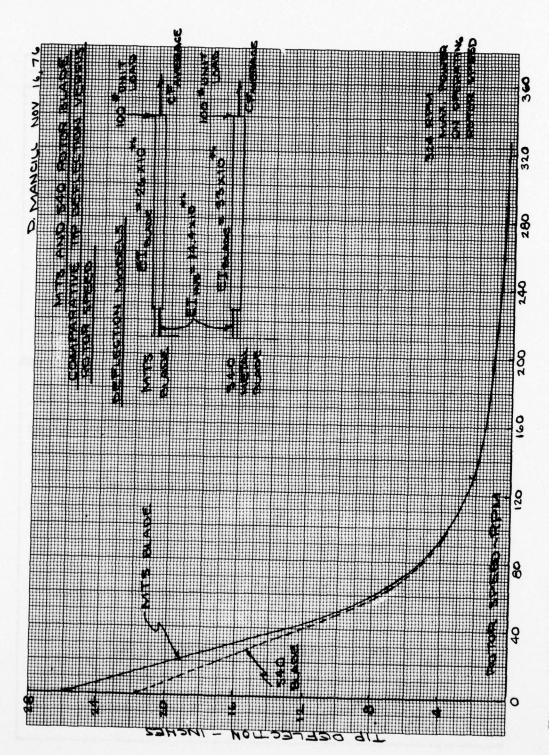
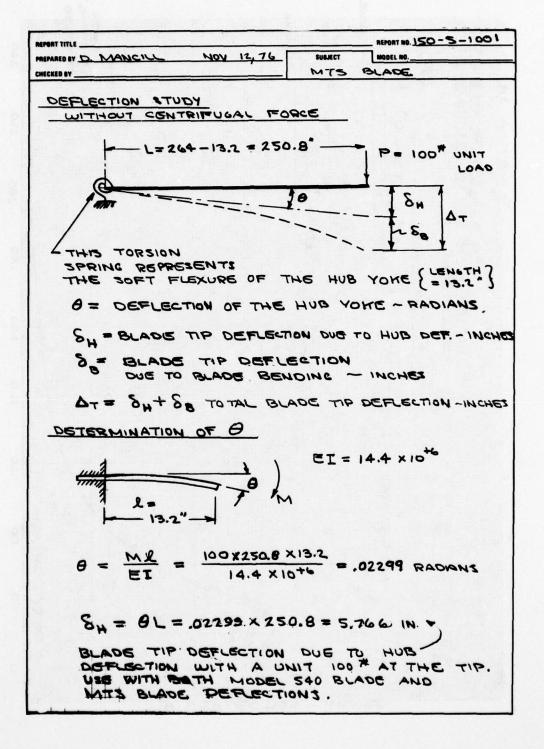


Figure B-11. MTS and 540 rotor blade comparative tip deflection versus rotor speed.

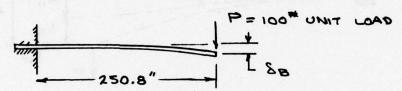


REPORT HO. 150 -8-1001
PREPARED BY D. MANCILL NOV 12,76 SUBJECT MODEL NO.
CHECKED BY MTS BLADE

DEFLECTION STUDY (WITHOUT C.F.)

FOR THIS COMPARATIVE DEFLECTION STUDY, THE FLAPWISE BENDING STIFFNESS IS ASSUMED TO BE CONSTANT ALONG THE BLADE.

THE STRUCTURAL BLADE DEFLECTION :



 $S_B = \frac{PL^3}{3EI}$ THE EI OF THE CONSTANT

BLADE SECTION WILL BE USED.

FOR THE SAO METAL BLADE

EI 540= 33.0 x10+6

THE "MTS BLADE

EIMTS = 26.0 X10+6

OR ET 540 = 33 = 1.27 STIFFNESS RATIO

SB 540 = 100 (250.8) 46 = 15,935 INCHES

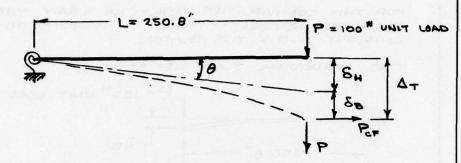
&B MTS = 100(250.8)3 3 x 26×10+6 = 20.225 INCHES

THE TOTAL DEFLECTION

ΔTS40 = SH + SBS40 = 5.766+15.935 = 21.701"

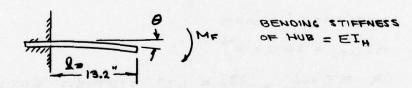
ATMTS = 84 + 8 BMTS = 5.766 + 20.225 = 25.391"

DEFLECTION STUDY (WITH CENTRIFUGAL FORCE)



CENTRIPUGAL FORCE WILL STIFFEN THE BLADE, THUS REDUCING THE DEFLECTIONS.

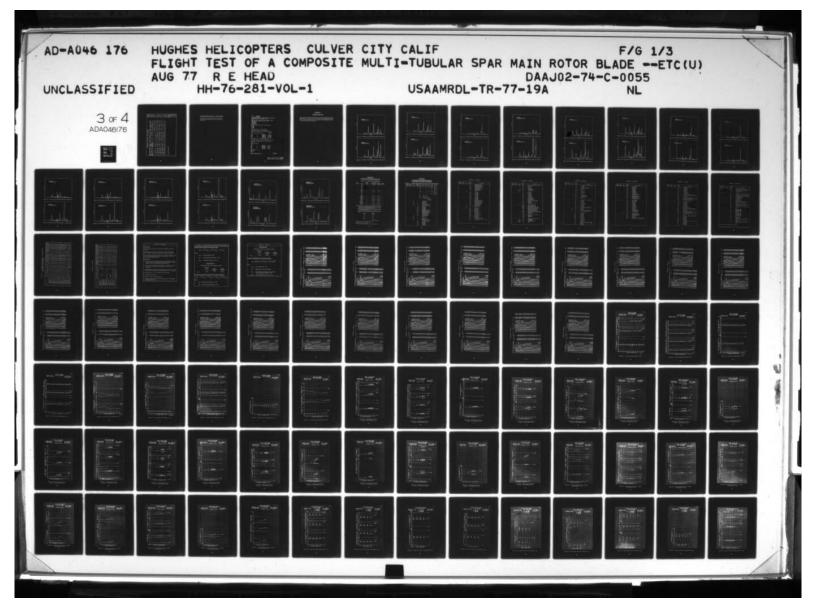
MOMENT AT THE HUB FLEXURG = MF



REPORT NO. 150-3-1001 DEFLECTION STUDY (WITH CENTRIFUGAL FORCE) BLADE DEFLECTION EI 8 FROM ROARK FOURTH SOITION, PC 151, CASE 13 SB = PCF (L- FTANH U) WHERE & = VEIB U= L Δ= 84+ 8B = OL+ 8B $\theta = \frac{1}{2} (\Delta_T - \delta_\theta) - (c)$ EQUATING EQUATIONS (a) AND (c) £[{PL-Pc Δ+} = + (Δ+-δ) SOLVING FOR AT $\Delta_{T} = \frac{EI_{H}}{EI_{L} + P_{L}} \left[\frac{PL^{2}}{EI_{H}} + \delta_{B} \right] ------(A)$ WITHOUT CENTRIFUGAL FORCE $\Delta_{T} = \frac{P L^{2}}{E L_{u}} + \frac{P L^{3}}{3 E L_{u}}$

Roark, FORMULAS FOR STRESS AND STRAIN, Fourth Edition, McGraw-Hill Book Company, 1963.

ORT PARI CKE	TITLE ED BY D BY	D. MA	nace	,	101	15,-	76	SUBJECT MT3	MODEL NO	-5-100
						7		prince	Jetu 3	ENESS - SA
	9	۵٦	25.991 15.566 7.036	2.177	1.183	. S71	.367	LOAD		M STIFF
	9	S.74.+®	25.991 17.999 11.435	7.622	6.657	6.286	6.106	OA01 TINO # 001 = 9		EIB = 26.0 XIO * (MTS BLADE) THE CONSTANT BLADE SECTION STIFFNESS A = $\frac{\text{EIH}}{\text{EIH}}$ $\left[\frac{2 \text{PL}^2}{2 \text{PL}^2} + S_2\right] = \left(\frac{3}{2}\right) \cdot \text{WHERE} \left(\frac{2}{2}\right) = \frac{100}{250.8} \left(\frac{250.8}{3}\right)$
BLADE	6	28	20.225	1.856	169.	.520	.340	0 11 0		MT BLAC
SHW	Ð	TANH T	.9862	2.1309 .99993 1.854	1.0000	1.0000	1.0000			CONSTAN
STUBY (MTS BLADE	9	þ	195.54 1.1816 .8572 97.77 2.5652 .9862	5.1309	7.6956 1.0000	24.44 10.262 1.0000	12.829	D = 13.2 W	+6 = 5.766 14	DG) THE
DEFLECTION	0	*	195.54	48.88	32,59	24.44	19.55	•-	4 x 10	& BLADE
0650	0	EI, +P. P.	1.0 .0.13 .6.53	.1856	TTT.	6060	1090.	= 250.6	ESS = EIu = 14.4 x11 13.2 (250.8)2 (100) 14.4 x10 +6	- (M)
	0	4	6.90	ng.6 10880	194.4 24480	259.2 43520	68000 ,00089	ONSTANTS L = 264 - 13.2 = 250.8 W	AUB STIFFNESS = 13.2 (26.0 ×10+6 (M
	9	RAR	0 4 4	29.6	194.4	259.2	324	CONSTANTS	AUB ST RL3P EIH	1 0
+	9	900 0% BALA	000	40	09	80	100	100	1 91	EI.



REPORT TITLE PREPARED BY	0.	MM	eiu.	,	100	16.7	6	<u> </u>	SUBJECT	MODEL NO
ECKED BY	_							_	MT	S BLADE
	- -	sept.	OR OR		26		TA		nerali	
	@	44	101.12	14.079	6.782	2.161	1.180	175.	367	
	0	S.74C+®	21.701	16.28	11,023	7.565	6.640	6.279	6.102	
06)	9	می	15,935 21,701	10.514 16.28	5.257	1.799	.874	.513	. 336	
40 BLA	0	TANH C	ı	.8135	.9792	9866.	1.0000	1.0000	1.0000	
5) XQ	9	þ	1	1.1384	2.2779 9752	55.07 4.5542 .5998	36.72 6.830 1.0000	9,1068 1.0000	11.384 1.0000	
TS NO	9	¥	1	220.3	1.0.1	55.07	36.72	27.54	22.03	
DEFLECTION STUDY (540 BLADE)	•	EI,+R.L	1.0	.8448	. 6153	.2856	rrri.	6060.	1090.	
D	0	Per	0	089	2720	129.6 10880	194.4 24480	259.2 43520	68000	8 33 X 10 to
	@	MAR	0	32.4	8,4	129.6	194.4	259.2	324	41
	е	% % % % % % % % % % % % % % % % % % %	0	0	20	40	09	00	00	Ą

COMPUTER PROGRAM DATA - BOX PROGRAM

This program determines the internal shear flow distribution and torsional stiffness of a multi-cell torque box.

RUN BOX 12:36 04/22/75 THIS FROGRAM DETERMINES THE INTERNAL SHEAR FLOW DISTRIBUTION AND TORSIONAL STIFFNESS OF A MULTI-CELL TOPACE BOX INPUT NUMBER OF CELLS IN THE SECTION INPUT CELL APEAS AND SUM (L/T) FOR CELLS FROM LEFT TO RIGHT NOTE: CELLS MUST BE NUMBERED FROM LEFT TO RIGHT ?2.763,133.248 74.73.345.301 74.58.348.587 ?4.33,3522+.171 711.96,7211.141 INPUT (L/T) FOR COMMON CELL WALLS STARTING FROM WEB 1-2 7122.872 7119.681 7120.238 7107.097 PROBLEM HAS GONE THRU SO OR MORE ITERATIONS LAST ITERATION NOT WITHIN 1% OF TOTAL SHEAR FLOW DO YOU WISH TO CONTINUE (5) MORE ITERATIONS ? (YES OR NO) Ge = 10 SHEAR FLOW DISTRIBUTION FOR GO = 1 CELL .069107 SHEAR FLOW CELL SHEAR FLOW 8.26259E-2 SHEAP FLOW CELL CELL 7.14323E-2 SHEAP FLOW CELL 5.01506E-2 SHEAR FLOW CELL 4.06643E-3 GJ = 32.57TOTAL TORQUE 3.25678 CELL STIFFNESS EQUALS .307052 T/G RADIANS/UNIT LENGTH OF CELL DO YOU WISH TO DETAIN THE SHEAR FLOW DISTRIBUTION FOR A GIVEN TORQUE ? (YES OR NO) ENTER AFPLIED TORQUE 710000 SHEAR FLOW CELL 212.194 253.704 CELL CELL SHEAF FLOW 250.038 SHEAR FLOW 219.334 153.986 CELL CELL SHEAR FLOW CELL 12.4676 APPLIED TOPGUE 16606 NOW AT 890 SRU(5:0.6

READY

USAGE ON 04/22/75 AT 12:39:58 SRU'S:1.1 ELAPSED TIME: 00:63:40 G.F. ACHER

BEST AVAILABLE COPY

APPENDIX C

DYNAMIC TEST DATA

The data from the input load frequency sweeps are plotted here for MTS flight blades, S/N-006 and -007, mounted on a 540 hub (NSN 1615-00-918-9357). This is followed by data from a pair of 540 blades (NSN 1516-00-178-9680) mounted on the same hub.

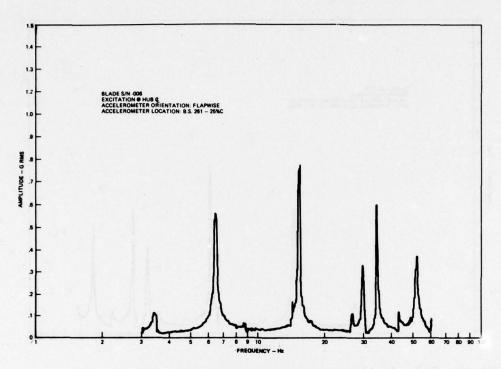


Figure C-1. MTS main rotor assembly dynamic response test.

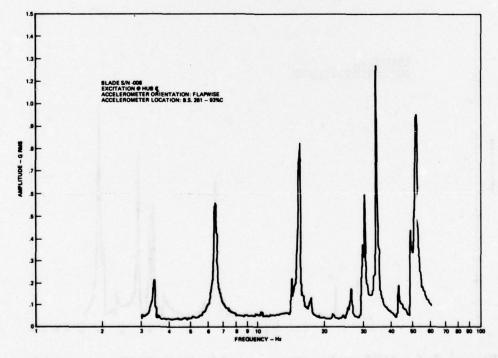


Figure C-2. MTS main rotor assembly dynamic response test.

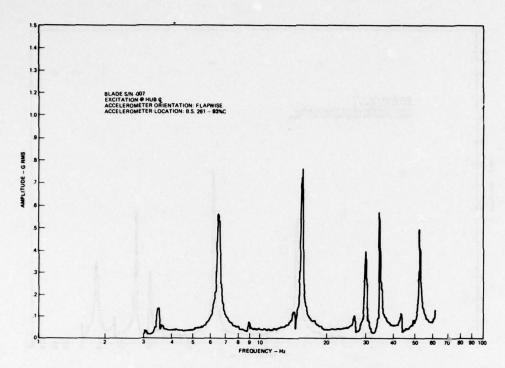


Figure C-3. MTS main rotor assembly dynamic response test.

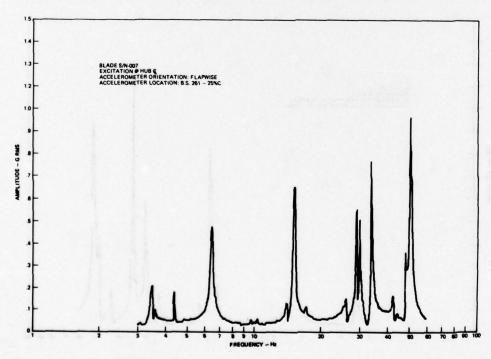


Figure C-4. MTS main rotor assembly dynamic response test.

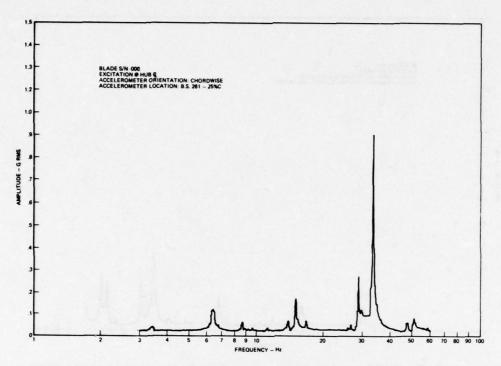


Figure C-5. MTS main rotor assembly dynamic response test.

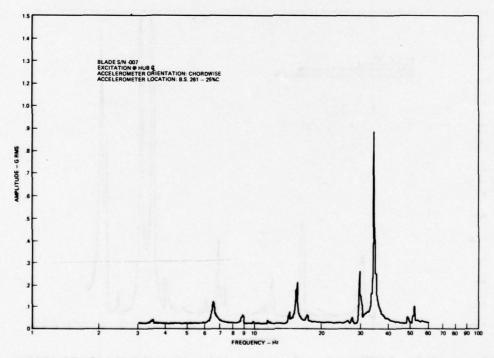


Figure C-6. MTS main rotor assembly dynamic response test.

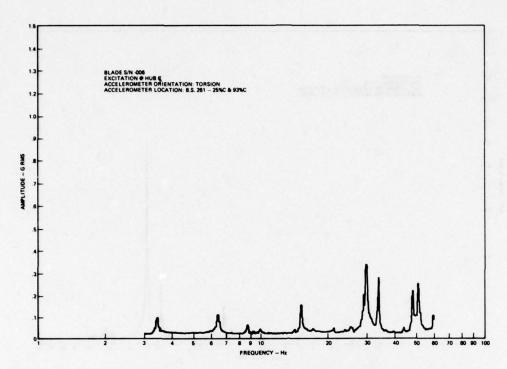


Figure C-7. MTS main rotor assembly dynamic response test.

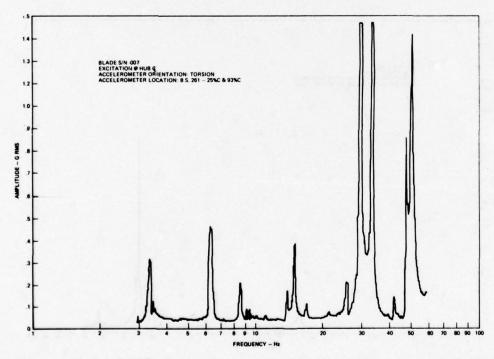


Figure C-8. MTS main rotor assembly dynamic response test.

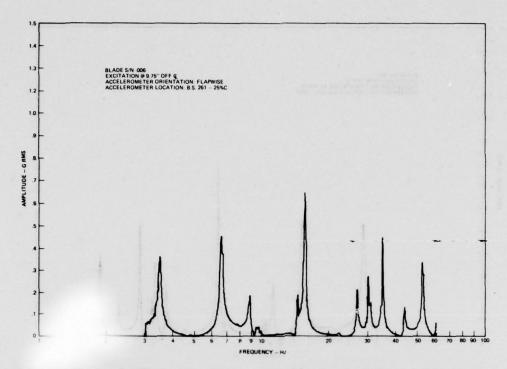


Figure C-9. MTS main rotor assembly dynamic response test.

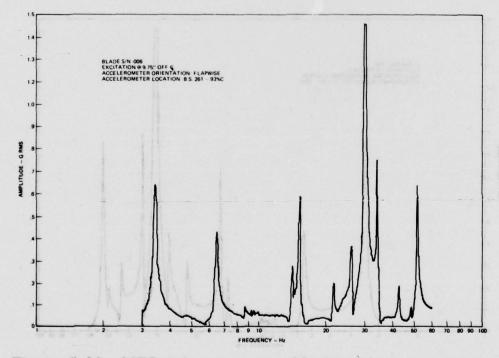


Figure C-10. MTS main rotor assembly dynamic response test.

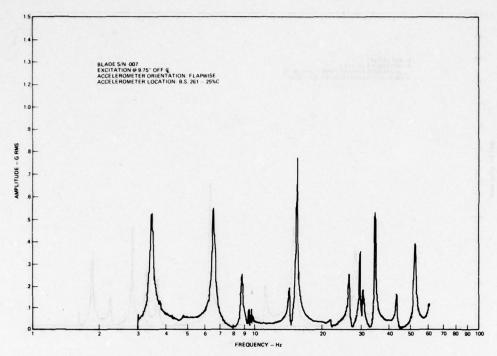


Figure C-11. MTS main rotor assembly dynamic response test.

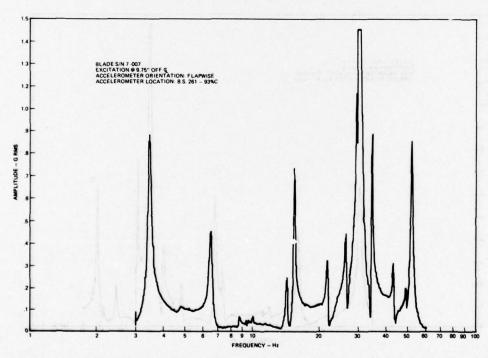


Figure C-12. MTS main rotor assembly dynamic response test.

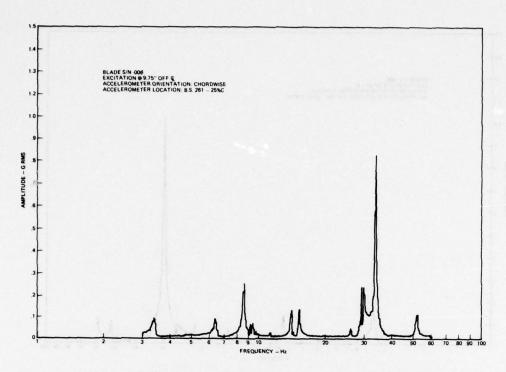


Figure C-13. MTS main rotor assembly dynamic response test.

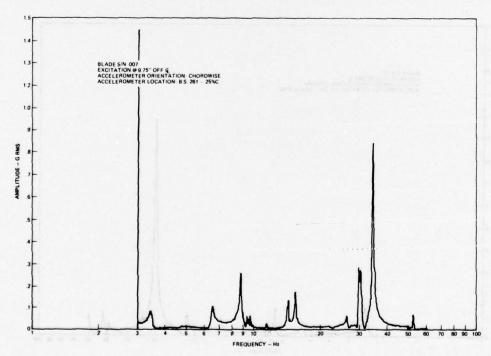


Figure C-14. MTS main rotor assembly dynamic response test.

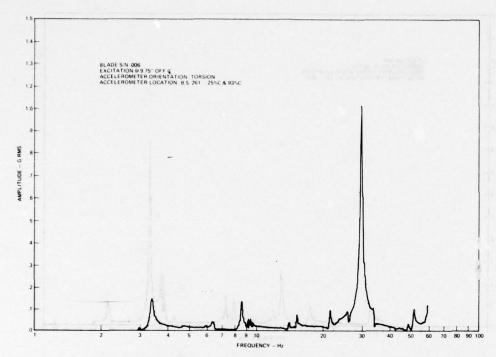


Figure C-15. MTS main rotor assembly dynamic response test.

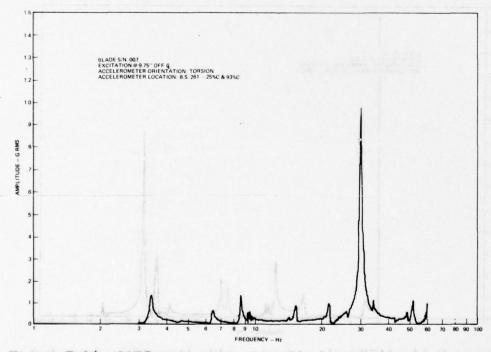


Figure C-16. MTS main rotor assembly dynamic response test.

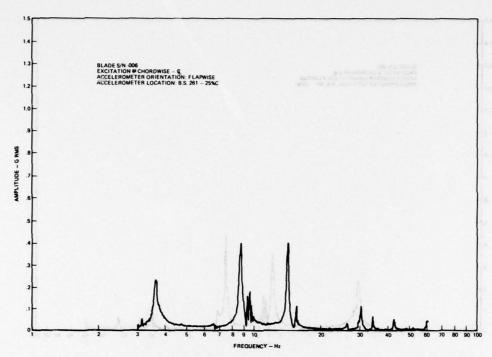


Figure C-17. MTS main rotor assembly dynamic response test.

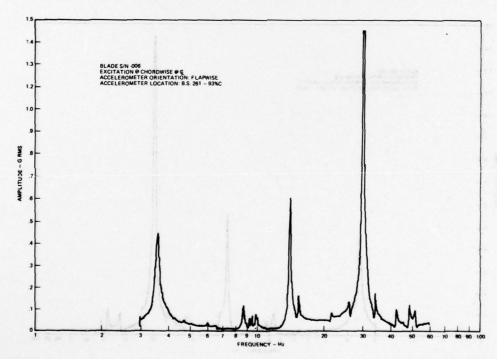


Figure C-18. MTS main rotor assembly dynamic response test.

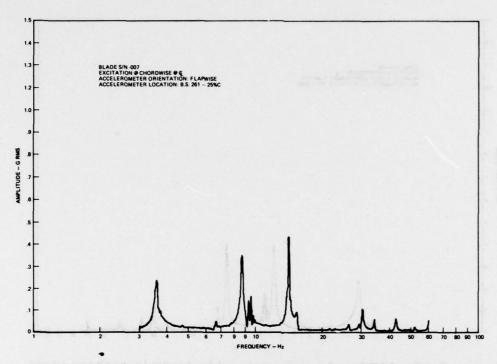


Figure C-19. MTS main rotor assembly dynamic response test.

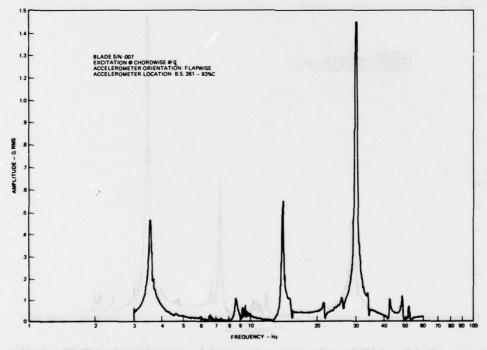


Figure C-20. MTS main rotor assembly dynamic response test.

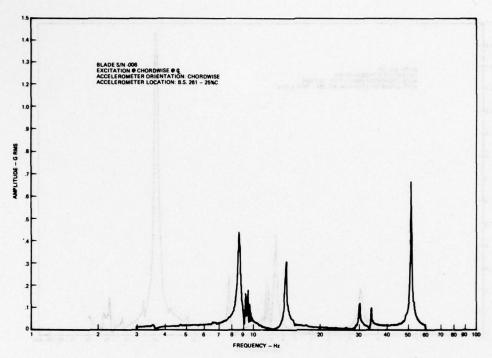


Figure C-21. MTS main rotor assembly dynamic response test.

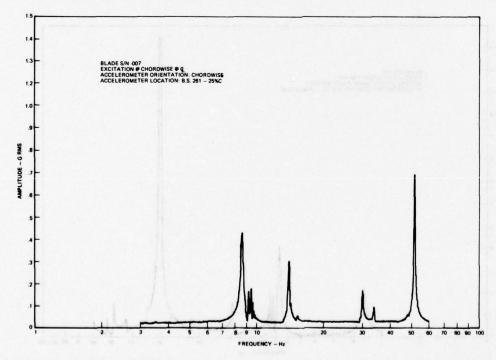


Figure C-22. MTS main rotor assembly dynamic response test.

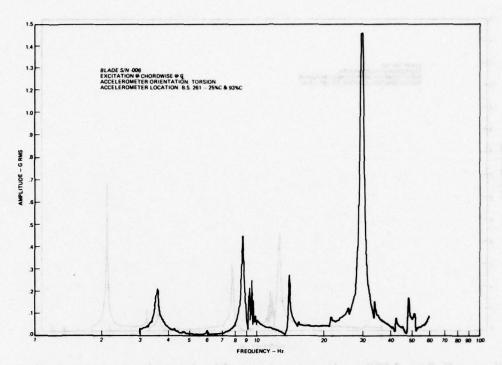


Figure C-23. MTS main rotor assembly dynamic response test.

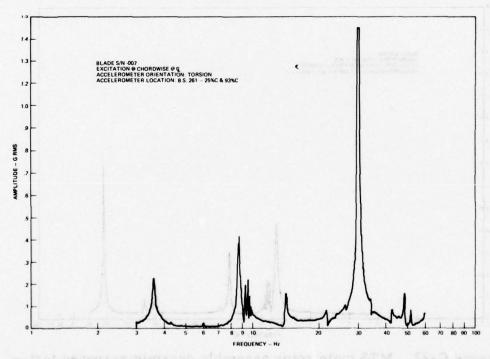


Figure C-24. MTS main rotor assembly dynamic response test.

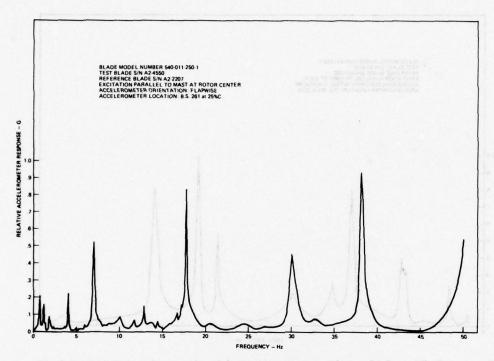


Figure C-25. 540 main rotor assembly dynamic response test.

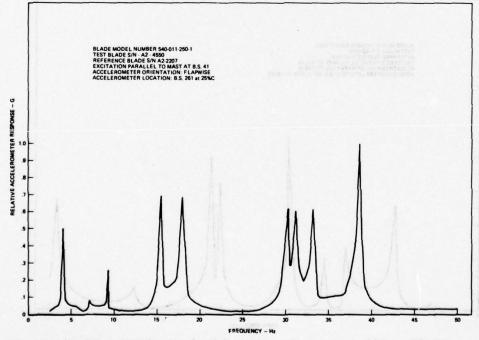


Figure C-26. 540 main rotor assembly dynamic response test.

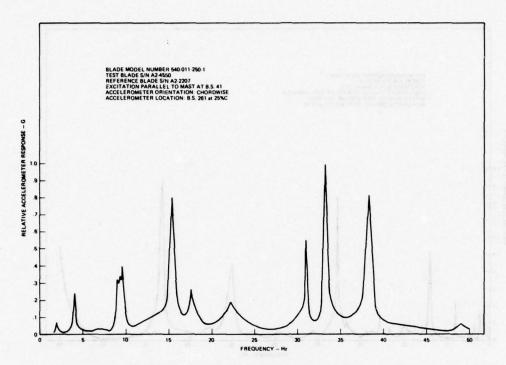


Figure C-27. 540 main rotor assembly dynamic response test.

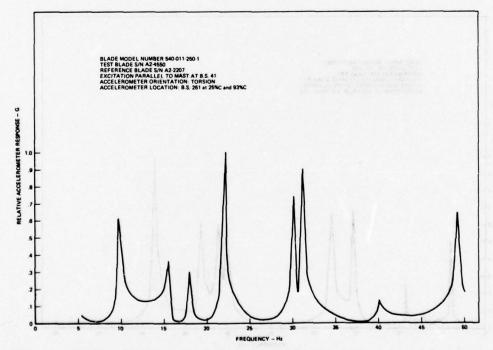


Figure C-28. 540 main rotor assembly dynamic response test.

APPENDIX D

SUPPLEMENTARY GROUND TEST DATA

TABLE D-1. GROUND TEST SCHEDULE

		Collective		Cyclic Pitch	Pulse	
Run Number	RPM	Pitch (percent)		Forward Longitudinal (percent)	Right Lateral (percent)	Time (minutes)
1	230	10	1	10 (1 second)#	10 (1 second)*	15
	280 290				155	
	294 300					
	305					
	310 315					
	320					
	324					
2	Run 1 RPM Schedule	0		10 (1 second)	10 (1 second)	21
3	294	0		10 (10 second)	10 (10 second)	17
	300 305 310					
	315					
	320 324					
4	Run 3 RPM Schedule	20		10 (10 second)	10 (10 second)	18
5	Run 3 RPM Schedule	40+		10 (10 second)	10 (10 second)	25
6	Run 3 RPM Schedule	0		20 (10 second)	20 (10 second)	19
	324	40		10 (10 second)	10 (10 second)	
7	Run 3 RPM Schedule			10 (10 second)	10 (10 second)	23
8	Run 3 RPM Schedule	20		20 (10 second)	20 (10 second)	24
9	Run 3 RPM Schedule	40		20 (10 second)	20 (10 second)	28
	324	20		20 (10 second)	20 (10 second)	

Beginning with Run Number 10, all runs were made at 324 rpm. Each run was broken into three segments:

- 20 percent ** of the run: collective pitch was held at 40 percent while 10 percent forward and 10 percent right cyclic pitch inputs were made for 10 seconds each. The cyclic inputs were made at 0 percent, 10 percent, and 20 percent time intervals. **
- 40 percent** of the run: collective pitch was held at 40 percent while 20 percent forward and right cyclic pitch inputs were made for 10 seconds each. The cyclic inputs were made at the 30, 40, 50, and 60 percent time intervals. **
- 20 percent** of the run: longitudinal and lateral cyclic pitch was held in neutral. Collective
 pitch was held at the 10, 0, 20, 30, 40, and 10 percent levels, each for 6 percent** of the
 run time.

Run Number		Time** (minutes)	
Manner		(minutes)	
10		66	
11		66	
12		20	
13		20	
14		22	
15		19	
10		36	
17		34	
18		66	
19		66	
	To	tal 605 minutes :	= 10.08 hours

Denotes length of time the cyclic control was held away from neutral.

^{*}Corresponds to maximum allowable engine torque.

Percentage figures refer to 100 percent being the total time of the specific ground run.

APPENDIX E

SUPPLEMENTARY FLIGHT TEST DATA; MTS BLADES - FORWARD CG CONDITION

TABLE E-1. FLIGHT TEST SCHEDULE, BASIC MTS BLADE PROGRAM

Flight Number	Time (hours)	RPM	Airspeed (knots)	SCAS	Collective	Lateral	Pedal	Longitudinal	Input
1	0.6	324	0	OFF	0	53	50	35-65	Slow
				OFF	0	53	50	35-65	10 second
				ON	0	53	50	35-65	10 secon step
				OFF	0	53	50	35-65	Slow
				OFF	0	53	50	35-65	10 secon
				ON	0	53	50	35-65	10 secon
				ON	Hover	- Feel Ou	ıt		
						- Feel Ou			
				OFF					
				ON	Forwa	rd Cyclic	Pulse 5	5%	
				OFF	Forwa	rd Cyclic	Pulse 5	5%	
		Pro-				1	est Cor	ditions	
2	0, 3	324	0		Tail Rot	or Track			
-		324	0		Pedal R				
			0			to Hover			
			0		Stable H				
		0-324	0			eep on G	round		
		324	0			to Hover		Marine Mark	
			0			Turn to R Turn to L			
			0-10		Acceler		cit, will	Table Toller	
			10		Level F				
			10-0		Deceler				
			0-20		Acceler				0
			20-0		Level F				
			0-10		Deceler Bight Si	ation deward A	ccelerat	ion	
			10			deward F		ton when you	
			10-0			deward D		tion	
			0-10			eward Ac		on	
			10			eward Fli			
			10-0			eward De		on	
			0			rd Accele	ration		
			10-0			rd Decele	ration		
			0			Landing			
		324-0	0		Shutdow				
3	0.2	324	0		Lift Off	to Hover			
			0		Stable H				
		0-324	0			eep on G	round		
		324	0			to Hover	inht 14	:14	
			0			Turn to R Turn to L			
			0-10		Acceler.		cit, Wil		
			10		Level F				
			10-0		Deceler			of soult be discoul	
			0-20		Acceler				
			20		Level F				
			20-0		Deceler	ation			

TABLE E-1 - Continued

Flight Number	Time (hours)	RPM	Airspeed (knots)	Test Conditions	Pilght 9
4	0, 3	324	0-10	Right Sideward Acceleration	1
			10	Right Sideward Flight	
			10-0		
			0-10		
			10	Dort Dido was a right	
			10-0	Left Sideward Deceleration	
			0-10	Rearward Acceleration	
			Ma a 10 contoaceay	Rearward Flight	
			10-0	Rearward Deceleration	
		224.0	0	Hover to Landing	
		324-0	0	Shutdown	
5	0.5	324	0-30	Acceleration	
	0.5	327	30	Level Flight	
			30-0	Deceleration	
			0-40	Acceleration	
			40	Level Flight	
			40-0	Deceleration	
			0-50	Acceleration	
			50	Level Flight	
			50-0	Deceleration	
			0-60	Acceleration	
			60	Level Flight	
			00.0	Deceleration	
			10	Tright - Indiana - Inghi	
			10-0		
			0-10		
			10	Left Sideward Flight Left Sideward Deceleration	
			0-10	Rearward Acceleration	
			10	Rearward Acceleration Rearward Flight	
			10-0	Rearward Deceleration	
			0	Hover to Landing	
		324-0	0	Shutdown	
6			0-70	Mild Acceleration	
		305 Just			
			70-0		
			0-80	Mild Acceleration	
			80-0		
			0-40		
			40	Level Flight	
			40-0		
			0-50	Moderate Acceleration	
			50		
			50-0 0-60		
			60 60-0	Level Flight Moderate Flare	
			0	Hover Left Turn, 30°/sec	
			0-60-0		
			1 1931 Solfrage that	Descent, Hover	
				27 954	
			the state of		

TABLE E-1 - Continued

Flight Number	Time (hours)	RPM	Airspeed (knots)	Test Conditions
7	0.6	324	0-70-0	Accelerate, Climb at 500 fpm, Autorotation Descent, Flare
			70	Climb
			80	Level Flight
			85	Level Flight
			70	1. 25g Left Turn
			70	1, 25g Right Turn
		324-294-324	70	Autorotation RPM Sweep
		324	70	Power Recovery
8	0.0	324	70	Climb at 1000 fpm
8	0.8	324	70	Level Flight
			85	Level Flight
			95	Level Flight
			105	Level Flight
			70	1.5g Left Turn
			70	1.5g Right Turn
			70	1. 25g Pullup
			85	1, 25g Left Turn
			85	1, 25g Right Turn
			70	One Ball Left Sideslip
			70	One Ball Right Sideslip
			70	Autorotation Entry
			70	Autorotation, 30° Bank, Left Turn
			70	Autorotation, 30° Bank, Right Turn
			75	Autorotation
			85	Autorotation
			85	Power Recovery
			85-0	Approach to Hover and Flare
9	1.1	324	0-10-0	Mild Acceleration and Flare
			0-20-0	Mild Acceleration and Flare
			0-40-0	Mild Acceleration and Flare
			0-10-0	Mild Acceleration and Flare to Right
			0-10-0	Mild Acceleration and Flare to Left
			0-10-0	Mild Acceleration and Flare Rearward
			0-40-0	Moderate Acceleration and Flare
			0	Hover Turn to Right, 30°/second
			0	Hover Turn to Left, 30°/second
			0-40-0	Maximum Acceleration and Flare
			0-60-0	Acceleration, 60-kts Climb, Power Descent
			0-70	Acceleration and Climb at 70 kts at 500 fpm
			70	Autorotation
			70	Power Recovery
			70-0	Land
			0-70	Acceleration and Climb at 1000 fpm
			85	Level Flight
			85	Autorotation
			85	Power Recovery
			85-0	Land
10	0.4	324	0-85	Acceleration, Climb at 85 kts at 500 fpm
		The Page 1	70	1. 25g Left Turn
			70	1. 25g Right Turn
		324-294-324	70	Autorotation RPM Sweep
		324	70	Power Recovery
		324	70-0	Land

TABLE E-1 - Continued

Flight Number	Time (hours)	RPM	Airspeed (knots)	Test Conditions	
11	1.8	324	0-85	Acceleration, Climb at 85 kts at 1000 fpm	
			95	Level Flight	
			105	Level Flight	
			70	Autorotation, 30° Left Turn	
			70	Autorotation, 30° Right Turn	
			60	Autorotation	
			60	Power Recovery	
			60-0	Land	
			70	Climb	
			70	1.5g Left Turn	
			70	1.5g Right Turn	
			70	1. 25g Pullup	
			70-0	Land	
			70	Climb	
			85	1. 25g Left Turn	
			85	1. 25g Right Turn	
			70		
			70	1/2-Ball Right Sideslip 1/2-Ball Left Sideslip	
			85		
			85	Autorotation	
			85-0	Power Recovery Land	
12	0.8	324	0-70	Acceleration, Climb at 70 kts at 1500 fpm	
	•••	30.	70	Level Flight	
			85	Level Flight	
			105		
				Level Flight	
			119	Level Flight	
			105	1. 25g Right Turn	
			105	1. 25g Left Turn	
			85	1.5g Right Turn	
			85	1.5g Left Turn	
			85	1. 25g Pullup	
			70	1.5g Pullup	
			70	Turn Reversal: 45° Right to 45° Left	
			70	Turn Reversal: 45° Left to 45° Right	
		294	85	Autorotation	
		324	85	Autorotation	
		339	85	Autorotation	
		324	0	Hover, ±10% Longitudinal Stick Reversal	
			0	Hover, ±10% Lateral Stick Reversal	
			0	Hover, ±10% Pedal Reversal	
13	0.9	324	85	Climb at 500 fpm	
			70	Level Flight	
			85	Level Flight	
			105	Level Flight	
			119	Level Flight	
			127	Level Flight	
			105	1. 25g Pullup	
			105	1.5g Right Turn	
			105	1.5g Left Turn	
			119	1. 25g Right Turn	
			119	1. 25g Left Turn	
			70	1.75g Right Turn	
			70	1.75g Left Turn	
			85	1.5g Pullup	
			85	Turn Reversal, 45° Right to 45° Left, Mild	
			85	Turn Reversal, 45° Left to 45° Right, Mild	
			105	Autorotation	
			85	I. 5g Right Turn	

TABLE E-1 - Continued

Flight Number	Time (hours) RF		irspeed knots)	Test Conditions
14	0.9 32	24	102	Climb at 500 fpm
			85	Climb at 1000 fpm
			70	Level Flight
			85	Level Flight
			105	Level Flight
			119	Level Flight
			127	Level Flight
			136	Level Flight
			127	1. 25g Right Turn
			127	1. 25g Left Turn
			119	1: 25g Pullup
			85	1/2-Ball Left Sideslip
			85	1/2-Ball Right Sideslip
			105	1.5g Pullup
			105	Lateral Reversal, Mild
			105	Longitudinal Reversal, Mild
			105	Pedal Reversal, Mild
			119	Lateral Reversal, Mild
			119	Longitudinal Reversal, Mild
			119	Pedal Reversal, Mild
15	1.0 32	24	85	Climb at 1500 fpm
			102	Climb at 1000 fpm
			119	Climb at 500 fpm
			70	Level Flight
			85	Level Flight
			105	Level Flight
			119	Level Flight
			127	Level Flight
			136	Level Flight
			136	1. 25g Right Turn
			136	1. 25g Left Turn
			127	1. 25g Pullup
			119	1.5g Right Turn
			119	1.5g Left Turn
			119	1.5g Pullup
			136	1/4-Ball Left Sideslip
			136	1/4-Ball Right Sideslip
			85	1 Ball Right Sideslip
			85	1 Ball Left Sideslip
16	0.5 32	24	0-136	Moderate Acceleration
			136	Climb at Maximum Power
			102	Climb at Maximum Power
			119	Climb at Maximum Power
			127	1,5g Right Turn
			127	1.5g Left Turn
			119	1.5g Pullup
			102	Turn Reversal, 45° Right to 45° Left, Mild
			102	Turn Reversal, 45° Left to 45° Right, Mild
			ALLEY TO	
			word of the last o	
			The same of the sa	

TABLE E-1 - Continued

Flight Number	Time (hours)	RPM	Airspeed (knots)	Test Conditions
17	0.3	324	0-136	Accelerate at Maximum Power
			105	Level Flight
			85	1.5g Right Turn
			85	1,75g Right Turn
			85	1.5g Left Turn
			85	1.75g Left Turn
			119	1.5g Right Turn
			119	1.75g Right Turn
			119	1.5g Left Turn
			119	1.75g Left Turn
			70	Climb at Maximum Power
			70	Pushover to 0.75g
			119	Turn Reversal, 45° Left to 45° Right, Mild
			119	
				Turn Reversal, 45° Right to 45° Left, Mild
			136	1.5g Left Turn
			127	1.5g Pullup
			119	Descent at Torquemeter = 20 psi
			119	Descent Pullup at 1.25g at Torquemeter = 20 ps
			119	Descent at Torquemeter = 10 psi
			119	Descent Pullup at 1, 25g at Torquemeter = 10 ps
			136-0	Approach with Moderate Flare
18	0.9	324	0-136	Accelerate at Maximum Power
			85	1.5g Right Turn
			85	1.75g Right Turn
			85	1.5g Left Turn
			85	1.75g Left Turn
			119	1.5g Right Turn
			119	1,75g Right Turn
			119	1.5g Left Turn
			119	1.75g Left Turn
			70	Climb at Maximum Power
			70	Pushover to 0,75g
			119	Turn Reversal, 45° Left to 45° Right, Mild
			119	Turn Reversal, 45° Right to 45° Left, Mild
			10/	1.5g Left Turn
		71.	136	1.5g Pullup
			119	Descent at Torquemeter = 20 psi
			119	Descent Pullup at 1, 25g at Torquemeter = 20 ps
			119	Descent at Torquemeter = 10 psi
			119	Descent Pullup at 1, 25g at Torquemeter = 10 ps
			136-0	Buildup to Quick Stop
19	0.9	324	0	Jump Takeoff Flat Pitch to 5 psi Over Hover Torque
			0	Jump Takeoff Light on Skids to 5 psi Over
				Hover Torque
			85	Level Flight
			105	Level Flight
			119	Level Flight
			127	Level Flight
			136	Level Flight
			119	Descent Pullup at 1.5g at Torquemeter = 20 psi
			85	1. 9g Right Turn
			85	1. 9g Left Turn
			119	1. 8g Right Turn
			119	1. 8g Left Turn
			105	
			105	1.8g Right Turn 1.8g Left Turn
			105	I OV Left Lurn

TABLE E -1 - Continued

Flight Number	Time (hours)	RPM	Airspeed (knots)	Test Conditions
19		324	136	Descent at Torquemeter = 20 psi
(cont.)			136	Descent Pullup at 1.25g at Torquemeter = 20 ps
			136	Turn Reversal, 45° Left to 45° Right, Mild
			136	Turn Reversal, 45° Right to 45° Left, Mild
			136	Climb at Maximum Power
			136	Pushover to 0.75g
20	0.9	324	0	Jump Takeoff Flat Pitch to Torquemeter = 50 psi
			105	Turn Reversal, 45° Left to 45° Right, Moderate
			105	Turn Reversal, 45° Right to 45° Left, Moderate
			136	Turn Reversal, 45° Left to 45° Right, Moderate
			136	Turn Reversal, 45° Right to 45° Left, Moderate
			136	1/4-Ball Right Sideslip
			136	1/2-Ball Right Sideslip
			136	1/2-Ball Right Sideslip
			136	•
				1/2-Ball Left Sideslip
			119	1.8g Left Turn
			65	Climb at Maximum Power
			65	Pushover to 0.5g
			136	Descent Pullup at 1.5g at Torquemeter = 20 psi
			119	Descent at Torquemeter = 20 psi
			119	45° Right Bank in Descent at Torquemeter = 20 psi
			119	45° Left Bank in Descent at Torquemeter = 20 p
			136	Descent at Torquemeter = 20 psi
			136	45° Right Bank in Descent at Torquemeter = 20 psi
			136	45° Left Bank in Descent at Torquemeter = 20 ps
			136-0	Quick Stop
			130-0	Quick Stop
21	0.7	324	0	Hover
			5	Right Sideward Flight
			10	Right Sideward Flight
			15	Right Sideward Flight
			20	Right Sideward Flight
			24	Right Sideward Flight
			0	Hover
			5	Left Sideward Flight
			10	Left Sideward Flight
			15	Left Sideward Flight
			20	Left Sideward Flight
			24	Left Sideward Flight
			0	Hover
			5	Rearward Flight
			10	Rearward Flight
			119	Right Rolling Pullup to 1.6g at Torquemeter =
			119	20 psi Left Rolling Pullup to 1.6g at Torquemeter =
			136	20 psi Right Rolling Pullup to 1.5g at Torquemeter =
			136	20 psi Left Rolling Pullup to 1,5g at Torquemeter =

This concludes the basic flight test program for the MTS Blades.

TABLE E-2. ALLOWABLE LOADS FOR AH-1G MAIN ROTORS WITH MTS AND 540 BLADES

End. 10 Hour Limit Allowable Allowable Allowable Allowable Load Load Load Limit Allowable Allowable Allowable Load Load Load Load Load Load Load Load			Allov	Allowable Loads		AH-1G	Maximum (Full	AH-1G Flight	Measured Loads Envelope)	Maximum /	Maximum Anticipated AH-1G Loa (Limited MTS Flight Envelope)(1)	Maximum Anticipated AH-1G Loads (Limited MTS Flight Envelope)(1)
M/R Blade Limit Allowable Allowable I.oad Flap Bend Sta 48 42400 45450 47230 57500 Flap Bend Sta 60 30400 32590 33870 40000 M/R Flap Bend Sta 110 13600 14580 15150 29220 M/R Flap Bend Sta 180 13600 14580 15150 20800 M/R Flap Bend Sta 180 13600 14580 15150 22070 M/R Flap Bend Sta 220 13600 14580 15150 22070 M/R Flap Bend Sta 220 13600 14580 15150 24910 M/R Ghord Bend Sta 88 113600 123300 135500 430000 M/R Blade (5) 13500 15500 47000 110000 M/R Blade (5) 15580 16700 17360 27720 M/R Brace Load 11800 12650 13150 - - M/R Brace Load 1580 3330 -	eas.	Measurement	End.	10 Hour	l Hour		Ma	Maneuver	Stabilized	Maneuver	uver	Stabilized
42400 45450 47230 57500 30400 32590 33870 40000 13600 14580 15150 29220 13600 14580 15150 22070 13600 14580 15150 22070 13600 14580 15150 24910 13600 123300 135500 428000 68170 73960 81330 428000 1580 16700 17360 27720 11800 12650 13150 - 5920(11) 6423 7063 -14189 1580 3330 - +4400 1580 - 7660			Limit ±	Allowable	Allowable		Max Load	Max Alt Load	Level Flt. Max Alt.	Max Load	Max Alt Load	Level Flt Max Alt.
30400 32590 33870 40000 13600 14580 15150 29220 13600 14580 15150 20800 13600 14580 15150 22070 13600 14580 15150 24910 13600 123300 135500 430000 68170 73960 81330 428000 15580 16700 17360 27720 11800 12650 13150 - 5920(11) 6423 7063 14189 1580 3330 - 44600 1580 3330 - 44600		4	42400	45450	47230	57500	46768	2730	5895 +23490	27720	1896 +23175	690 +13532
13600 14580 15150 29220 13600 14580 15150 20800 13600 14580 15150 22070 13600 14580 15150 24910 113600 123300 135500 430000 68170 73960 81330 428000 15580 16700 17360 27720 11800 12650 13150 - 6423 7063 +20518 5920 (11) 6423 7063 +4800 1580 3330 - +4400		9	30400	32590	33870	40000	-33500	- 2420 +31100	1034	30767	- 4496 +26271	- 2076 +10024
13600 14580 15150 20800 13600 14580 15150 22070 13600 14580 15150 24910 113600 123300 135500 430000 68170 73960 81330 428000 39400 42750 47000 110000 15580 16700 17360 27720 11800 12650 13150 - 5920 (11) 6423 7063 14189 1580 3330 - 7660 1580 3330 - 7660		00	13600	14580	15150	29220	-29220	- 4080 +20900	1483 ±11800	-17370	- 2779 +14590	- 74 + 7568
13600 14580 15150 22070 13600 14580 15150 24910 113600 123300 135500 430000 68170 73960 81330 428000 39400 42750 47000 110000 15580 16700 17360 27720 11800 12650 13150 - 5920 (11) 6423 7063 -14189 1580 3330 - + 44000		M/R Flap Bend Sta 110	13600	14580	15150	20800	-20800	- 3300 +15600	166 +	-14120	- 2402 +11318	- 1508 + 6701
13600 14580 15150 24910 113600 123300 135500 430000 68170 73960 81330 428030 39400 42750 47000 110030 15580 16700 17360 27720 11800 12650 13150 - 5920 (11) 6423 7063 -14189 1580 3330 - + 44000			13600	14580	15150	22070	-22070	- 6400 +15670	- 5416 + 7637	-20830	- 6420 +12400	- 3824 + 5313
113600 123300 135500 430000 68170 73960 81330 428030 39400 42750 47000 110030 15580 16700 17360 27720 11800 12650 13150 - 5920 (11) 6423 7063 -14189 1580 3330 - + 44000		1 ~		14580	15150	24910	-24910	- 8860 +15200	-10179 + 5521	-21048	- 8072 +12976	- 8843 + 3983
68170 73960 81330 428030 2 39400 42750 47000 110000 15580 16700 17360 27720 11800 12650 13150 - 5920 (11) 6423 7063 +20518 1580 3330 - +4400			113600	123300	135500	430000	339600 (4)	106000(4)	106220 (4) +69800	267800 (4)	118900(4) +97290	117700 (4)
39400 42750 47000 110000 15580 16700 17360 27720 11800 12650 13150 - 5920(11) 6423 7063 +20518 1580 3330 - +4400		d Bend Sta	68170	73960	81330	428030	279400	146400 +117200	162500	261100	162100+99000	158844 +36800
15580 16700 17360 27720 2 11800 12650 13150				42750	47000	110000	87240	31680 +43660	44190 +18810	76130	26540 +43660	44630 +17501
11800 12650 13150				16700	17360	27720	27720	6850 + 19830	2205 + 8127	19080	3786 +15290	2495 ± 4990
5920 (11) 6423 7063 +20518 1 1580 3330 - + 4400		M/R Blade Torsion Sta 180	11800	12650	13150	- 1	7		No Measured Loads	d Loads		Δ
1580 3330 - + 4400					7063	+20518	19124	5968 ± 8613	5981 ± 3930	15080	5700 ± 6307	6629 ± 2255
		M/R Pitch (1/rev)1b Link Axial Load		3330	•	+ 4400	4400	1087 ± 3148	± 1071	3028	601 ± 2427	396

TABLE E-2 - Continued

Moeasurement End, Limit Allowable Allowable Allowable Load Limit Limit Allowable Allowable Allowable Load Limit Limit Allowable Allowable Load Limit Limit Limit Limit Allowable Allowable Load Limit Limi	N sea	Harry See I	Allow	Allowable Loads	100	AH-1G	Maximun (Full	Maximum AH-1G Measured Loads (Full Flight Envelope)	sured Loads	Maximum (Limited	Anticipated MTS Flight	Maximum Anticipated AH-1G Loads (Limited MTS Flight Envelope)(1)
Limit	No.	Measurement	End.	10 Hour	1 Hour	Limit	Man	euver	Stabilized	Man	euver	Stabilized
See Note (3) See Note (3) See Note (3) See Note (3) T1987 -35186		ACTION OF THE PARTY OF THE PART	Limit ±	Allowable	Allowable	Load	Max. Load	Max. Alt. Load	Level Fit. Max Alt.	Max. Load	Max. Alt. Load	Level Flt. Max Alt.
See Note (3) See Note (3)		M/R Yoke Flap Bend Sta 4.8	4.258.0			71987	-35186	3419 +16239	-15112 + 7583	22364	3777 +11897	-21209
36000 41000 6700030490 - 452 - 640 -30490 - 3452		M/R Yoke Chord Bend Sta 5.8	See	Note (3)	eriodis.	441600	314700	58443 +175300	121947 +82243	238770	93006 +145760	82242 +48211
36000		M/R Drive Shaft(7) Bending Moment - 0° (in line with blade)	100			grade s	-30490	- 452 + 30040	- 640 +11830		- 452 + 30040	-1544
This component is not a fatigue Use Interaction - 215550		M/R Drive Shaft Bending Moment -900 (7)	36000 psi	41000 psi	67000 psi		-30590	- 153 + 30170	- 320 +11550	-30590	- 908	- 310 +10530
ccelera- Equation C 3.224		M/R Drive Shaft Torque 2/rev					215550	40030 + 38980	97882 + 6247	200970	40030 +38980	97882 + 6247
This component is not a fatigue 19067 + 110437 + 2502 + 2508 + 2014 + 2024 + 2018 + 2018 + 2018 + 2018 + 2018 + 2018 + 2018 + 2018 + 2018 + 2018 + 2018		Vertical Acceleration at C.G. 2/rev g's	Equa	tion C		0.00	3, 224	2.21 + 1.014	1. 033	2.591	2.068	1. 022 ±0. 309
This component is not a fatigue 19067 + 10437 6875 15880 + 5586 15880 + 5054			1621	2400	3700	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	- 4125		X 1	- 3231	- 1207 + 2024	- 369 + 642
		Lift Link 2/rev lb	This c limite	component is d life part.	not a fatig	en.	19067	-	6875 + 2378	15880	5586 + 5054	6837 + 1479

TABLE E-2 - Continued

General Notes

A load frequency of one/rev is assumed for all blades and rotating controls.

A load frequency of two/rev is assumed for main rotor drive shaft torque, vertical acceleration, lateral boost actuator, and lift link.

Positive flapwise bending denotes tension in lower side of blades, positive chordwise bending denotes tension in leading edge of blade, and positive axial load denotes tension.

Specific Notes

- (1) Loads are within the flight envelope for the MTS blades, which is limited in speed and load factor to 80 percent of the AH-1G flight envelope, and to a gross weight of 8500 ± 200 pounds.
- (2) Endurance limit is based on blade failure. The drag brace load is used in interaction equation A to establish the life of the main rotor grip.
- (3) Measured loads are used in interaction equations A and B to establish the life of the main rotor grip and yoke extension, respectively.
- (4) Measured load = 17.76 x measured drag brace load.
- (5) Based on pitch link load.
- (6) Measured loads are from Station 210.
- (7) Measured loads are adjusted for HH location of the bending gages (different from Bell).

TABLE E-3. 540 ROTOR HUB LOAD INTERACTION EQUATIONS

INTERACTION EQUATION A (MAIN ROTOR GRIP)

 $f_{ALT} = 0.01646 M_{F_{4.8}} + 0.08514 M_{F_{48}} + 0.2667 P_{DB}$

where:

f_{ALT} = Alternating Stress - PSI

M_F = Alternating Flapwise Moment - in-lb

PDB = Alternating Drag Brace Load - lb

Allowables (PSI)

324 RPM and 1/Rev Load Frequency Assumed

	Endurance		
	Limit	10 Hour Allowable	l Hour Allowable
	Tanpa marc	Allowable	has I I I I I I I I I I I I I I I I I I I
fALT	6250	7700	14000

INTERACTION EQUATION B (MAIN ROTOR YOKE EXTENSION)

$$f_{ALT} = 0.809 M_{F_{4.8}} + 0.274 M_{F_{48}} + 0.0313 M_{C_{5.8}} + 0.00968 M_{C_{48}}$$

where:

Mc = Alternating Chord Moment - in-lb

 M_{F} = Alternating Flapwise Moment - in-lb

TABLE E-3 - Continued

Allowables (PSI)

324 RPM and 1/Rev Load Frequency Assumed

1 Hour
Allowable
42500

INTERACTION EQUATION C (MAIN ROTOR MAST)

$$f_{ALT} = [(2498 N_V + 0.9601 M_R)^2 + 0.126 (TOR)^2]^{1/2}$$

where:

fALT = Alternating Stress - PSI

 N_{V} = Alternating Vertical Load Factor $\sim g$

M_R = The resultant of parallel and perpendicular alternating bending moments. in-lb

TOR = Alternating Mast Torsion Load ~ in-lb

AH-1G S/N 67-15683 HUGHES HELICOPTERS MULTI-TUBULAR SPAR ROTOR BLADES TABLE E-4.

98	4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.
MEAN.	######################################
TEST CONDITION	TURN REVERSAL, NOD 136 KIRS FYA CONT. REVERSAL 119 KIRS PLLLIP. LEVE. R. IGHT - 98 KIRS PLLLIP. LEVE. R. IGHT - 136 KIRS STAB. ALTO, 324 RRH - 98 KIRS STAB. ALTO, 339 RRH - 98 KIRS ALTO TURN. REGULEY - 78 KIRS ALTO TURN. REGULEY - 78 KIRS ALTO TURN. LEFT - 78 KIRS ALTO TURN. LEFT - 78 KIRS ALTO TURN. LEFT - 98 KIRS RIGHT SIDES. IP - 78 KIRS RIGHT SIDES. IP - 78 KIRS BLOWE. STEADY - 135 KIRS BLOWE. IT. TURN PULLUP - 119 KIRS BLOWE. THE AND THE PURBURANT - 110 KIRS BLOWE. THE AND THE PURBURANT - 110 KIRS BLOWE. THE AND THE PURBURANT - 110 KIRS BLOWE. STEADY - 136
ġ	୴ୡଌଞ୍ଜଳନ୍ତ ଅନ୍ତର୍ ଅନ୍ତର ଅନ
	######################################
MBAN.	%%%%%%%%% %%%%%% %%%% %%% %% %% %% %
NO. TEST CONDITION	1. NORPEL START 0-100% NR 2. NORPEL START 0-100% NR 3. NORPEL TAKEDEF 5. HOURE TURN, LEFT 30 DEG-SEC 6. HOURE TURN, LEFT 30 DEG-SEC 7. HOURE, LAT REUERSAL 11. SIDEJARD R. IGHT - LEFT 12. SIDEJARD R. IGHT - LEFT 13. SEGRENARD R. IGHT - LEFT 14. LEVEL R. IGHT - 119 KIRS 15. LEVEL R. IGHT - 119 KIRS 16. LEVEL R. IGHT - 119 KIRS 17. LEVEL R. IGHT - 126 KIRS 18. LEVEL R. IGHT - 136 KIRS 19. LEVEL R. IGHT - 136 KIRS 22. CLINB, 1500 FFM - 70 KIRS 23. CLINB, 1500 FFM - 70 KIRS 24. CLINB, 1500 FFM - 105 KIRS 25. CLINB, 1500 FFM - 105 KIRS 26. CLINB, 1500 FFM - 105 KIRS 27. CLINB, 1500 FFM - 105 KIRS 28. CLINB, 1500 FFM - 105 KIRS 29. CLINB, 1600 FFM - 105 KIRS 20. CLINB, 1600 FFM -
	TEST CONDITION MEAN. OSC. NO. TEST CONDITION MEAN.

TABLE E-4 - Continued

+-57500.	980.	######################################
C LIMITS	MERN.	ĸĸijĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸ
STATIC		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
42400.	2	2
LIMIT	TEST CONDITION	28. 28. 28. 28. 28. 28. 28. 28. 28. 28.
ENDURANCE	TEST	PULLIP RECENT RE
INLB	Š	፞ ਸ਼ੑਲ਼ਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑਲ਼ੑ
4000 FT	.090	284 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
STA. 48 IN HD-	MERN.	\$8831144168118888888881188818888888888888
DE FLAP BENDING @	CONDITION	1989 NR
M.R. BLADE DGN- 8476 L		STRATE 0-1 TAKEDIEF F. TAKEDIEF F. TURN, LEFT - 1 TO F. LIGHT
F	TEST	2
PARAMETER	ġ	

TABLE E-4 - Continued

+-40000.	.3SC	23157-115911-17-17-17-17-17-17-17-17-17-17-17-17-1
STATIC LIMITS	MEAN.	######################################
IN-LB ENDURANCE LIMIT 30400. STATIC	NO. TEST CONDITION	51. TURN REVERSAL, MDD 136 KIRS 52. LAT. CONT. REVERSAL - 119 KIRS 53. LAT. CONT. REVERSAL - 119 KIRS 54. DIR. CONT. REVERSAL - 119 KIRS 55. FULLUP, LEVER FIGHT - 85 KIRS 56. FULLUP, LEVER FIGHT - 85 KIRS 57. FULLUP, LEVER FIGHT - 135 KIRS 58. FULLUP, LEVER FIGHT - 135 KIRS 59. PULLUP, LEVER FIGHT - 136 KIRS 60. AUTO PULL FIGHT - 127 KIRS 61. STAB. AUTO. 324 RPH - 85 KIRS 62. STAB. AUTO. 324 RPH - 85 KIRS 63. STAB. AUTO. 324 RPH - 85 KIRS 64. STAB. AUTO. 324 RPH - 85 KIRS 65. STAB. AUTO. 324 RPH - 85 KIRS 66. STAB. AUTO. 324 RPH - 85 KIRS 67. AUTO TURN, RECOURY 70. LEFT SIDES.LIP - 70 KIRS 71. LEFT SIDES.LIP - 70 KIRS 72. LEFT SIDES.LIP - 85 KIRS 73. LEFT SIDES.LIP - 95 KIRS 74. RIGHT SIDES.LIP - 95 KIRS 75. RIGHT SIDES.LIP - 95 KIRS 76. DIVE, RIGHT TURN - 119 KIRS 77. DIVE, STEBOY - 136 KIRS 78. DIVE, RIGHT TURN - 119 KIRS 88. DIVE, LET TURN FULLUP - 119 KIRS 89. DIVE, LET TURN FULLUP - 136 KIRS 89. DIVE, LT TURN FULLUP - 136 KIRS 89. DIVE, LT TURN FULLUP - 136 KIRS 89. CLIMB. MOX. RATE, PUSHOURR - 65 99. CLIMB. MOX. R
4000 FT	.080	699 199 199 199 199 199 199 199
STA.66 IN HD=	MEAN.	7. 28. 28. 28. 28. 28. 28. 28. 28. 28. 28
PARAMETER M.R. BLADE FLAP BENDING @ 192.4	NO. TEST CONDITION	1. NORTH, STORT 0-1000; NR 2. NORTH, STORT 0-1000; NR 3. NORTH, TAKEOFF 5. HOVER TURN, LEFT 30 DE5-SEC 6. HOVER TURN, RIGHT 30 DE5-SEC 10. HOVER TURN, RIGHT 30 DE5-SEC 11. SIDEJARD R. IGHT - LEFT 12. SIDEJARD R. IGHT - LEFT 13. SIDEJARD R. IGHT - LEFT 14. LEVE R. IGHT - REVIESSAL 15. LEVE R. IGHT - 105 KIRS 15. LEVE R. IGHT - 105 KIRS 16. LEVE R. IGHT - 105 KIRS 17. LEVE R. IGHT - 105 KIRS 18. LEVE R. IGHT - 105 KIRS 19. LEVE R. IGHT - 105 KIRS 19. LEVE R. IGHT - 105 KIRS 20. CLIMB 1000 FPH - 70 KIRS 21. CLIMB 1000 FPH - 70 KIRS 22. CLIMB 1000 FPH - 70 KIRS 23. CLIMB 1000 FPH - 85 KIRS 24. CLIMB 1000 FPH - 85 KIRS 25. CLIMB 1000 FPH - 85 KIRS 26. CLIMB 1000 FPH - 85 KIRS 27. CLIMB 1000 FPH - 105 KIRS 28. CLIMB 1000 FPH - 105 KIRS 29. CLIMB 1000 FPH - 105 KIRS 20. LIMB 1000 FPH - 1000

TABLE E-4 - Continued

+-29220.	980.	4.658.866.666.666.666.666.666.666.666.666
STRTIC LIMITS	MEAN.	### ##################################
ENDURANCE LIMIT 13600. STATIC	TEST CONDITION	TURN REVERSAL. 119 KIRS PAR CONT. REVERSAL. 119 KIRS DIR. CONT. REVERSAL. 119 KIRS PULLUP. LEVIE F. LIGHT - 78 KIRS PULLUP. LEVIE F. LIGHT - 105 KIRS PULLUP. LEVIE F. LIGHT - 177 KIRS PULLUP. LEVIE F. LIGHT - 177 KIRS PULLUP. LEVIE F. LIGHT - 177 KIRS STARB. AUTO. 324 RPH - 38 KIRS STARB. AUTO. 324 RPH - 165 KIRS AUTO. DURN. LEFT - 70 KIRS AUTO. DURN. LEFT - 70 KIRS RIGHT SIDES. IP - 78 KIRS RIGHT SIDES. IP - 78 KIRS BULLET SIDES. IP - 136 KIRS DUUE. STERDY - 136 KIRS DUUE. STERDY - 136 KIRS DUUE. STERDY - 136 KIRS DUUE. LEFT TURN - 136 KIRS DUUE. STERDY - 136 KIRS DUUE. LEFT TURN - 136 KIRS DUUE. LEFT TURN - 136 KIRS DUUE. RT. TURN PULLUP - 136 KIRS CLIMB. PAX. RATE. PUSHOUR- 66 CLIMB. PAX. RATE. PUSHOUR- 67 CLI
INTE	ż	<u>ჃႷႷႯႯႯႯႯႷჄჅჄჅჇჅჅჇჅႷჇჇჇჇჇჇჇჇჇჇჇჇჇჇჇჇჇჇჇჇჇჇ</u>
JA 1000 FT	.080	8.14.9.14.9.9.14.9.9.19.9.9.9.9.9.9.9.9.9
STR. 85	MER.	C44 0200044666666666666666666666666666666
PORPUETER H.R. BLADE FLAP BENDING 6 : 192.4	NO. TEST CONDITION	1 NOBYL START 6-100% NR 5 NOBYL START 6-100% NR 5 NOBYL TAKEDET 7 NOBYL TAKEDET 7 NOBYL TAKEDET 7 NOBYL TAKEDET 8 NOBYL TAKEDET 10 NOBYL TAKEDET 10 NOBYL TAKEDET 10 NOBYL TAKEDET 10 NOBYL TAKEDET 11 SIDELARD R. LEFT 12 SIDELARD R. LEFT 13 NOBYL TAKEDET 14 NOBYL TAKEDET 15 SIDELARD R. LEFT 16 NOBYL TAKEDET 16 NOBYL TAKEDET 16 NOBYL TAKEDET 17 LEVER R. LIGHT 18 SIDELARD R. LIGHT 18 SEA KIRS 18 CLINB, 1500 FFM 19 KIRS 19 CLINB, 1500 FFM 19 KIRS 10 CLINB, 1500 FFM 10 10 CLIN
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	+-20800.	08C	7. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3.
	STRIIC LIMITS	MEAN.	86446446488846468888888488848888888888
	IN-LB ENDURANCE LIMIT 13600. STATIC	NO. TEST CONDITION	\$1. TURN REVERSAL, MOD 136 KIRS \$2. F.A CONT. REVERSAL - 119 KIRS \$3. DIR. CONT. REVERSAL - 119 KIRS \$4. DIR. CONT. REVERSAL - 119 KIRS \$5. PULLUP, LEVEL R. LIGHT - 86 KIRS \$5. PULLUP, LEVEL R. LIGHT - 195 KIRS \$5. PULLUP, LEVEL R. LIGHT - 195 KIRS \$6. PULLUP, DIVE - 136 KIRS \$6. PULLUP, DIVE - 136 KIRS \$6. PULLUP, DIVE - 136 KIRS \$6. STAB. AUTO, 324 RPH - 195 KIRS \$6. STAB. AUTO, 324 RPH - 195 KIRS \$6. STAB. AUTO, 324 RPH - 195 KIRS \$6. STAB. AUTO, 324 RPH - 85 KIRS \$6. STAB. AUTO, 324 RPH - 85 KIRS \$6. STAB. AUTO, 339 RPH - 85 KIRS \$6. STAB. AUTO, 339 RPH - 85 KIRS \$6. STAB. AUTO, 339 RPH - 85 KIRS \$6. STAB. AUTO, 124 RPH - 136 KIRS \$7. LEFT SIDES.LIP - 76 KIRS \$7. LEFT SIDES.LIP - 76 KIRS \$7. LEFT SIDES.LIP - 76 KIRS \$7. RIGHT SIDES.LIP - 136 KIRS \$7. RIGHT S
-	4000 FT	.080	######################################
:	STR.110 IN HD=	MEAN.	864823000044004664480000000000000000000000000
	PARAMETER M.R. BLADE FLAP BENDING @ S TOGA = 8476 LB TOCG = 192.4	NO. TEST CONDITION	1. NORTH STRRT 0-100% NR 2. NORTH STRRT 0-100% NR 3. NORTH STRRT 0-100% NR 5. HOUR TURN, LEFT 30 DEG-SEC 6. HOUR TURN, LEFT 30 DEG-SEC 10. HOUR TURN, LEFT 30 DEG-SEC 11. SIDEJARD R. IGHT - LEFT 12. SIDEJARD R. IGHT - LEFT 13. REARRARD R. IGHT - LEFT 14. LEVE R. FLIGHT - 119 KIRS 15. LEVE R. FLIGHT - 102 KIRS 16. LEVE R. FLIGHT - 103 KIRS 17. LEVE R. IGHT - 119 KIRS 18. LEVE R. IGHT - 126 KIRS 19. LEVE R. IGHT - 126 KIRS 22. CLINB, 1000 FPM - 70 KIRS 23. CLINB, 1000 FPM - 70 KIRS 24. LINB, 1000 FPM - 1005 KIRS 25. CLINB, 1000 FPM - 1005 KIRS 26. LINB, 1000 FPM - 1005 KIRS 27. CLINB, 1000 FPM - 1005 KIRS 28. CLINB, 1000 FPM - 1005 KIRS 29. CLINB, 1000 FPM - 1005 KIRS 29. CLINB, 1000 FPM - 1005 KIRS 29. CLINB, 1000 FPM - 1005 KIRS 20. CLINB, 1000 FPM - 1005 KIRS 20. LINB, 1000 FPM - 1000 FPM - 1005 KIRS 20. LINB, 1000 FPM - 1000 FPM - 1005 KIRS 20. LINB, 1000 FPM - 1000 FPM

TABLE E-4 - Continued

+-22070.	OSC.	\$\$\$\$4.44\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
STATIC LIMITS	MEAN.	
		28
T 13600.	NITION	200
ENDURANCE LIMIT	TEST CONDITION	TURN REVERSAL, MDD. – 136 KIL FAC CONT. REVERSAL – 119 KIR DIR. CONT. REVERSAL – 119 KIR PULLUP, LEVEL F. 16HT – 70 KIR PULLUP, LEVEL F. 16HT – 105 KIR PULLUP, LEVEL F. 16HT – 105 KIR PULLUP, LEVEL F. 16HT – 105 KIR PULLUP, LEVEL F. 16HT – 127 KIR PULLUP, DIVE – 136 KIRS STAB. AUTO. 324 RPM – 105 KIRS STAB. AUTO. 324 RPM – 136 KIRS EET SIDESLIP – 70 KIRS STAB. STAB. – 136 KIRS DIVE. STEEDY – 136 KIRS DIVE. STEEDY – 136 KIRS DIVE. LEFT TURN – 119 KIRS DIVE. LEFT TURN – 119 KIRS DIVE. LEFT TURN – 119 KIRS DIVE. LETT TURN PULLUP – 119 K DIVE. KIRT TURN ROLLUP – 119 K DIVER ROL
	E	2.898898889283732328585555598938748757732855555555555555555555555555555555
S IN-LB	Ž	ℴ℀ⅆ℧ⅆⅆⅆⅆⅆ ⅆⅆ℧℧ⅅⅆ⅄℈⅂⅂⅂⅂⅂⅂ⅆℴ℧ⅆⅆⅆⅆⅆⅆⅆⅆⅆⅆⅆⅆⅆⅆⅆⅆⅆⅆⅆⅆ
UNITS 4000 FT	.090	### ##################################
STA. 185 IN HD= 4000	MEAN.	### ### ### ### ### ### ### ### ### ##
M.R. BLADE FLAP BENDING @ TOGN= 8476 LB TOCG= 192.4	CONDITION	100% NR 100 -0% 100 10
PARAMETER M.R. BL TOGIJ= 847	TEST CON	NORMAL START 0-100% NP NORMAL START 0-100% NP NORMAL STAREDFF JUMP TAKEDFF HOUER 162 324 RAH HOUER 162 324 RAH HOUER 102 324 RAH HOUER 102 324 RAH HOUER 103 324 RAH HOUER 103 132 BEG-SE HOUER 103 132 BEG-SE HOUER 103 132 RAH STARED FILIAT - LEFT EVEL FILIAT - 102 KIRS LEVEL FILIAT - 103 KIRS LEVEL FILIAT - 103 KIRS LEVEL FILIAT - 103 KIRS LINE 1000 FPH - 70 KIRS LINE 1000 FPH - 35 KIRS CLINB 1000 FPH - 105 KIRS CLINB 1000 FPH - 100 FPH - 100 KIRS CLINB 1000 FPH - 100 FPH - 1
PAIRA	£	ਜ਼ੑਗ਼ੑਜ਼ੑ ਫ਼ਲ਼ਫ਼ਫ਼ਜ਼ੵਜ਼ੑਜ਼ੑਫ਼ੑਜ਼ੑਜ਼ੑਫ਼ੑਜ਼ੑਜ਼ੑਜ਼ੑਖ਼ੑਜ਼ੑਜ਼ੑਜ਼ੑਜ਼ੑਜ਼ੑਜ਼ੑਜ਼ੑਜ਼ੑਜ਼ੑਜ਼ੑ

TABLE E-4 - Continued

+-24910.	OSC.	980 100 100 100 100 100 100 100 100 100 1	### ### ##############################	
STATIC LIMITS	MEAN.	6.00 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
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13600.	101.	00-1-119 00-1-119 00-1-119 00-1-119 00-1-119 00-1-119 00-1-119	1988 1988	
E LIMIT	TEST CONDITION	REAL, MO REVERSE REVERSE SUBL FLI SUBL	20000000000000000000000000000000000000	
ENDURANCE LIMIT	TES	URN REVERSA 174 CONT. RE 21LLP. LEVE 21LLP. LEVE 21LLP. LEVE 21LLP. LEVE 21LLP. LEVE 21LLP. LEVE 21LLP. LEVE 21LLP. LEVE 21LLP. DIVE	80100000000000000000000000000000000000	
IN-LB	Š		෬ඁ෭෫ඁ෭෬ඁ෬ඁ෫෧ඁ෬෫෫෦෬ඁ෫෫෦෬෫෫෧෫෧෫෧෪෧෪෧෪෧෧෧෧෫෫ ෦෬ඁ෭෫෬ඁ෬ඁ෫෧ඁ෫෧෫෦෬෦෫෫෦෬෫෫෧෫෧෫෧෪෧෪෧෪෧෧෧෧෧෫෫	
P. FT	USC	2578 1394. 3266. 3257. 3257. 3477. 4616.	84847488888888888888888888888888888888	8213.
5= 4000	÷	~#.id#.	چېرونو د ښېرونو چې د و ورونو د و ورونو و د و ورونو و و و و و و و و و و و و و و و و	ທ່
STA. 220 IN HD= 400	MEAN.	44.137. 2.883. 2.883. 2.883. 2.833. 2.437. 2.437.	24 44 44 44 44 44 44 44 44 44 44 44 44 4	-5575.
@ STA. 220 4 IN HD=	MEAN.	7	RS RS RIPS RIPS RIPS RIPS RIPS RIPS RIPS	105 KIAS -5575.
@ STA. 220 4 IN HD=		100-0%. NR. 100-0%. NR. 130 DEG-SEC. 130 DEG-SEC. 130 DEG-SEC. 150-150-150-150-150-150-150-150-150-150-	85 KIRS 102 KIRS 113 KIRS 113 KIRS 113 KIRS 124 KIRS 126 KIRS 125 KIRS 125 KIRS 126 KIRS 126 KIRS 126 KIRS 126 KIRS 127 KIRS 128 KIR	MGD 105 KIAS -5575.
@ STA. 220 4 IN HD=	CONDITION	100-0%. NR. 100-0%. NR. 130 DEG-SEC. 130 DEG-SEC. 130 DEG-SEC. 150-150-150-150-150-150-150-150-150-150-	85 KIRS 102 KIRS 113 KIRS 113 KIRS 113 KIRS 124 KIRS 126 KIRS 125 KIRS 125 KIRS 126 KIRS 126 KIRS 126 KIRS 126 KIRS 127 KIRS 128 KIR	JEKSAL, MGD 105 KIAS -5575.
M.R. BLADE FLAP BENDING @ STA.220 TOGA+ 8476 LB TOCG* 192.4 IN HD=		DRYAL START 0-100% NR DRYAL SHUDDAN 100-0% DRYAL TAKEDEF -4137 UNER TURN, RIGHT 30 DEG-SEC -3603 OUER TURN, LEFT 30 DEG-SEC -3603 OUER, FYA REVERSAL -2818 OUER, DIR. REVERSAL -3777 DEG-RED F. 1647 -3537 OUER, DIR. REVERSAL -3777 -2447	F. Gert	REVERSAL, MGD 105 KIAS
@ STA. 220 4 IN HD=	CONDITION	NORTHAL START 0-100% NR. NORTHAL SHUTDOLN 100-0%. NORTHAL THEOFF. HOUER LGE 324 RPH HOUER TURN, LEFT 30 DEG-SEC HOUER FOR REVERSAL HOUER, F/A REVERSAL HOUER, DIR. REVERSAL HOUER, DIR. REVERSAL HOUER, DIR. REVERSAL SIDBLARD R. IGHT - LEFT SIDBLARD R. IGHT - LEFT	L F. 1647 - 76 KIAS L F. 1647 - 85 KIAS L F. 1647 - 102 KIAS L F. 1647 - 102 KIAS L F. 1647 - 127 KIAS L F. 1647 - 127 KIAS L F. 1647 - 126 KIAS L F. 1647 - 126 KIAS B. 1500 FPM - 70 KIAS B. 1500 FPM - 85 KIAS B. 1500 FPM - 105 KIAS B. 1500 FPM - 105 KIAS B. 1500 FPM - 110 KIAS B. 1600 FPM - 110 KIAS B. 160 KIAS LURY, 26 KIAS LURY, 26 KIAS LURY, 125 KIAS LURY, 125 KIAS LURY, 135 KIAS LURY, 136 KIAS REVERSAL, MILD - 126 KIAS REVERSAL, MILD - 126 KIAS REVERSAL, MILD - 136 KIAS REVERSAL, MILD - 136 KIAS	TURN REVERSAL, MGD 105 KIRS

TABLE E-4 - Continued

+-441000.	OSC.	11 65,50 65,60 65,
STATIC LIMITS	MEGN.	2000 100 100 100 100 100 100 100 100 100
IN-LB ENDURANCE LIMIT 71549. STATI	NO. TEST CONDITION	51. TURN NEVERSAL, MDD 136 KIAS 52. LAT. CONT. REDEESAL - 119 KIAS 53. LAT. CONT. REDEESAL - 119 KIAS 54. DIR. CONT. REDEESAL - 119 KIAS 55. PULLUP, LEVER, FIIGHT - 105 KIAS 56. PULLUP, LEVER, FIIGHT - 105 KIAS 57. PULLUP, LEVER, FIIGHT - 127 KIAS 58. PULLUP, LEVER, FIIGHT - 127 KIAS 59. PULLUP, LEVER, FIIGHT - 127 KIAS 50. STAB. AUTO. 324 RPH - 85 KIAS 62. STAB. AUTO. 324 RPH - 85 KIAS 63. STAB. AUTO. 324 RPH - 85 KIAS 64. STAB. AUTO. 324 RPH - 85 KIAS 65. STAB. AUTO. 324 RPH - 85 KIAS 65. STAB. AUTO. 329 RPH - 85 KIAS 66. STAB. AUTO. 329 RPH - 85 KIAS 67. AUTO TURN. RECOVER? 68. AUTO TURN. RECOVER? 69. AUTO TURN. AUTO. 326 KIAS 69. AUTO TURN. AUTO. 326 KIAS 69. AUTO. STEEDY - 126 KIAS 69. DIVE. REFT TURN PULLUP - 136 KIAS 69. DIVE. LEFT TURN PULLUP - 136 KIAS 69. CLIMB. MAX. RATE. PUSHOUGR - 65 69. CLIMB.
4000 FT	OSC.	ᡮ᠋᠋᠋᠋᠋᠋᠋᠋᠋᠋᠋᠋᠋ ᡊ᠋ᡊᡊᡳ᠘ᡮᡌᡎᢂ᠙᠙ᡩᠿᠯ᠙ᢣ᠕ᢊᢊᡌᡌᡢᠰᢧᡌᡌᡧ᠘ᡮ᠙᠙ᡮᡮ ᡊᡆᡊᡳ᠘ᡮᡭᡈᡶ᠙ᡩ᠙ᡩᠿᠯ᠙ᢣᢋᡶ᠙ᡭᠲ᠘ᡌ᠘ᠰ᠘ᢥ᠘ᡮ᠘ᡮ᠘ᡮ᠘ ᡊᢘ᠙᠙ᡭᡭᢤ᠙᠙᠙ᡩᡥᠯᢪ᠙ᡶᢋᡶ᠙ᡭᠲ᠘ᡩ᠘ᠰ᠘ᡮ᠘ᡮ᠘ᡮ᠘ᡮ᠘ ᡊᢘ᠙᠙ᡭᡭᢤ᠙ᢤ᠙᠙ᢤᢜᢪᠯ᠘ᡮᢋᢋᠲ᠘᠘᠘᠘᠘ᢤ᠘ᠰ᠘ᡮ᠘ᡮ᠘ᡮ᠘ᡮ᠘ᡮ᠘ ŶŶŶŶŶŶŶŶŶŶŶŶŶŶŶŶŶŶŶŶŶŶŶŶŶŶ
8. E. B.	MEAN.	2.00
PARAMETER M.R. HUB CHORD BENDING @ STA. TOGAL= 8476 LB TOGG= 192.4 IN	NO. TEST CONDITION	1. NORMAL START 0-100% NR 2. NORMAL TAKEDEF 4. JUMP TAKEDEF 5. HOVER TURN, LEFT 30 DEE-SEC 6. HOVER TURN, LEFT 30 DEE-SEC 7. HOVER TURN, LEFT 30 DEE-SEC 8. HOVER TURN, LEFT 30 DEE-SEC 10. SIDELARD K. LIGHT - LEFT 12. SIDELARD K. LIGHT - LEFT 13. SIDELARD K. LIGHT - LEFT 14. LEVEL R. LIGHT - 10 K. KIRS 15. LEVEL R. LIGHT - 10 K. KIRS 16. LEVEL R. LIGHT - 10 K. KIRS 17. LEVEL R. LIGHT - 10 K. KIRS 18. LEVEL R. LIGHT - 10 K. KIRS 19. LEVEL R. LIGHT - 10 K. KIRS 22. C. LINB 1000 FFM - 70 K. KIRS 23. C. LINB 1000 FFM - 85 K. KIRS 24. C. LINB 1000 FFM - 10 K. KIRS 25. C. LINB 1000 FFM - 10 K. KIRS 26. C. LINB 1000 FFM - 10 K. KIRS 27. C. LINB 1000 FFM - 10 K. KIRS 28. C. LINB 1000 FFM - 10 K. KIRS 29. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 21. C. LINB 1000 FFM - 10 K. KIRS 22. C. LINB 1000 FFM - 10 K. KIRS 23. C. LINB 1000 FFM - 10 K. KIRS 24. C. LINB 1000 FFM - 10 K. KIRS 25. C. LINB 1000 FFM - 10 K. KIRS 26. C. LINB 1000 FFM - 10 K. KIRS 27. C. LINB 1000 FFM - 10 K. KIRS 28. C. LINB 1000 FFM - 10 K. KIRS 29. C. LINB 1000 FFM - 10 K. KIRS 29. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 21. C. LINB 1000 FFM - 10 K. KIRS 22. C. LINB 1000 FFM - 10 K. KIRS 23. C. LINB 1000 FFM - 10 K. KIRS 24. LEFT TURN, 10 K. KIRS 25. C. LINB 1000 FFM - 10 K. KIRS 26. C. LINB 1000 FFM - 10 K. KIRS 27. LINB 1000 FFM - 10 K. KIRS 28. C. LINB 1000 FFM - 10 K. KIRS 29. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20. C. LINB 1000 FFM - 10 K. KIRS 20.

TABLE E-4 - Continued

+-428000.	OSC.	88888888888888888888888888888888888888
STATIC LIMITS	MEAN.	9898. 111156. 111156. 111156. 111156. 111156. 111151.
ENDURANCE LIMIT 68170. STATIC	TEST CONDITION	TURN REVERSAL, NDD 136 KIRS LAT. CONT. REVERSAL - 119 KIRS LAT. CONT. REVERSAL - 119 KIRS DILLUP, LEVEL F. IIGHT - 86 KIRS PULLUP, LEVEL F. IIGHT - 185 KIRS PULLUP, LEVEL F. IIGHT - 185 KIRS PULLUP, LEVEL F. IIGHT - 185 KIRS PULLUP, LEVEL F. IIGHT - 127 KIRS PULLUP, LEVEL F. IIGHT - 127 KIRS PULLUP, LEVEL F. IIGHT - 127 KIRS PULLUP, DIVE - 136 KIRS AUTO 324 RPM - 65 KIRS STAB. AUTO 324 RPM - 85 KIRS STAB. AUTO 324 RPM - 85 KIRS STAB. AUTO 324 RPM - 85 KIRS AUTO TURN, RIGHT - 70 KIRS AUTO TURN, RIGHT - 70 KIRS RIGHT SIDESLIP - 95 KIRS RIGHT SIDESLIP - 95 KIRS RIGHT SIDESLIP - 136 KIRS DIVE, STEADY - 136 KIRS DIVE, STEADY - 136 KIRS DIVE, STEADY - 136 KIRS DIVE, RIGHT TURN - 119 KIRS DIVE, LEFT TURN - 119 KIRS DIVE, LEFT TURN - 119 KIRS DIVE, LEFT TURN PULLUP - 136 KIRS DIVE, LEFT TURN PULLUP - 136 KIRS DIVE, LEFT TURN PULLUP - 136 KIRS DIVE, RIGHT TURN - 136 KIRS DIVE, LEFT TURN PULLUP - 136 KIRS DIVE, RIGHT TURN - 136 KIRS DIVE, RIGHT TURN - 119 KIRS DIVE, RIGHT TURN - 136 KIRS DIVE, RIGHT TURN - 136 KIRS DIVE, PULLUP - 136 KIRS CLIMB, MAX. RATE, PUSHOVER - 63
IN-LB	Š	<u>ĸŖŖĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸ</u>
4000 FT	OSC.	6.11.00.00.00.00.00.00.00.00.00.00.00.00.
STA.85 IN HD=	MEAN.	100.000
PARAMETER M.R. BLADE CHORD BENDING @ STA.85 TOG4- 8476 LB TOG6- 192.4 IN HD	NO. TEST CONDITION	1. NORTHE, START 0-100% NR. 2. NORTHE, SHUTDOM, 100-0%. 3. NORTHE, TAKEDEF. 4. JUNP TAKEDEF. 5. HOUER TURN, RIGHT 30 DEG-SEC. 6. HOUER TURN, RIGHT 30 DEG-SEC. 10. HOUER, LAT REVERSAL 11. SIDBLARD FLIGHT - LEFT T. 12. SIDBLARD FLIGHT - LEFT T. 13. REPREASED. 14. LEVEL R. IGHT - 102 KIRS. 15. LEVEL R. IGHT - 102 KIRS. 16. LEVEL R. IGHT - 102 KIRS. 17. LEVEL R. IGHT - 102 KIRS. 18. LEVEL R. IGHT - 102 KIRS. 19. LEVEL R. IGHT - 102 KIRS. 22. CLIMB, 1500 FPM - 70 KIRS. 23. CLIMB, 1500 FPM - 70 KIRS. 24. CLIMB, 1500 FPM - 70 KIRS. 25. CLIMB, 1500 FPM - 105 KIRS. 26. CLIMB, 1500 FPM - 105 KIRS. 27. CLIMB, 1500 FPM - 105 KIRS. 28. CLIMB, 1500 FPM - 105 KIRS. 29. CLIMB, 1500 FPM - 105 KIRS. 29. CLIMB, 1500 FPM - 105 KIRS. 20. CLIMB, 1500 FWH - 105 KIRS. 20. CLIMB,

TABLE E-4 - Continued

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STATIC LIMITS	MEAN.	### ##################################
		- 136 KIRS - 119 KIRS - 127 KIRS - 128 KIRS - 138 KIRS
IIT 39400.	MOLTION	
ENDURANCE LIMIT	TEST CONDITION	TURN REVERSAL, MOD. FYA COMT. REVERSAL LIGHT. CONT. REVERSAL FULLUP, LEUB. FLIGH PULLUP, STAR RPM STAR. AUTO, 324 RPM STAR. AUTO, 324 RPM STAR. AUTO, 334 RPM STAR. AUTO, 334 RPM STAR. AUTO, 334 RPM STAR. AUTO, 139 RPM CUTO DINN, RECOURTY APPROACH AND FLEEL FY SIDESLIP - 136 DINE, RIGHT TURN - 119 DINE, LITT TURN PULLUP DINE, RIGHT TURN PULLUP DINE, LITT TURN PULLUP DINE, RIGHT TU
		28888848888288884888888888888888888888
IN-LB	Z	ℴℴℴℴℴℴℴℴ ℴℴℴℴℴℴℴℴℴℴℴℴℴℴℴℴℴℴℴℴℴℴℴℴℴℴℴℴ
180 UNITS HD= 4000 FT	.080	4.444
I	MEHN.	9.69 1.00
BLADE CHORD BENDING 3476 LB TOGG= 192.4	CONDITION	NORTHAL STAFT 0-100% NR NORTHAL TAREOFE JUNE TAKEOFE JUNE TAKEOFE JUNE TAKEOFE JUNE TAKEOFE HOUER, LIGHT 30 DEG-SEC HOUER, FAR REVERSAL HOUER, LAT. LIGHT - 119 KIAS LEVEL FLIGHT - 119 KIAS LEVEL FLIGHT - 119 KIAS LEVEL FLIGHT - 136 KIAS RIGHT FLIKH - 136 KIAS
PARAMETER M.R. TOGW= 8	NO. TEST	11. NORPAL STATE OF THE PROPERTY OF THE PROPER

TABLE E-4 - Continued

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STATIC LIMITS	MEAN.	
ENDURANCE LIMIT 15580. STATIC	TEST CONDITION	TURN REVERSAL, MOD 136 KIAS LAT. CONT. REVERSAL - 119 KIAS LAT. CONT. REVERSAL - 119 KIAS DIR. CONT. REVERSAL - 119 KIAS BULLUP, LEVEL R. LIGHT - 85 KIAS PULLUP, LEVEL R. LIGHT - 127 KIAS STAB AUTO. 324 RPM - 85 KIAS STAB AUTO. 324 RPM - 85 KIAS PROGRAM - 80 KIAS PROGRAM - 126 KIAS PROGRAM - 126 KIAS PROGRAM - 126 KIAS PULLUP - 126 KIAS DIVE, RIGHT TURN - 119 KIAS DIVE, RIGHT TURN - 119 KIAS DIVE, RIGHT TURN - 119 KIAS DIVE, RIGHT TURN - 1136 KIAS DIVE, R. TURN PULLUP - 136 KIAS DIVE, RATE, PUSHOUGR - 65 CLIMB, MAX. RATE,
IN-LB	Š	<u>ආෆ්ෆ්අතුබ්ල අග්ලී අග්ලීල ඔහුණු දුරුප්දේ හුණු ඉතිසි කුම්ම ඉතිසි මුම්ම</u>
UNITS 1000 FT	. DSC.	\$44,000,000,000,000,000,000,000,000,000,
@ STA.85 N HD= 4000	MEAN.	44.44.44.44.44.44.44.44.44.44.44.44.44.
PARAMETER M.R. BLADE TORSION BENDING @ TOGA= 8476 LB TOGS= 192.4 IN	NO. TEST CONDITION	1. NORMAL START 0-1000: NR 3. NORMAL TAKEDEN 4. JUNP TAKEDEN 5. HOUER LIGE 324 REN 6. HOUER LIGH, LEFT 30 DEG-SEC 7. HOUER LIGH 18 STARES 1. SIDELARD RIGHT 30 DEG-SEC 8. HOUER, LIGH REVERSAL 11. SIDELARD RIGHT - LEFT 12. SIDELARD RIGHT - LEFT 13. EDRILL RIGHT - REVERSAL 14. EVEL RIGHT - REVERSAL 15. LEVEL RIGHT - REVERSAL 16. SIDELARD RIGHT - LEFT 17. LEVEL RIGHT - REVERSAL 18. LEVEL RIGHT - REVERSAL 19. LEVEL RIGHT - REVERSAL 19. LEVEL RIGHT - REVERSAL 19. LEVEL RIGHT - 102 KIRS 22. CLIMB SOO FFM - 70 KIRS 23. CLIMB 500 FFM - 70 KIRS 24. CLIMB 500 FFM - 85 KIRS 25. CLIMB 500 FFM - 105 KIRS 26. CLIMB 500 FFM - 105 KIRS 27. CLIMB 500 FFM - 105 KIRS 28. CLIMB 500 FFM - 119 KIRS 29. CLIMB 500 FFM - 119 KIRS 29. CLIMB 1000 FFM - 105 KIRS 29. LEFT TURN, 105 KIRS 29. LURN REVERSAL MILLD - 105 KIRS 20. LURN REVERSAL MILLD

TABLE E-4 - Continued

	OSC.	884-8888-8888-8888-8888-8888-8888-8888
STATIC LIMITS	MEAN.	4.86.89.84.89.84.84.84.85.88.89.89.89.89.89.89.89.89.89.89.89.89.
ENDURANCE LIMIT 11800.	NO. TEST CONDITION	51. TURN REVERSAL, MDD 136 KIAS 52. F-A CONT. REVERSAL - 119 KIAS 53. LAT. CONT. REVERSAL - 119 KIAS 54. DIR. CONT. REVERSAL - 119 KIAS 55. PULLUP, LEVEL R. IGHT - 85 KIAS 57. PULLUP, LEVEL R. IGHT - 85 KIAS 59. PULLUP, LEVEL R. IGHT - 127 KIAS 60. PULLUP, LEVEL R. IGHT - 127 KIAS 61. AUTOROPATION ENTRY - 70 KIAS 62. STAB. AUTO. 324 RPM - 85 KIAS 62. STAB. AUTO. 324 RPM - 85 KIAS 63. STAB. AUTO. 324 RPM - 85 KIAS 64. STAB. AUTO. 324 RPM - 85 KIAS 65. STAB. AUTO. 324 RPM - 85 KIAS 65. STAB. AUTO. 329 RPM - 85 KIAS 66. STAB. AUTO. 329 RPM - 85 KIAS 67. AUTO PURN. REDOVERY 71. LEFT SIDESLIP - 70 KIAS 68. AUTO TURN. REDOVERY 72. LEFT SIDESLIP - 136 KIAS 73. LEFT SIDESLIP - 136 KIAS 74. RIGHT SIDESLIP - 136 KIAS 75. LEFT SIDESLIP - 136 KIAS 76. DIUE, STEADY - 136 KIAS 77. DIUE, STEADY - 136 KIAS 78. DIUE, STEADY - 136 KIAS 78. DIUE, RIGHT TURN - 119 KIAS 78. DIUE, RIGHT TURN PULLUP - 136 KIAS 78. DIUE, RIGHT TURN PULLUP - 136 KIAS 79. DIUE, RIGHT TURN PULLUP - 136 KIAS 79. DIUE, RIGHT TURN PULLUP - 136 KIAS 70. DIUE, RIGHT TURN R. PULLUP - 136 KIAS 70. DIUE, RIGHT TURN R. PULLUP - 136 KIAS 70. DIUE, RIGHT TURN R. PULLUP - 136 KIAS 70. DIUE, RIGHT TURN R. PULLUP - 136 KIAS 70. DIUCK STOP - 136 KIAS TO HOUER.
UNITS IN-LB	OSC.	2.00 4.00 5.00 5.00 5.00 5.00 5.00 5.00 5
STA.180 HD= 4000 F	MEAN, O	ና ደጀዋሪያ የተመደመ የሚያቸው የሚ
PARAMETER M.R. BLADE TORSION BENDING (TOSM= 8476 LB TOGG= 192.4 I)	NO. TEST CONDITION	1. NORTH, STRET 0-100% NR 2. NORTH, STRET 0-100% NR 3. NORTH, STREDFE 5. HOURE 138: 344 RPH 10. HOURE 138: 344 RPH 10. HOURE 138: 344 RPH 10. HOURE 138: 346 RPH 10. HOURE 118: 346 RPH 11. SIDE-ARD F.IGHT - LEFT 12. SIDE-ARD F.IGHT - LEFT 13. REPRESEL - 100 F.IGHT 14. LEUEL F.IGHT - NO KIRS 15. LEUEL F.IGHT - 102 KIRS 16. LEUEL F.IGHT - 103 KIRS 17. LEUEL F.IGHT - 104 KIRS 18. LEUEL F.IGHT - 104 KIRS 22. CLINB. SOO FFH - 30 KIRS 23. CLINB. SOO FFH - 30 KIRS 24. CLINB. SOO FFH - 30 KIRS 25. CLINB. SOO FFH - 30 KIRS 26. CLINB. SOO FFH - 30 KIRS 27. CLINB. SOO FFH - 30 KIRS 28. CLINB. SOO FFH - 30 KIRS 29. CLINB. SOO FFH - 105 KIRS 29. CLINB. NAX. RATE - 105 KIRS 29. CLINB. NAX. RATE - 105 KIRS 30. CLINB. NAX. RATE - 105 KIRS 31. CLINB. NAX. RATE - 105 KIRS 32. CLINB. NAX. RATE - 105 KIRS 33. CLINB. NAX. RATE - 105 KIRS 34. LEFT TURN. NS KIRS 35. LEFT TURN. NS KIRS 36. LEFT TURN. NS KIRS 37. LEFT TURN. NS KIRS 38. LEFT TURN. NS KIRS 39. RIGHT TURN. NS KIRS 40. RIGHT TURN. NS KIRS 41. RIGHT TURN. NS KIRS 42. RIGHT TURN. NS KIRS 43. RIGHT TURN. NS KIRS 44. RIGHT TURN. NS KIRS 45. TURN REVERSER. MILD - 105 KIRS 46. TURN REVERSER. MILD - 105 KIRS 47. TURN REVERSER. MILD - 105 KIRS 48. TURN REVERSER. MILD - 105 KIRS 49. TURN REVERSER. MILD - 105 KIRS 50. TURN REVERSER. MILD - 105 KIR

TABLE E-4 - Continued

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ENDURANCE LIMIT	TEST CONDITION	2004-188-200-1
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UNITS HD= 4000 FT	OSC.	œwwwwwwwwwwwwwwwwwwwwwwwwwwwwwwwwwwwww
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D TOCG= 192.4 IN		
g.	3	2
H LINK LOAD 8476 LB T	CONDITION	2010-100 2017-1
PARAMETER PITCH TOGW= 8	TEST (NORTH START
PMETER		
PAIR	Š	ਜ਼ਗ਼ਜ਼ਖ਼ਜ਼ਜ਼ਜ਼ਫ਼ਜ਼ਜ਼ਜ਼ਜ਼ਸ਼ਜ਼ਜ਼ਜ਼ਜ਼ਖ਼

TABLE E-4 - Continued

OSC.	88449888888888888888888888888888888888
MEAN.	286 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
O. TEST CONDITION	51. TURN REVERSAL MOD 136 KIAS 52. LAT. CONT. REVERSAL - 119 KIAS 53. LAT. CONT. REVERSAL - 119 KIAS 54. PULLUP. LEVEL FLIGHT - 48 KIAS 55. PULLUP. LEVEL FLIGHT - 48 KIAS 55. PULLUP. LEVEL FLIGHT - 105 KIAS 56. PULLUP. LEVEL FLIGHT - 105 KIAS 57. PULLUP. LEVEL FLIGHT - 105 KIAS 58. PULLUP. LEVEL FLIGHT - 105 KIAS 59. PULLUP. LEVEL FLIGHT - 105 KIAS 61. AUTOROTATION ENTRY - 70 KIAS 62. STAB. AUTO. 324 RPH - 85 KIAS 63. STAB. AUTO. 324 RPH - 85 KIAS 64. STAB. AUTO. 324 RPH - 85 KIAS 65. STAB. AUTO. 324 RPH - 85 KIAS 66. STAB. AUTO. 324 RPH - 85 KIAS 66. STAB. AUTO. 324 RPH - 85 KIAS 67. LEFT SIDESLIP - 70 KIAS 68. STAB. AUTO. 105 KIAS 69. PULLUP - 119 KIAS 69. DIUE. STEADY - 136 KIAS 69. DIUE. STEADY - 136 KIAS 69. DIUE. KIT TURN - 119 KIAS 69. DIUE. RETT TURN - 110 KIAS 69. DIUE. RETT TURN - 1
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OSC.	9999 8999 8999 8999 8999 8999 8999 899
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NO. TEST CONDITION	1 NORTH START 0-100% NR 2 NORTH SHIDDLN 100-0% 3 NORTH SHIDDLN 100-0% 4 JULP TAKEDF 5 HOUER TIRN, RIGHT 30 DEG-SEC 8 HOUER TIRN, RIGHT 30 DEG-SEC 9 HOUER LOT REVERSAL 11 SIDEJARD FIGHT LEFT 13 REARAND FIGHT LEFT 14 LEVEL FLIGHT - RIGHT 15 LEVEL FLIGHT - 102 KIRS 15 LEVEL FLIGHT - 102 KIRS 16 LEVEL FLIGHT - 102 KIRS 17 LEVEL FLIGHT - 102 KIRS 18 LEVEL FLIGHT - 102 KIRS 19 LEVEL FLIGHT - 102 KIRS 19 LEVEL FLIGHT - 102 KIRS 22 CLINB 500 FPM - 30 KIRS 23 CLINB 1500 FPM - 30 KIRS 24 CLINB 1500 FPM - 105 KIRS 25 CLINB 1500 FPM - 105 KIRS 26 CLINB 1500 FPM - 105 KIRS 27 CLINB 1500 FPM - 105 KIRS 28 CLINB 1500 FPM - 105 KIRS 29 CLINB 1500 FPM - 105 KIRS 20 CLINB 100 FPM - 105 KIRS 20 CLINB 100 FPM - 105 KIRS 20 CLINB 100 FPM - 105 KIRS 20 KIGHT TURN 105 KIRS 20 KIRSTESAL MILLD 1105 KIRSTESAL MI
	. TEST CONDITION MEAN. OSC. NO. TEST CONDITION MEAN.

TABLE E-4 - Continued

	OSC.	24.17 26.18
STATIC LIMITS	MEAN.	2.00 a 10 4 2 4 2 4 2 4 2 4 2 4 2 4 2 4 2 4 2 4
IN-LB ENDURANCE LIMIT 22610. STATIC	NO. TEST CONDITION	51. TURN REVERSAL, MOD. — 136 KIRS 52. LAT. CONT. REVERSAL — 119 KIRS 53. LAT. CONT. REVERSAL — 119 KIRS 54. DIR. CONT. REVERSAL — 119 KIRS 55. PULLUP, LEVEL R. IGHT — 85 KIRS 56. PULLUP, LEVEL R. IGHT — 86 KIRS 57. PULLUP, LEVEL R. IGHT — 87 KIRS 58. PULLUP, LEVEL R. IGHT — 135 KIRS 61. AUTOMOTATION ENTRY — 70 KIRS 62. STAB. AUTO, 324 RRM — 85 KIRS 62. STAB. AUTO, 324 RRM — 85 KIRS 63. STAB. AUTO, 324 RRM — 85 KIRS 64. STAB. AUTO, 324 RRM — 86 KIRS 65. STAB. AUTO, 324 RRM — 86 KIRS 66. STAB. AUTO, 324 RRM — 86 KIRS 67. AUTO PUR, RECOVERY 70. LEFT SIDESLIP — 70 KIRS 71. LEFT SIDESLIP — 70 KIRS 72. LEFT SIDESLIP — 70 KIRS 73. LEFT SIDESLIP — 70 KIRS 74. RIGHT SIDESLIP — 70 KIRS 75. LEFT SIDESLIP — 70 KIRS 76. DIVE, STEADY — 136 KIRS 77. DIVE, STEADY — 136 KIRS 78. DIVE, STEADY — 136 KIRS 79. DIVE, STEADY — 136 KIRS 70. DIVE, R. STEADY — 136 KIRS 70. DIVE, R. TURN PULLUP— 119 KIRS 71. DIVE, RT. TURN PULLUP— 119 KIRS 72. LEFT TURN PULLUP— 119 KIRS 73. DIVE, RT. TURN PULLUP— 119 KIRS 74. DIVE, RT. TURN PULLUP— 119 KIRS 75. DIVE, RT. TURN PULLUP— 119 KIRS 76. DIVE, RT. TURN PULLUP— 119 KIRS 77. DIVE, RT. TURN PULLUP— 136 KIRS 77. DIVE, RT. TURN PULLUP— 136 KIRS 77. DIVE, RT. TURN PULLUP— 136 KIRS 77. DIVE, RT. TURN PULLUP— 137 KIRS 77. DIVER RT. TURN PULLUP— 137 KIRS 77. DIVER RT. TURN PULLUP— 137 KIRS 77. DIVER RT. TURN PULLUP— 137 KIRS 77. DIV
UNITS HD= 4000 FT	OSC.	1188
	MEAN.	လွန်းနိုင်ငံ မရှိနှင့်မှု မရှိနှင့် မြောင်းရှိနှင့် မြောင်းရှိနှင့် မြောင်းရှိနှင့် မြောင်းရှိနှင့် မြောင်းရှိနှင့် မြောင်း မြောင်းရှိနှင့် မြောင်းရှိနှင့် မြောင်းရှိနှင့် မြောင်းရှိနှင့် မြောင်းရှိနှင့် မြောင်းရှိနှင့် မြောင်းရှိနှင့်
PARAMETER M.R. MAST BENDING @ 0. DEG. TOGA = 8476 LB TOCG = 192.4 IN	NO. TEST CONDITION	1. NORPH, START 0-100% NR 3. NORPH, START 0-100% NR 3. NORPH, TAKEOFF 4. JULP TAKEOFF 5. HOUR TORN, RIGHT 30 DEG-SEC 6. HOUR TURN, RIGHT 30 DEG-SEC 10. HOUR TORN, REVERSAL 11. SIDBJARD RIGHT - LEFT 12. SIDBJARD RIGHT - RIGHT 13. SIDBJARD RIGHT - RIGHT 14. LEVEL RIGHT - RS KIRS 19. LEVEL RIGHT - RS KIRS 19. LEVEL RIGHT - 102 KIRS 20. CLIMB, 1000 FPM - 70 KIRS 22. CLIMB, 1000 FPM - 70 KIRS 23. CLIMB, 500 FPM - 105 KIRS 24. CLIMB, 500 FPM - 105 KIRS 25. CLIMB, 500 FPM - 105 KIRS 26. CLIMB, 500 FPM - 105 KIRS 27. CLIMB, 500 FPM - 105 KIRS 28. CLIMB, 500 FPM - 105 KIRS 29. CLIMB, 700 FPM - 105 KIRS 29. CLIMB, 700 FPM - 105 KIRS 29. CLIMB, 700 FPM - 105 KIRS 29. LEFT TURN, 70 KIRS 29. LEFT TURN, 105 KIRS

TABLE E-4 - Continued

	OSC.	### ##################################
STATIC LIMITS	MEAN.	ထုံရှိုင်မှုတွင် ကုန်လိုက်မှုတွင် ကုန်လိုက်မှုတွင် မှုတွင် မြောက်မှုတွင် မြောက်မှုတွင် မြောက်မှုတွင် မြောက်မှ ကုန်လိုက်ရှိတို့တွင် မြောက်မှုတွင် မြောက်မှုတွင် မြောက်မှုတွင် မြောက်မှုတွင် မြောက်မှုတွင် မြောက်မှုတွင် မြောက်
IN-LB BNDURANCE LIMIT 22610. STATIC	NO. TEST CONDITION	51. TURN REVERSAL 113 KIRS 52. EAG COMT. REVERSAL 113 KIRS 53. DIT. COMT. REVERSAL 113 KIRS 54. DIT. COMT. REVERSAL 113 KIRS 55. PULLUP. LEVEL F. LIGHT - 105 KIRS 56. PULLUP. LEVEL F. LIGHT - 105 KIRS 57. PULLUP. LEVEL R. LIGHT - 105 KIRS 58. PULLUP. LEVEL R. LIGHT - 105 KIRS 60. PULLUP. LEVEL R. LIGHT - 107 KIRS 60. PULLUP. LEVEL R. LIGHT - 107 KIRS 61. AUTO TURN BUTRY - 70 KIRS 62. STAB. AUTO, 224 RPH - 62 KIRS 63. STAB. AUTO, 234 RPH - 62 KIRS 64. STAB. AUTO, 339 RPH - 105 KIRS 65. AUTO TURN. RIGHT - 70 KIRS 66. STAB. AUTO, 239 RPH - 85 KIRS 67. AUTO TURN. RIGHT - 70 KIRS 68. AUTO FUR. RECOVERY 70. LEPT SIDESLIP - 70 KIRS 71. LEPT SIDESLIP - 70 KIRS 72. LEPT SIDESLIP - 70 KIRS 73. LEPT SIDESLIP - 70 KIRS 74. LEPT SIDESLIP - 70 KIRS 75. RIGHT SIDESLIP - 70 KIRS 76. RIGHT SIDESLIP - 70 KIRS 77. LEPT SIDESLIP - 70 KIRS 78. DIVE. STERAY - 119 KIRS 79. DIVE. RIGHT TURN - 119 KIRS 80. DIVE. LEPT TURN - 119 KIRS 81. DIVE. RIT TURN PULLUP - 136 KIRS 82. DIVE. LEPT TURN PULLUP - 136 KIRS 83. DIVE. RT. TURN PULLUP - 136 KIRS 84. DIVE. RT. TURN PULLUP - 136 KIRS 85. DIVE. RT. TURN PULLUP - 136 KIRS 86. DIVE. RT. TURN PULLUP - 136 KIRS 87. DIVE. RT. TURN PULLUP - 136 KIRS 88. DIVE. RT. TURN PULLUP - 136 KIRS 89. DIVER RTE. PUSHOVER - 65 91. DUICK STOP - 136 KIRS TO HOUER.
UNITS HD= 4600 FT	asc.	QQQ110144401000 QQQ110144400000 AQQ1101444000000000000000000000000000000
	MEAN.	ၛၛႜၟၛၯႜႜႜႜၛၟၜၯၟႜၛႜၛၛၟၯႜၯၟၛၯႜၛႜၛႜၛ ၛၛႜၟၛၯႜၛၟၟၜၯၛၛၟႜၟၛၟၛၟၯႜၛၟၛၯႜၛႜၛႜၛ ၛၛႜၛႜၛၛၛၯႍႜၛၛၛၛၟႜၛၛၟၛၛၛၛၛၛ
PERPITER M.R. MAST BENDING @ 90 DEG. TOGH TOGH 192.4 IN	NO. TEST CONDITION	1. NORMAL STAPT 0-100% NR 2. NORMAL STAPT 0-100% NR 3. NORMAL STAPT 0-100% NR 3. NORMAL TREEDEF 5. HOVER IGE 224 RF1 10. HOVER TURN. LEFT 30 DEG-SEC 6. HOVER TURN. LEFT 30 DEG-SEC 11. SIDELARD R-104T - REJERSAL 12. SIDELARD R-104T - REJERSAL 13. LEVEL R-104T - REJERSAL 14. LEVEL R-104T - REJERSAL 15. LEVEL R-104T - REJERSAL 16. LEVEL R-104T - REJERSAL 17. LEVEL R-104T - REJERSAL 18. LEVEL R-104T - REJERSAL 19. LEVEL R-104T - REJERSAL 104T - REJERSAL - REJERSAL 104T - REJERSAL - R

TABLE E-4 - Continued

	LIMITS	MEAN.	4.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9
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	ENDURANCE LIMIT	TEST CONDITION	発見解析可可可可可と ここここここここここここここここここここここここここここここここ
	ENDO		
	m	ż	<u>ႯŖŖĸĸŖŖĠĠĠĠĠŖŖĠĊĠ</u> ġġĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸ
	9		
	300 FT	OSC.	8C-8-0118C - 111111111111111111111111111111111
	N HD= 4000	MEAN.	888 9448 9448 9448 9448 9448 9448 9448
	PARAMETER THRUST LINK LOAD TOGA = 8476 LB TOCG: 192.4 IN		្តិចិច្ចិច្ច
	6. 19		2000 No
	Sp		27.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.
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TABLE E-4 - Continued

	OSC.	######################################
STATIC LIMITS	MEAN.	\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
ENDURANCE LIMIT 1290. STATIC	TEST CONDITION	TURN REVERSAL, NOD. — 136 KIRS FAR CONT. REVERSAL.—119 KIRS FULLUP. LEVEL F. LIGHT — 85 KIRS FULLUP. LEVEL F. LIGHT — 85 KIRS FULLUP. LEVEL F. LIGHT — 195 KIRS FULLUP. LEVEL F. LIGHT — 127 KIRS FULLUP. LEVEL F. LIGHT — 128 KIRS FULLUP. 224 RPH — 85 KIRS FULLUP. 224 RPH — 85 KIRS FULLUP. 239 RPH — 95 KIRS FULLUP. LEVEL F. TO KIRS FULLUP. LEFT TURN — 119 KIRS FULLUP. LIGHT — 136 KIRS FULLUP. LIGHT —
m	ė	<u> </u>
UNITS LB	OSC.	ąĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸ
	MEAN.	%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
PARAMETER LATERAL ACTUATOR LOAD TOGN* 8476 LB TOGF 192.4 IN	NO. TEST CONDITION	1. NORTH, START 0-100% NR 2. NORTH, SHUTDON 100-0% 3. NORTH, SHUTDON 100-0% 4. JULP TAKEOFF 10. HOURR, LET 30 DEG-SEC 10. HOURR, LET 30 DEG-SEC 10. HOURR, LET 30 DEG-SEC 10. SIDELARD R. IGHT - LEFT 12. SIDELARD R. IGHT - RETT 13. SERRARD R. IGHT - NO KINS 15. LEVEL R. IGHT - 102 KINS 16. LEVEL R. IGHT - 102 KINS 17. LEVEL R. IGHT - 102 KINS 18. LEVEL R. IGHT - 103 KINS 20. CLINB, 1000 FPH - 70 KINS 21. CLINB, 1000 FPH - 105 KINS 22. CLINB, 1000 FPH - 105 KINS 23. CLINB, 1000 FPH - 105 KINS 24. CLINB, 1000 FPH - 105 KINS 25. CLINB, 1000 FPH - 105 KINS 26. CLINB, 1000 FPH - 105 KINS 27. CLINB, 1000 FPH - 105 KINS 28. CLINB, 1000 FPH - 105 KINS 29. LEFT TURN, 205 KINS 29. L

TABLE E-4 - Continued

	OSC.	4443. 1822. 6924. 5102. 3011.	2186. 33704. 3333. 11289. 1509.	2882 2634. 391129. 39140. 1129. 1229.	200 200 200 200 200 200 200 200 200 200	2822 382744 1113 2711 1481 222	
STATIC LIMITS	MEAN.	184399. 145398. 149770. 143576. 71507.	112237. 142846. 131079. 66280. 89948. -5645.			64429 46643 45873 52838 52838 16821 16821 188597 188597 18115	
IN-LB ENDURANCE LIMIT 38980?	NO. TEST CONDITION	51. TURN REVERSAL, MOD 136 KIAS 52. F/A CONT. REVERSAL - 119 KIAS 53. LAT. 10NT. REVERSAL - 119 KIAS 54. DIR. CONT. REVERSAL - 119 KIAS 55. PULLUP. LEVIE. R. 11947 - 70 KIAS 56. PULLUP. LEVIE. R. 11947 - 70 KIAS	55. PULLUP. LEVEL F. LIGHT - 135. KIRS 58. PULLUP. LEVEL F. LIGHT - 119 KIRS 59. PULLUP. LEVEL F. LIGHT - 127 KIRS 60. PULLUP. LEVEL F. LIGHT - 127 KIRS 61. AUTOROTHICN ENTRY - 70 KIRS 62. STAB. AUTO. 324 RPM - 78 KIRS 63. STAB. AUTO. 324 RPM - 85 KIRS 64. STAB. AUTO. 324 RPM - 85 KIRS 65. STAB. AUTO. 324 RPM -	65. STAB. AUTO. 329 RPM - 85 KIAS. 66. STAB. AUTO. 339 RPM - 85 KIAS. 67. AUTO TURN, RIGHT - 70 KIAS. 69. AUTO TURN, LEFT - 70 KIAS. 70. LEFT SIDESLIP - 70 KIAS. 71. LEFT SIDESLIP - 70 KIAS. 72. LEFT SIDESLIP - 70 KIAS.	73. ELFT SIDESLIP - 79 KIHS 75. RIGHT SIDESLIP - 70 KIHS 75. RIGHT SIDESLIP - 85 KIHS 76. RIGHT SIDESLIP - 136 KIHS 77. DIVE, STEADY - 119 KIHS 79. DIVE, RIGHT TURN - 119 KIHS 80. DIVE, LEFT TURN - 119 KIHS 81. DIVE, RIGHT TURN - 119 KIHS	82. DIUE. LEFT TURN PULLUP- 136 KIGS. 83. DIUE. LT. TURN PULLUP- 119 KIGS. 84. DIUE. LT. TURN PULLUP- 136 KIGS. 85. DIUE. LT. TURN PULLUP- 136 KIGS. 86. DIUE. LT. TURN PULLUP- 136 KIGS. 87. DIUE. PULLUP- 136 KIGS. 88. CLINB. MAX. RATE. PUSHOUER- 136 KIGS. 99. CLINB. MAX. RATE. PUSHOUER- 136 KIGS. 91. GUICK STOP - 136 KIGS TO HOUER.	
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PARAMETER M.R. DRIVESHAFT TORSION TOGA: 8476 LB TOC6= 192.4 IN	NO. TEST CONDITION	1. NDRM. START 0-100% NR 2. NDRM. SHITDLN 100-0% 3. NDRM. INKEDFF 4. JUNP TAKEDFF 5. HOURING TAKEDFF 6. HOURING TAKEDFF 6. HOURING TAKEDFF	THOUSE TURN, KIGHT 30 DEG-SEL HOUER TURN, LEFT 30 DEG-SEC HOUER, LAT. REVERSAL 10. HOUER, LAT. REVERSAL 11. SIDELARD FLIGHT - RIGHT 12. SIDELARD FLIGHT - LEFT 13. REARLARD FLIGHT - LEFT	15. LIVUE, FLIGHT - 85 KIRS 16. LEVE, FLIGHT - 102 KIRS 17. LEVE, FLIGHT - 119 KIRS 18. LEVE, FLIGHT - 127 KIRS 20. LLIMB, 1500 FPM - 70 KIRS 21. CLIMB, 1500 FPM - 70 KIRS 22. CLIMB, 1500 FPM - 70 KIRS	23. CLIMB, 1500 FPH - 95 KIRS 24. CLIMB, 1500 FPH - 95 KIRS 25. CLIMB, 1500 FPH - 95 KIRS 26. CLIMB, 1600 FPH - 105 KIRS 27. CLIMB, 1000 FPH - 105 KIRS 28. CLIMB, 500 FPH - 119 KIRS 39. CLIMB, MKX, RATE - 105 KIRS 31. CLIMB, MKX, RATE - 105 KIRS 31. CLIMB, MKX, RATE - 119 KIRS	32. CLITTO THE ROTE - 136 KINS 34. LEFT TURN, 85 KINS 35. LEFT TURN, 85 KINS 36. LEFT TURN, 195 KINS 37. LEFT TURN, 119 KINS 39. LEFT TURN, 137 KINS 39. LEFT TURN, 137 KINS 40. RIGHT TURN, 105 KINS 41. RIGHT TURN, 105 KINS 42. RIGHT TURN, 105 KINS 43. RIGHT TURN, 105 KINS 44. RIGHT TURN, 105 KINS 44. RIGHT TURN, 127 KINS 44. RIGHT TURN, 127 KINS 45. RIGHT TURN, 127 KINS 46. RIGHT TURN, 127 KINS	46. TURN REVERSAL, MILD – 85 KIAS – 47. TURN REVERSAL, MILD – 119 KIAS – 49. TURN REVERSAL, MILD – 119 KIAS – 49. TURN REVERSAL, MILD – 136 KIAS – 50. TURN REVERSAL, MILD – 136 KIAS – 50. TURN REVERSAL, MILD – 136 KIAS

TABLE E-4 - Continued

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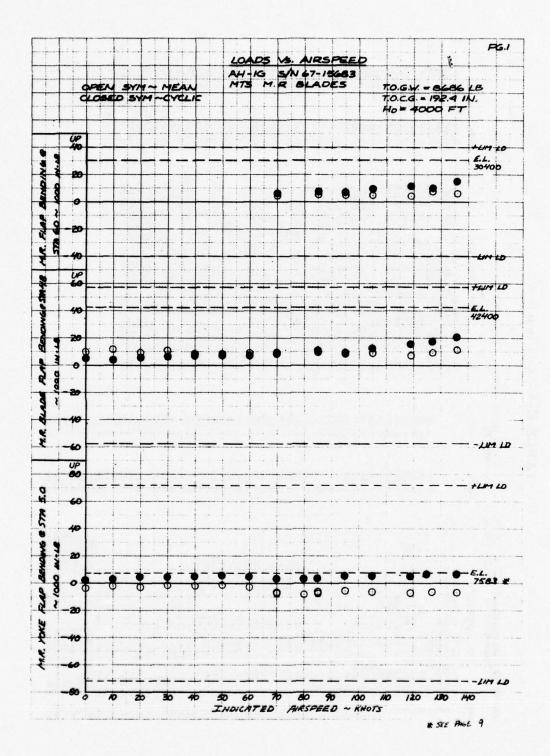


Figure E-1. Loads versus airspeed (Sheet 1 of 9).

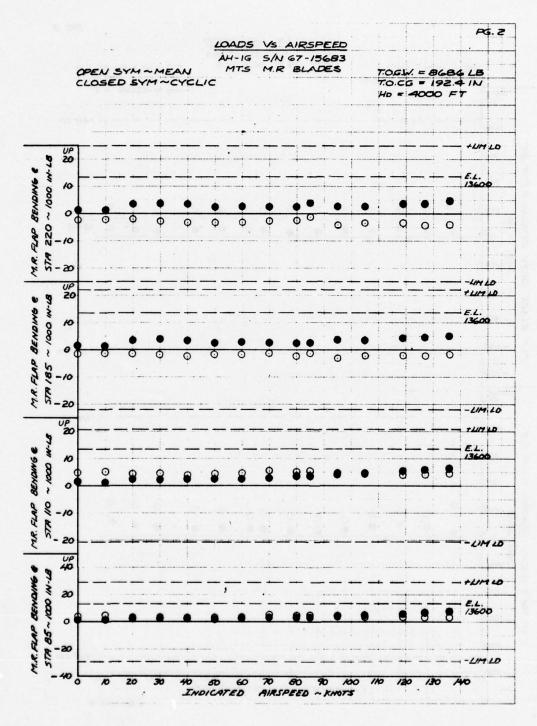


Figure E-1. Loads versus airspeed (Sheet 2 of 9).

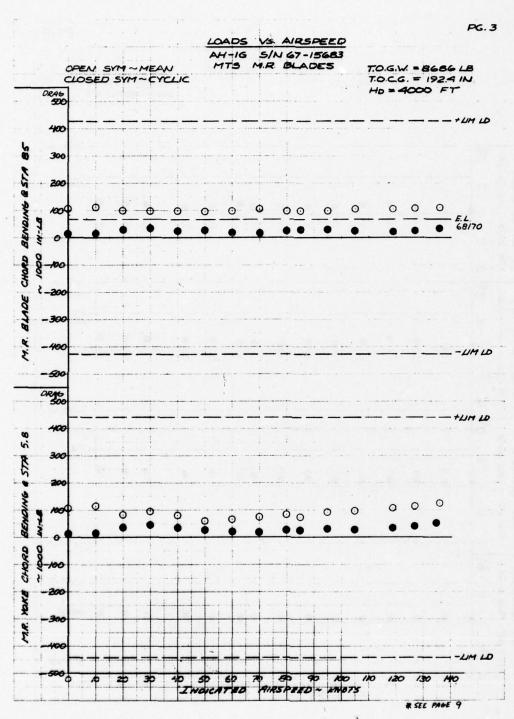


Figure E-1. Loads versus airspeed (Sheet 3 of 9).

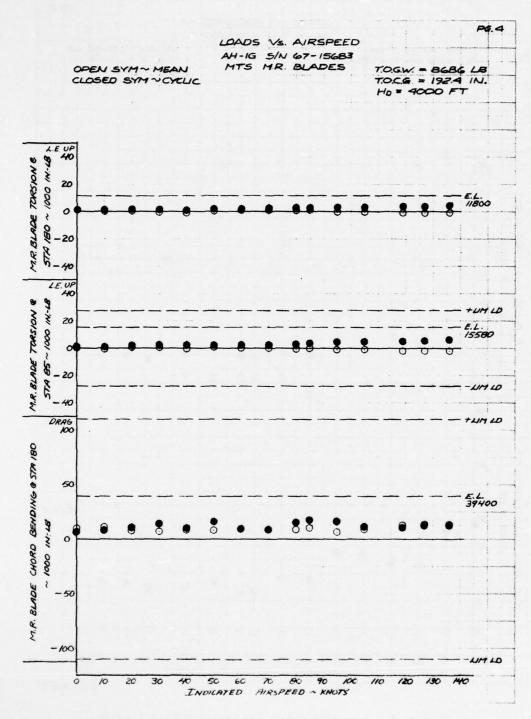


Figure E-1. Loads versus airspeed (Sheet 4 of 9).

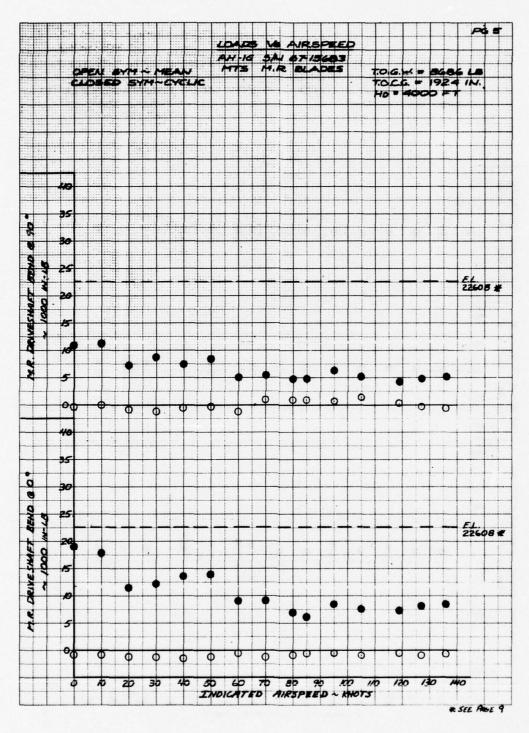


Figure E-1. Loads versus airspeed (Sheet 5 of 9).

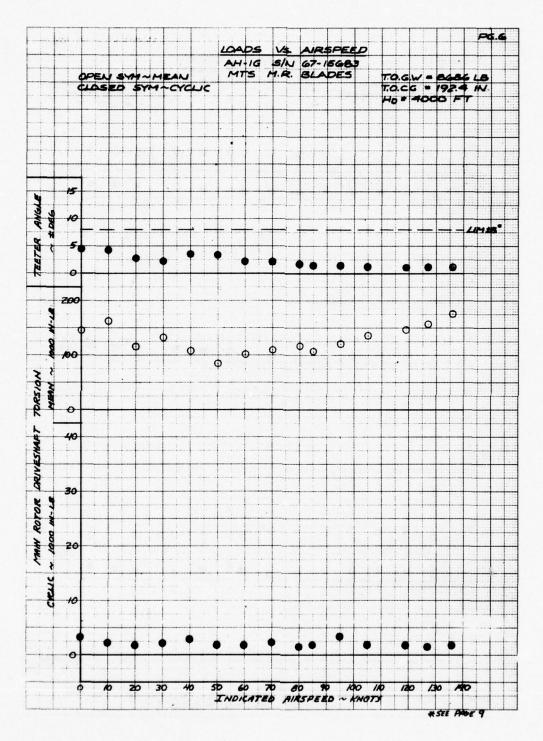


Figure E-1. Loads versus airspeed (Sheet 6 of 9).

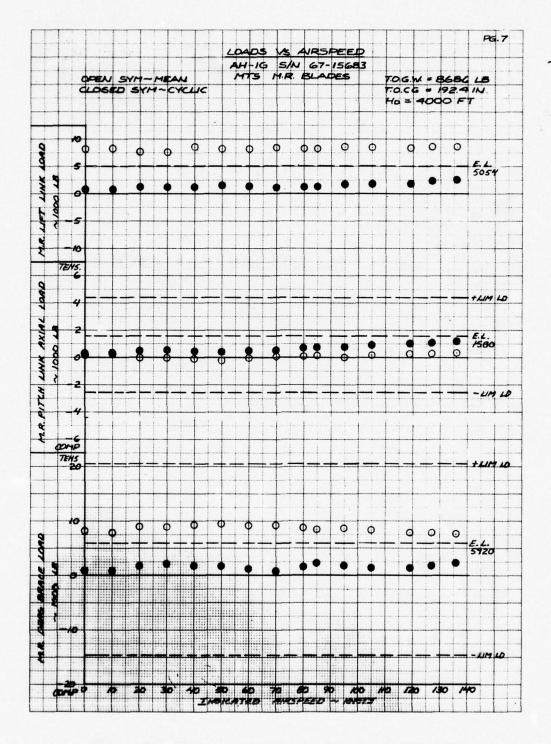


Figure E-1. Loads versus airspeed (Sheet 7 of 9).

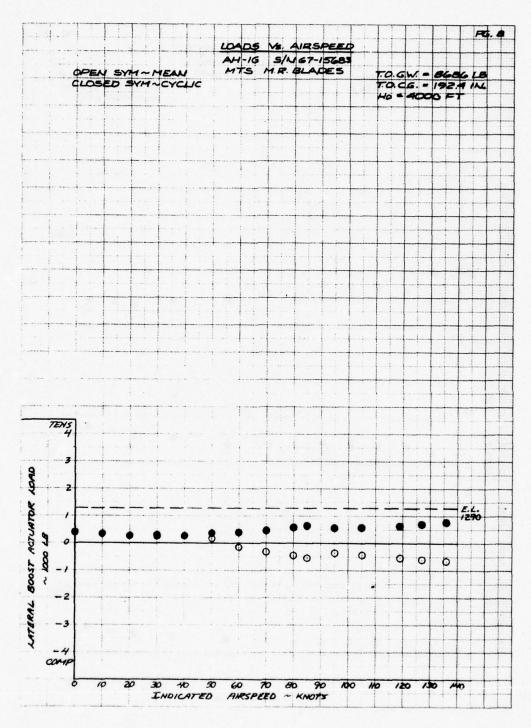


Figure E-1. Loads versus airspeed (Sheet 8 of 9).

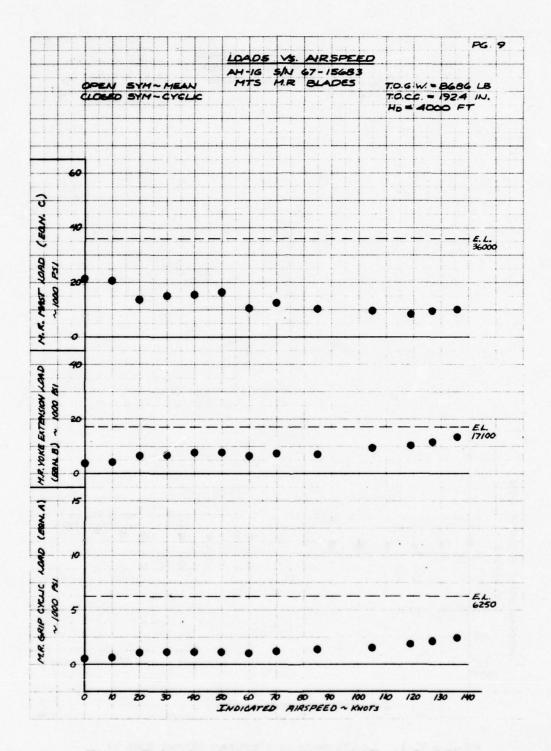


Figure E-1. Loads versus airspeed (Sheet 9 of 9).

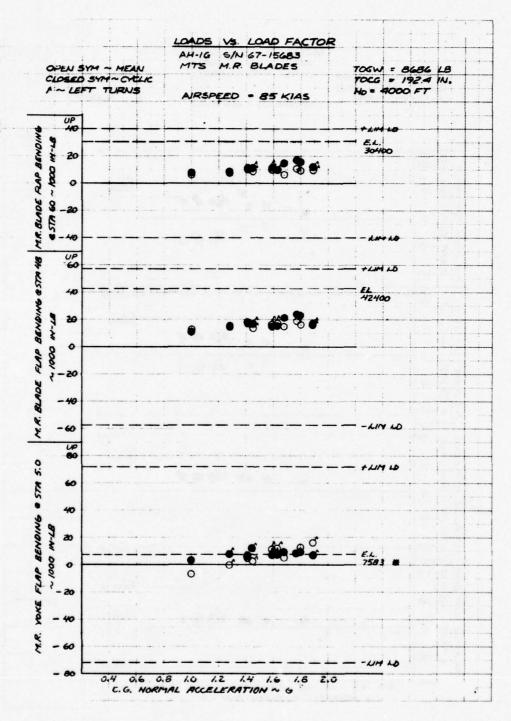


Figure E-2. Loads versus load factor - airspeed = 85 KIAS (Sheet 1 of 9).

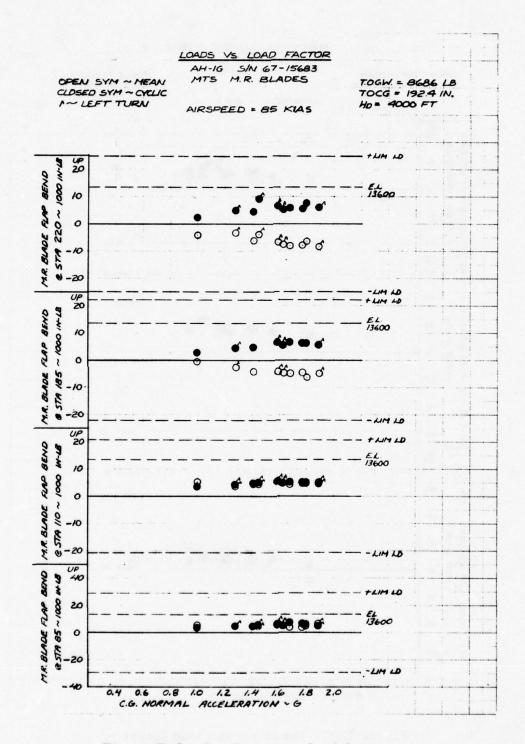


Figure E-2. Loads versus load factor - airspeed = 85 KIAS (Sheet 2 of 9).

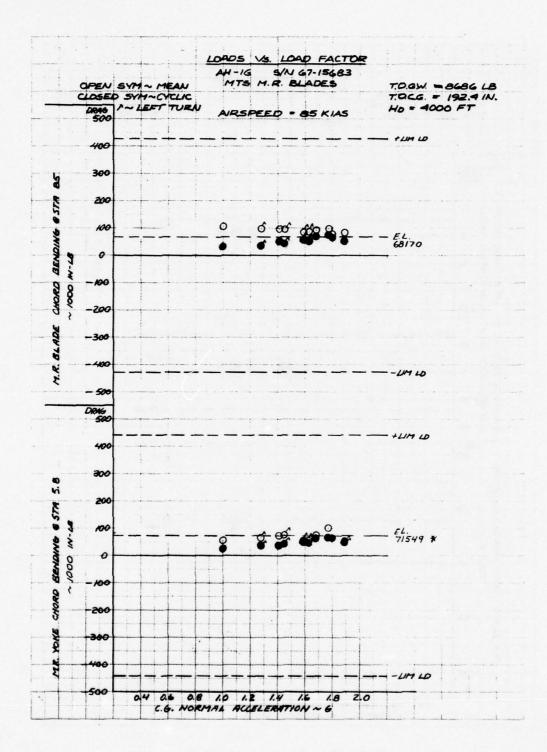


Figure E-2. Loads versus load factor - airspeed = 85 KIAS (Sheet 3 of 9).

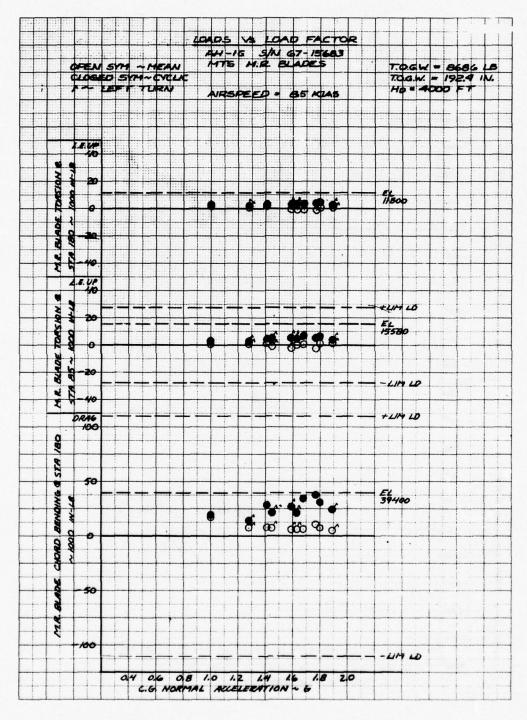


Figure E-2. Loads versus load factor - airspeed = 85 KIAS (Sheet 4 of 9).

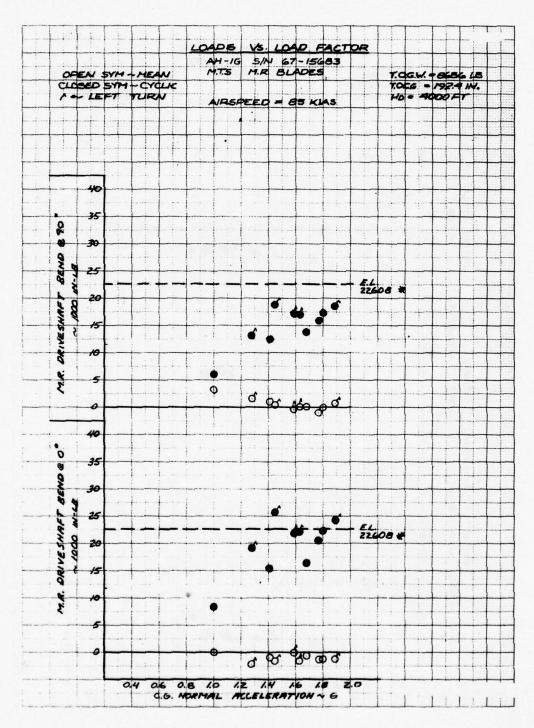


Figure E-2. Loads versus load factor - airspeed = 85 KIAS (Sheet 5 of 9).

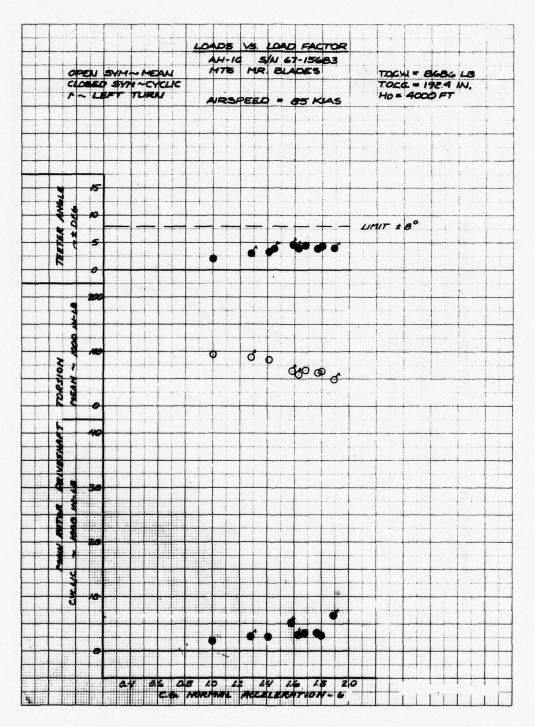


Figure E-2. Loads versus load factor - airspeed = 85 KIAS (Sheet 6 of 9).

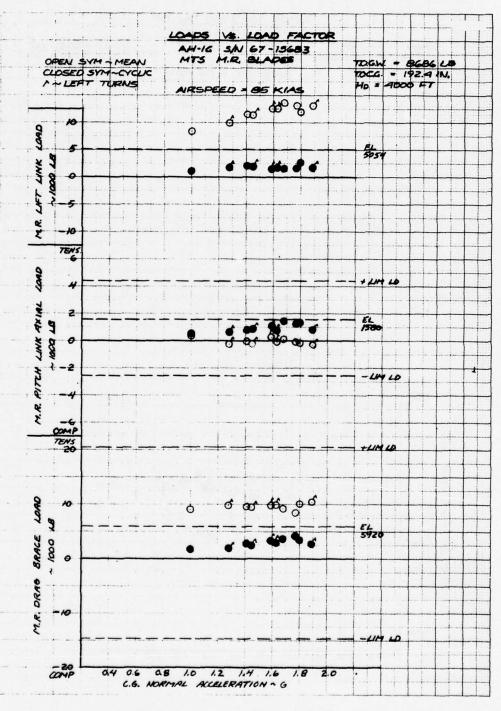


Figure E-2. Loads versus load factor - airspeed = 85 KIAS (Sheet 7 of 9).

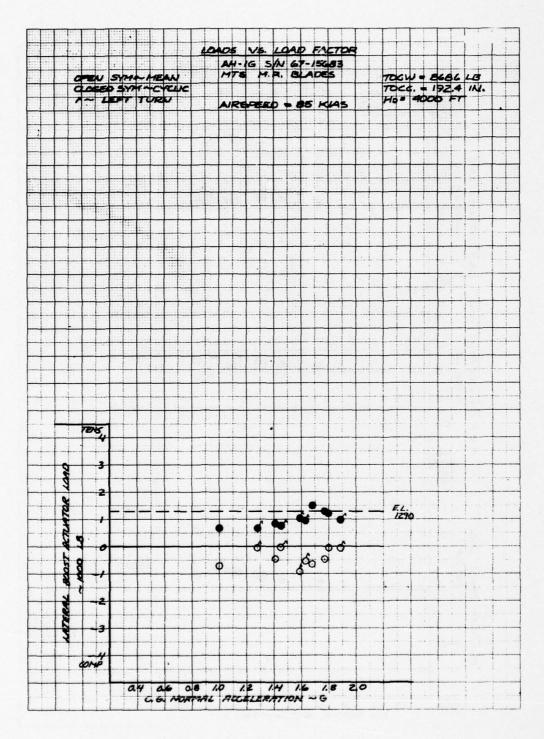


Figure E-2. Loads versus load factor - airspeed = 85 KIAS (Sheet 8 of 9).

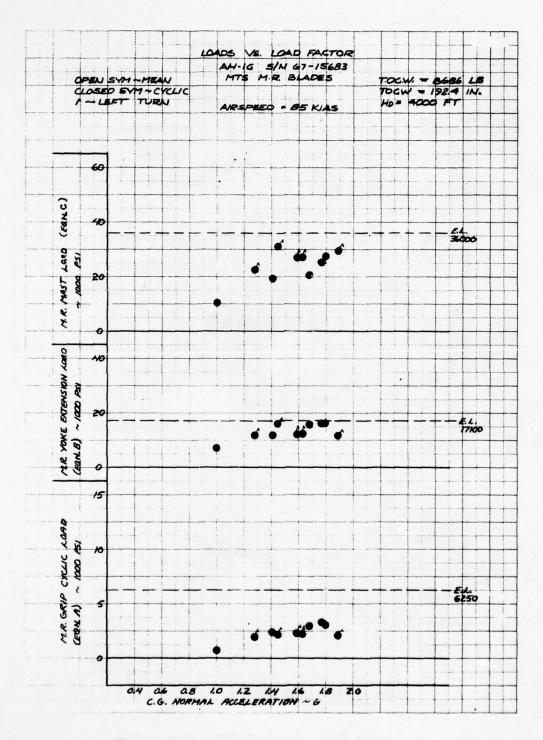


Figure E-2. Loads versus load factor - airspeed = 85 KIAS (Sheet 9 of 9).

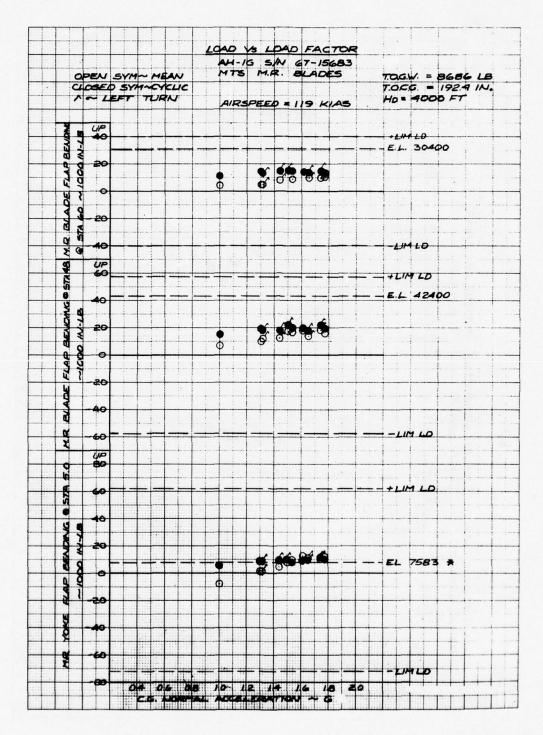


Figure E-3. Loads versus load factor - airspeed = 119 KIAS (Sheet 1 of 9).

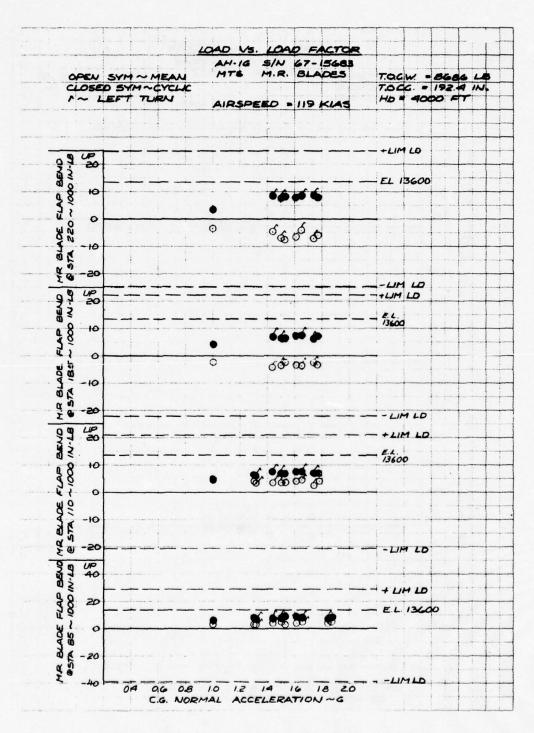


Figure E-3. Loads versus load factor - airspeed = 119 KIAS (Sheet 2 of 9).

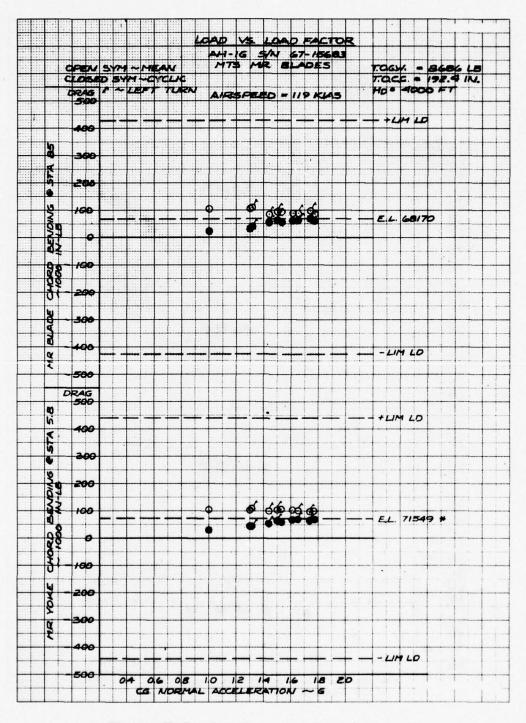


Figure E-3. Loads versus load factor - airspeed = 119 KIAS (Sheet 3 of 9).

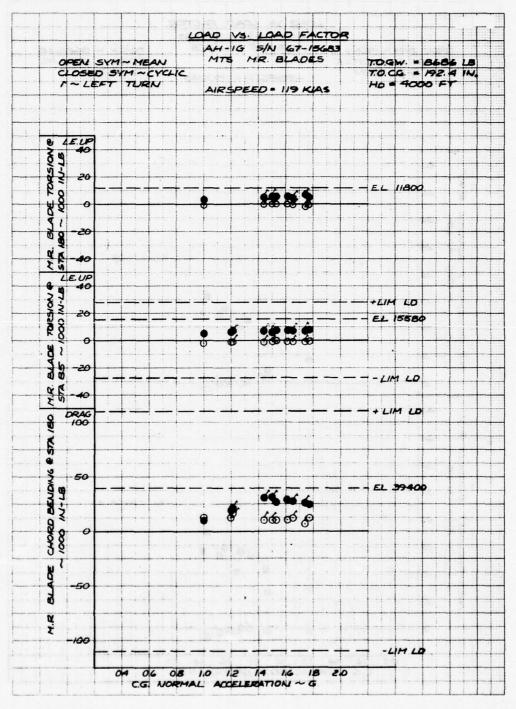


Figure E-3. Loads versus load factor - airspeed = 119 KIAS (Sheet 4 of 9).

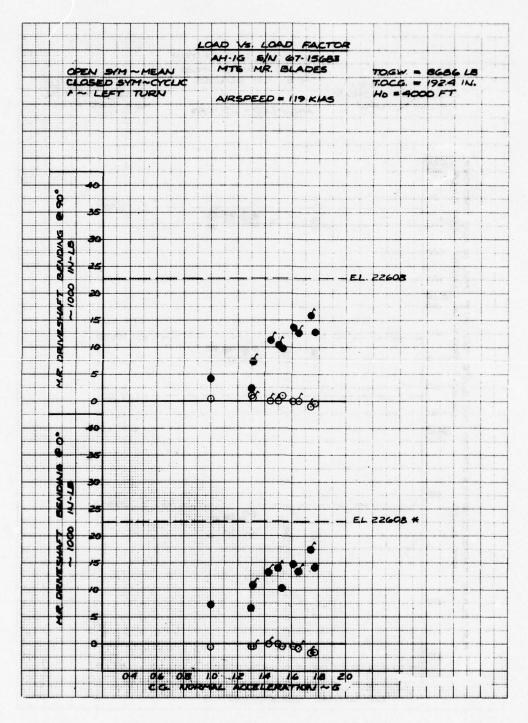


Figure E-3. Loads versus load factor - airspeed = 119 KIAS (Sheet 5 of 9).

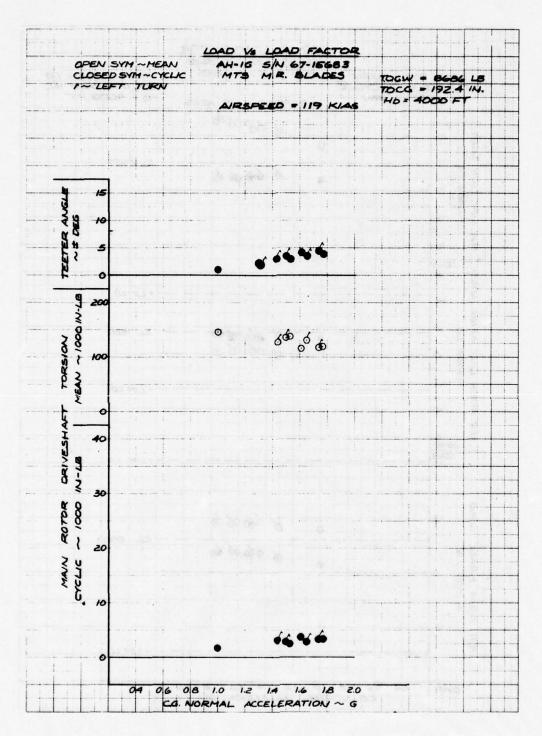


Figure E-3. Loads versus load factor - airspeed = 119 KIAS (Sheet 6 of 9).

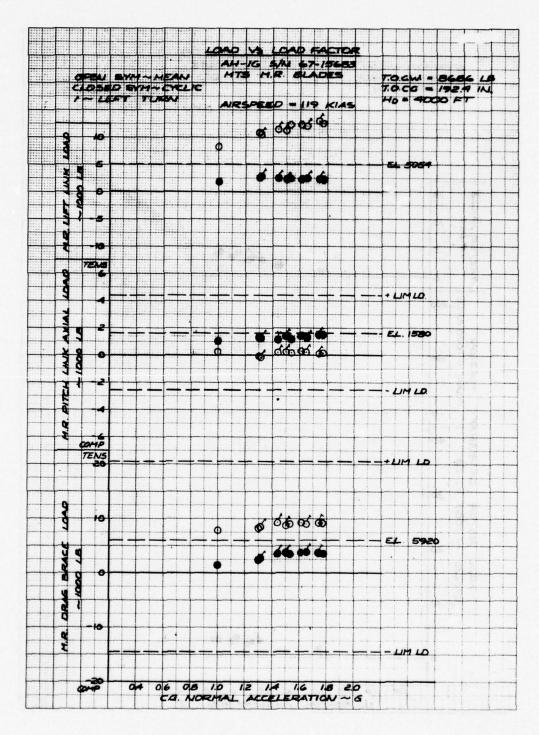


Figure E-3. Loads versus load factor - airspeed = 119 KIAS (Sheet 7 of 9).

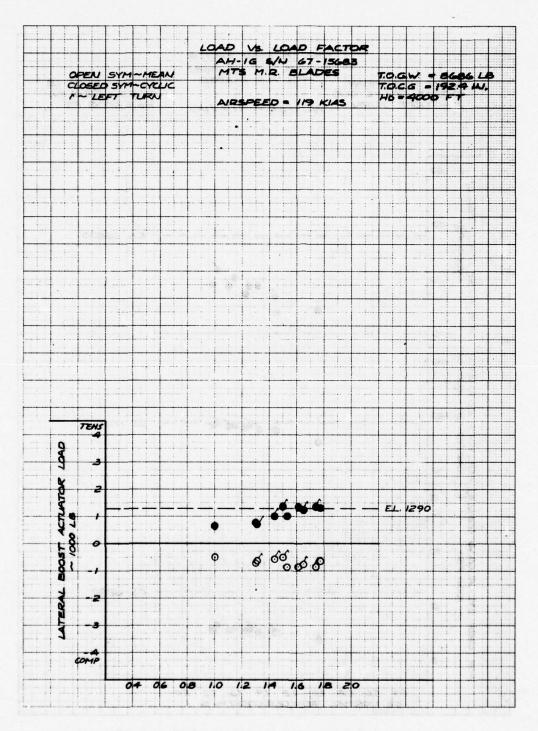


Figure E-3. Loads versus load factor - airspeed = 119 KIAS (Sheet 8 of 9).

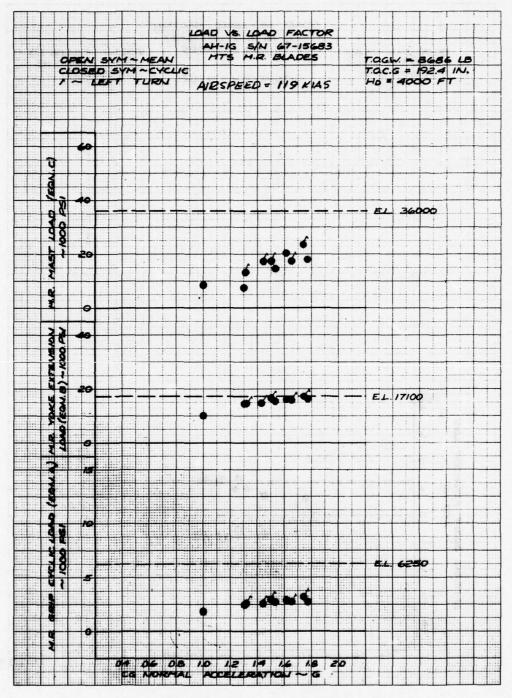


Figure E-3. Loads versus load factor - airspeed = 119 KIAS (Sheet 9 of 9).

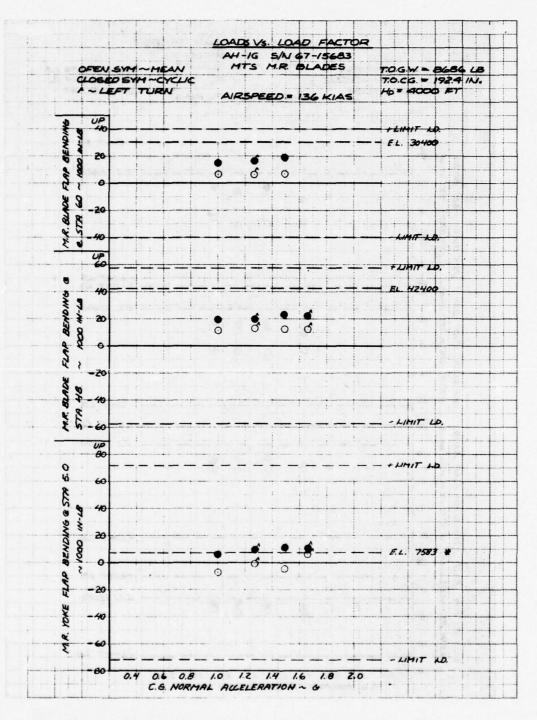


Figure E-4. Loads versus load factor - airspeed = 136 KIAS (Sheet 1 of 9).

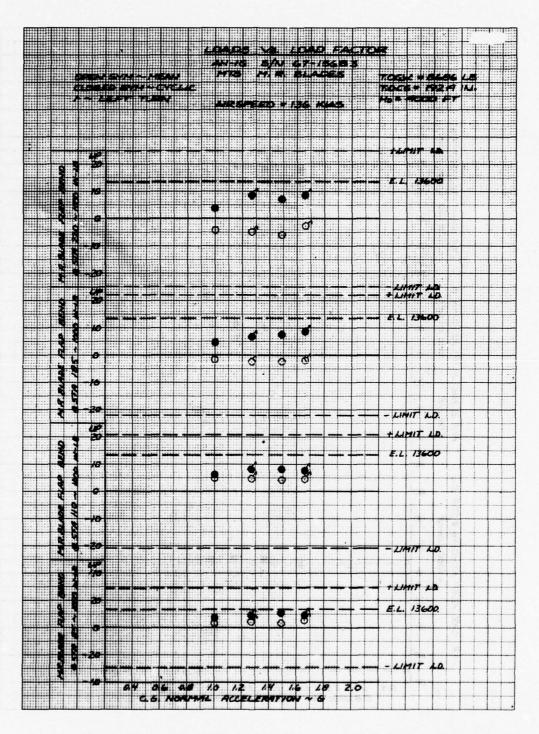


Figure E-4. Loads versus load factor - airspeed = 136 KIAS (Sheet 2 of 9).

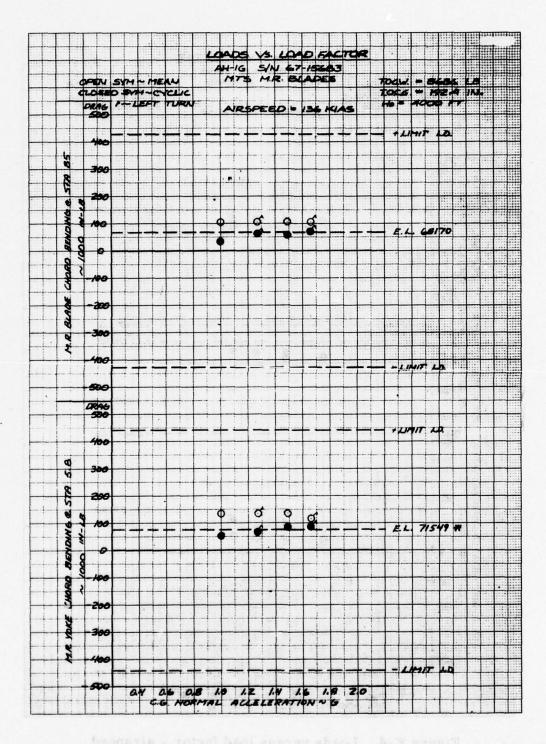


Figure E-4. Loads versus load factor - airspeed = 136 KIAS (Sheet 3 of 9).

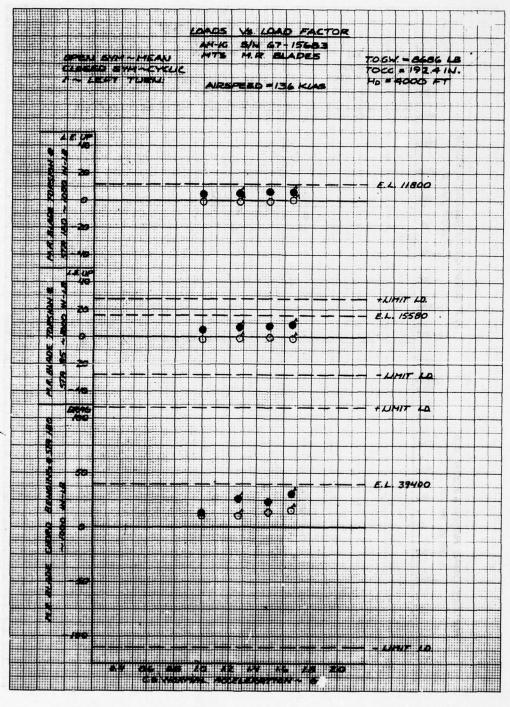


Figure E-4. Loads versus load factor - airspeed = 136 KIAS (Sheet 4 of 9).

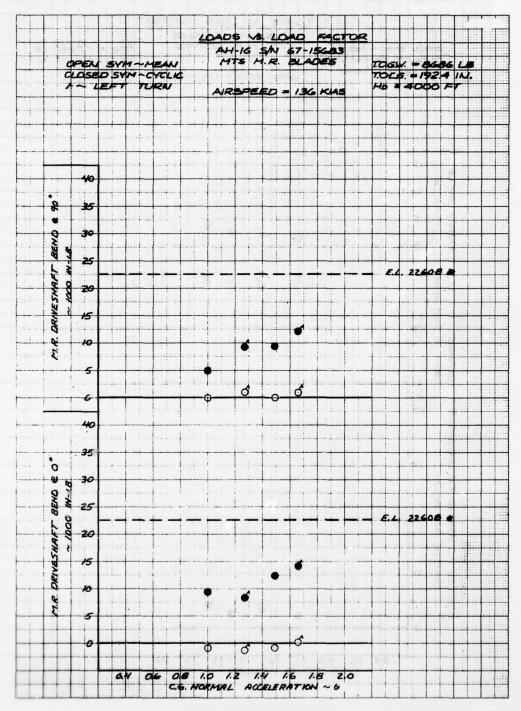


Figure E-4. Loads versus load factor - airspeed = 136 KIAS (Sheet 5 of 9).

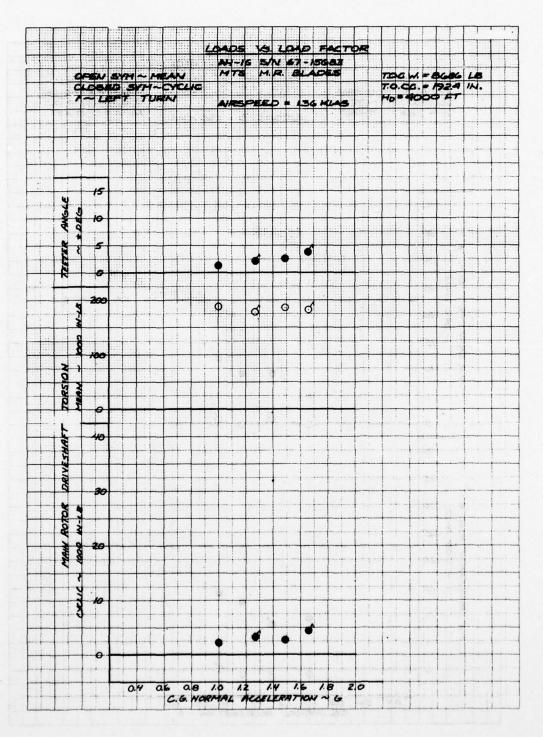


Figure E-4. Loads versus load factor - airspeed = 136 KIAS (Sheet 6 of 9).

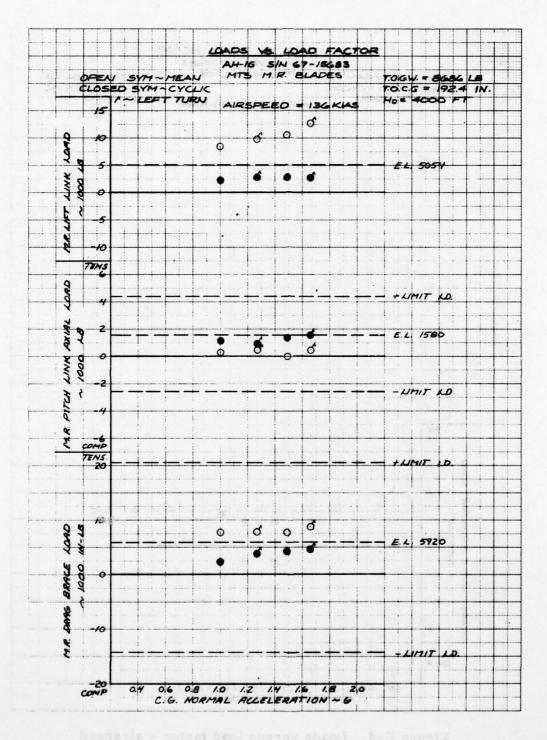


Figure E-4. Loads versus load factor - airspeed = 136 KIAS (Sheet 7 of 9).

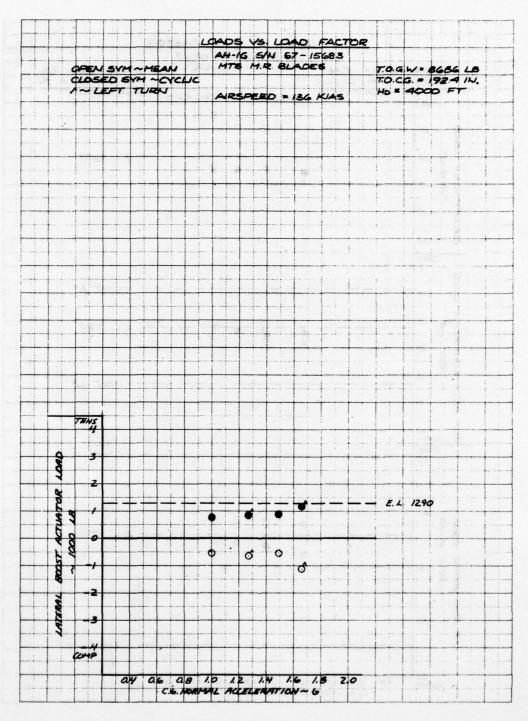


Figure E-4. Loads versus load factor - airspeed = 136 KIAS (Sheet 8 of 9).

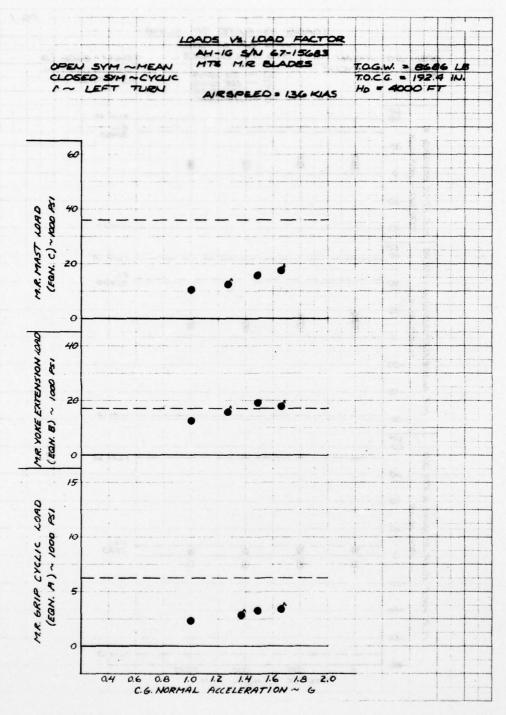


Figure E-4. Loads versus load factor - airspeed = 136 KIAS (Sheet 9 of 9).

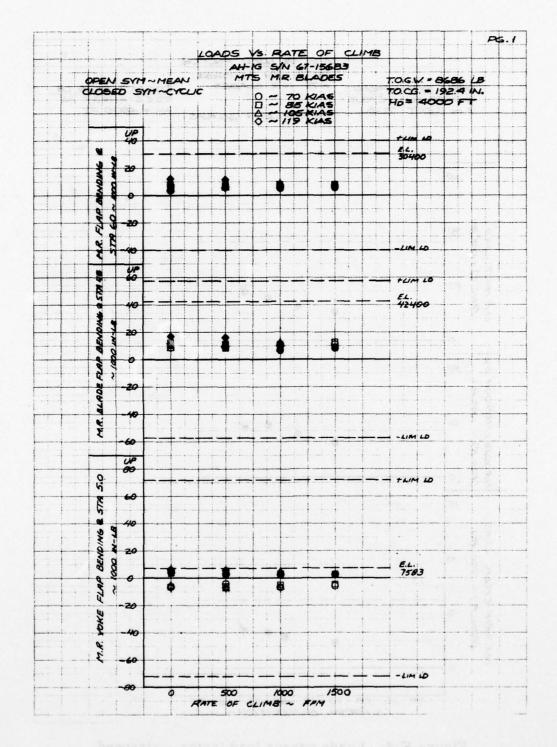


Figure E-5. Loads versus rate of climb (Sheet 1 of 8).

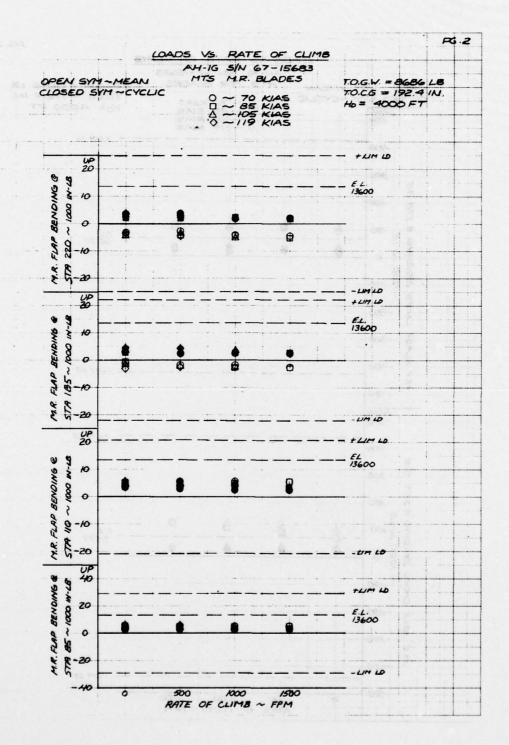


Figure E-5. Loads versus rate of climb (Sheet 2 of 8).

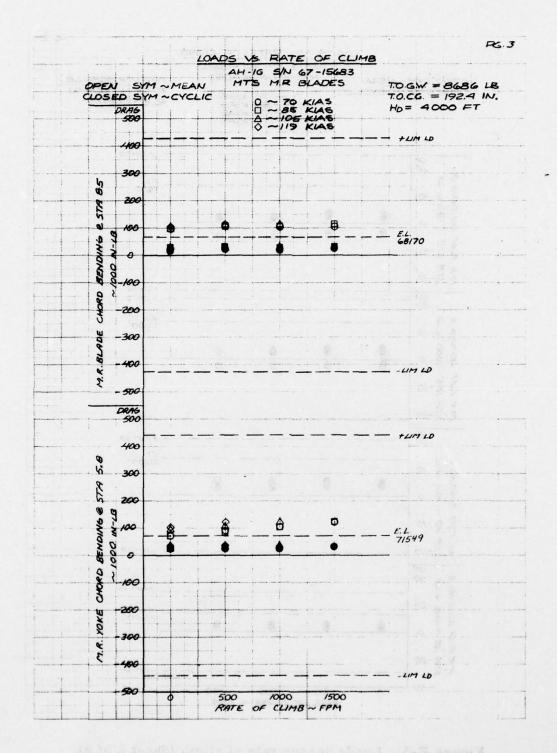


Figure E-5. Loads versus rate of climb (Sheet 3 of 8).

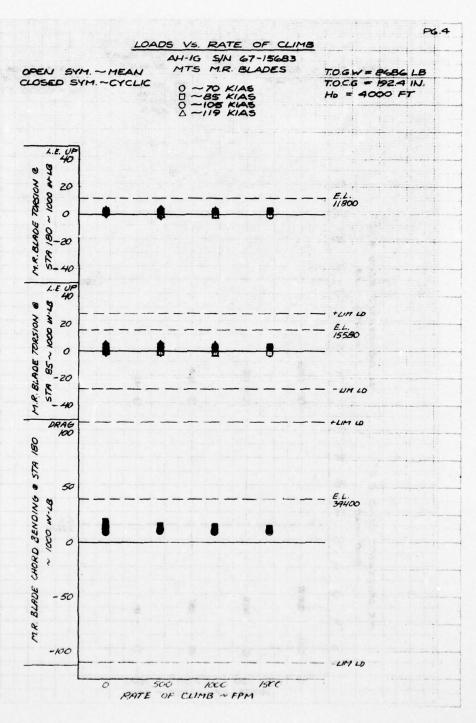


Figure E-5. Loads versus rate of climb (Sheet 4 of 8).

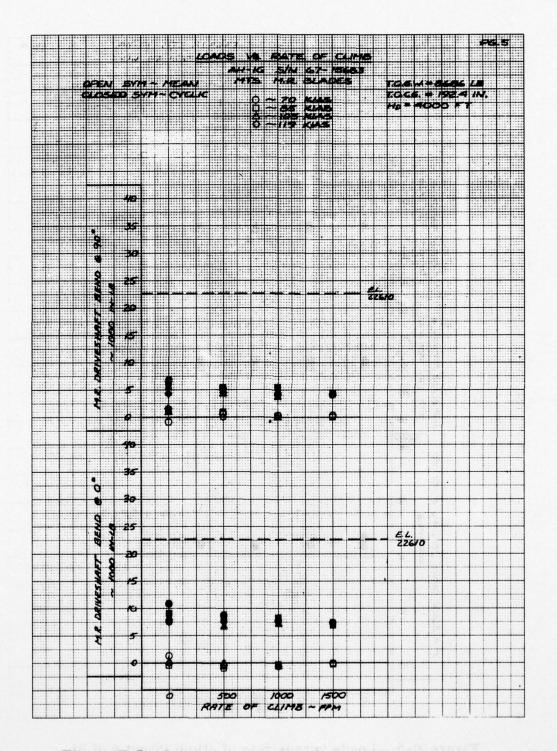


Figure E-5. Loads versus rate of climb (Sheet 5 of 8).

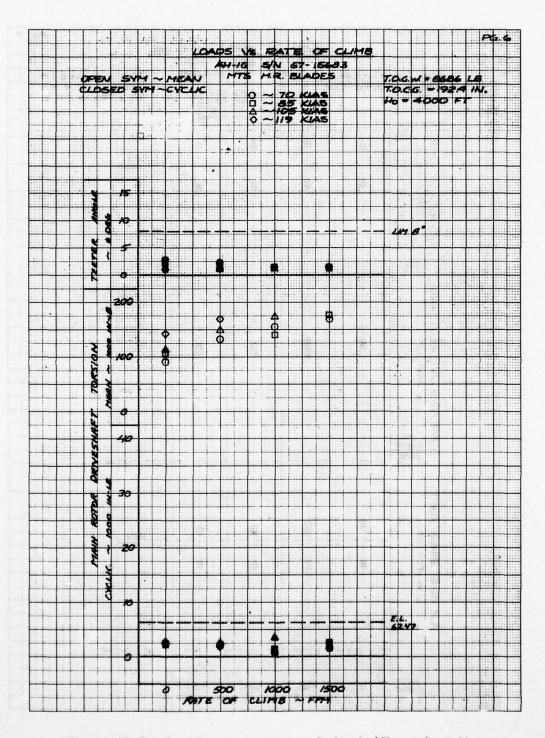


Figure E-5. Loads versus rate of climb (Sheet 6 of 8).

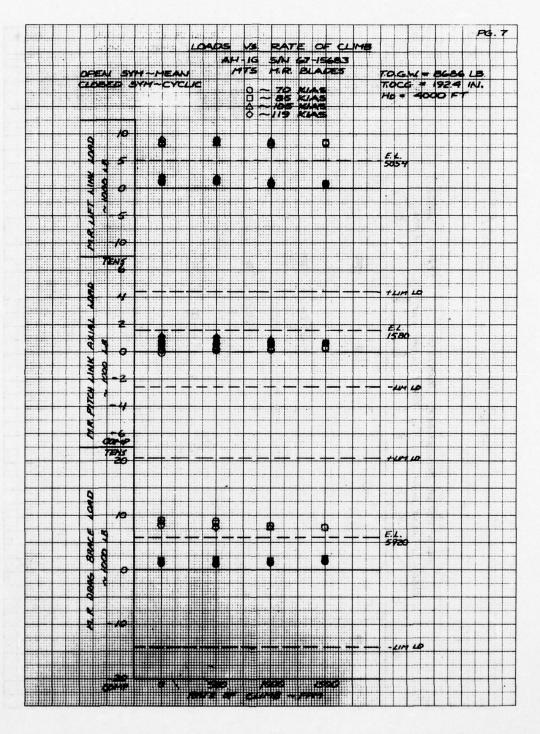


Figure E-5. Loads versus rate of climb (Sheet 7 of 8).

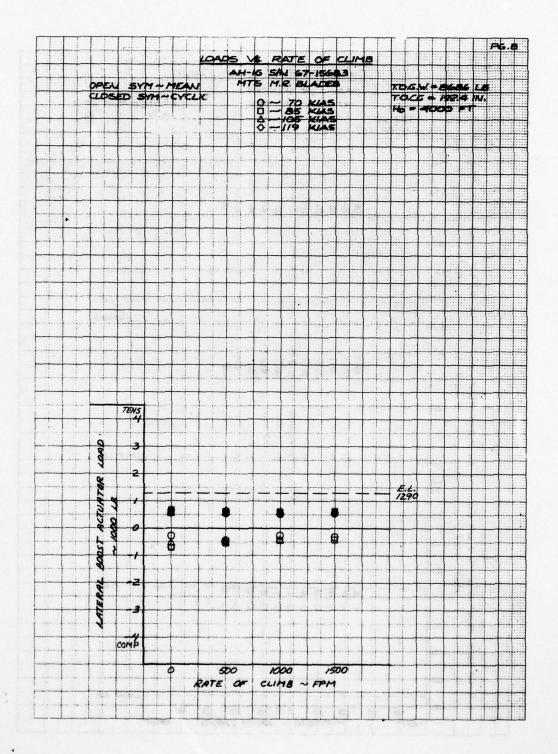


Figure E-5. Loads versus rate of climb (Sheet 8 of 8).

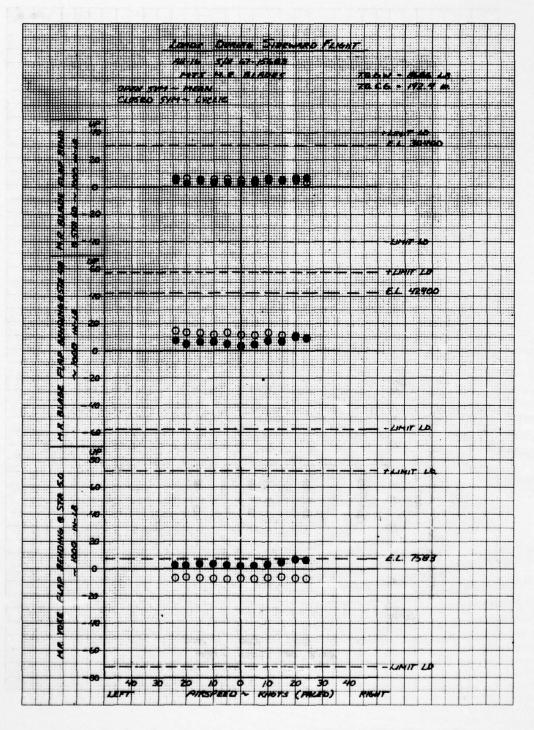
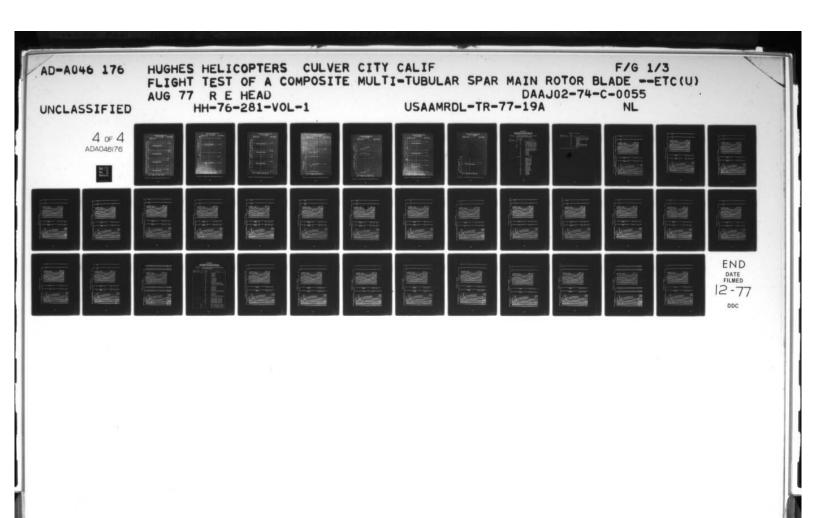


Figure E-6. Loads during sideward flight (Sheet 1 of 8).



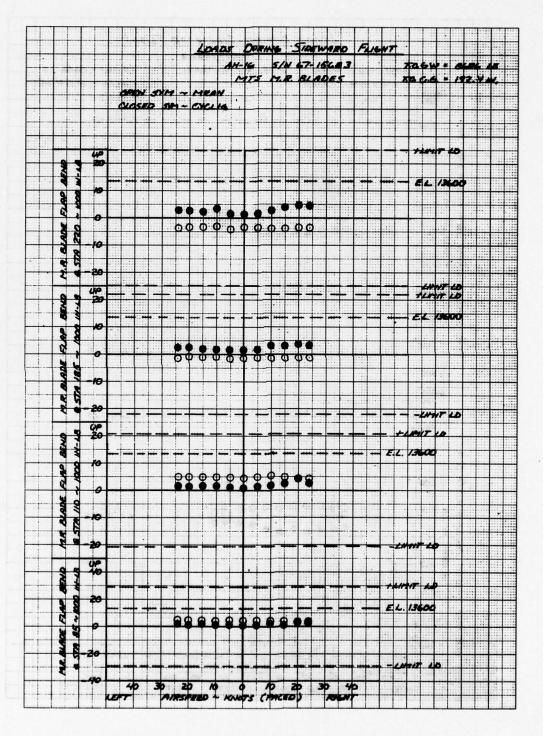


Figure E-6. Loads during sideward flight (Sheet 2 of 8).

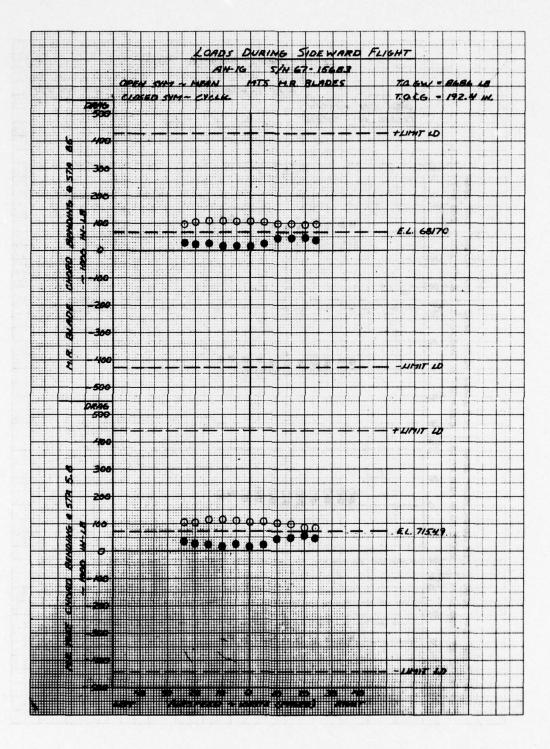


Figure E-6. Loads during sideward flight (Sheet 3 of 8).

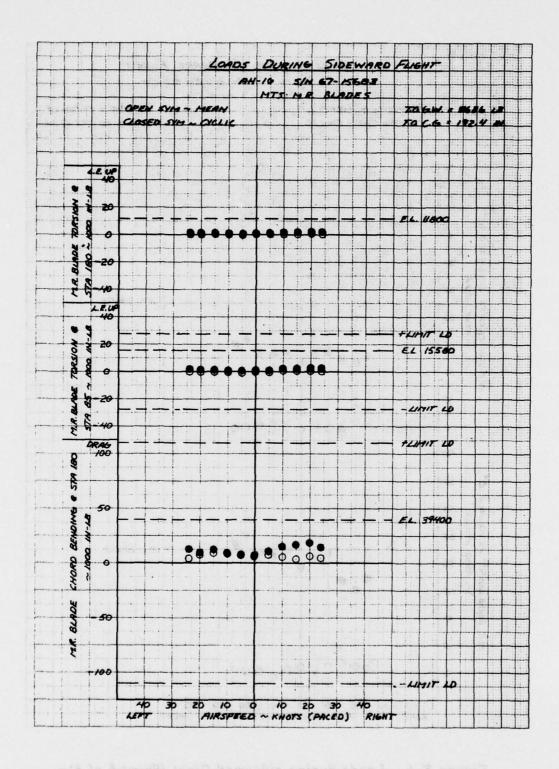


Figure E-6. Loads during sideward flight (Sheet 4 of 8).

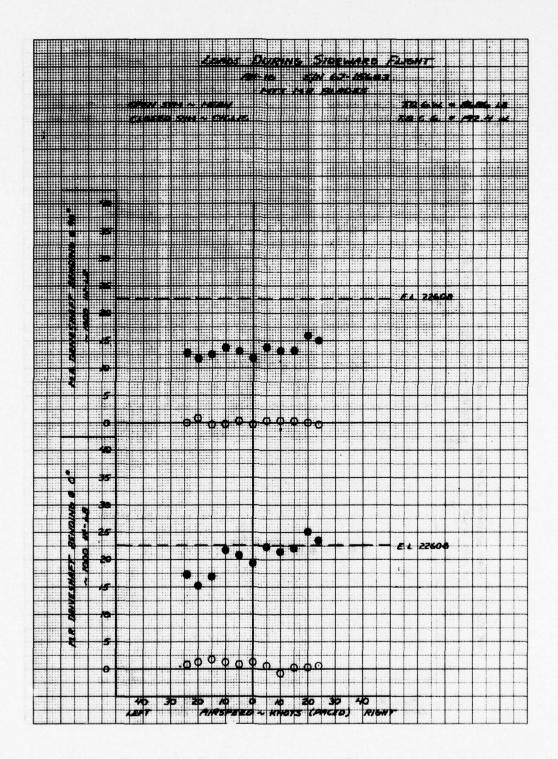


Figure E-6. Loads during sideward flight (Sheet 5 of 8).

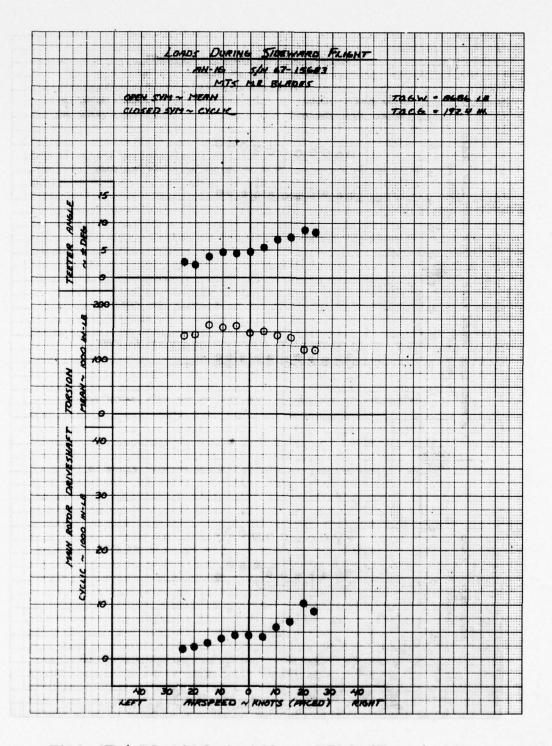


Figure E-6. Loads during sideward flight (Sheet 6 of 8).

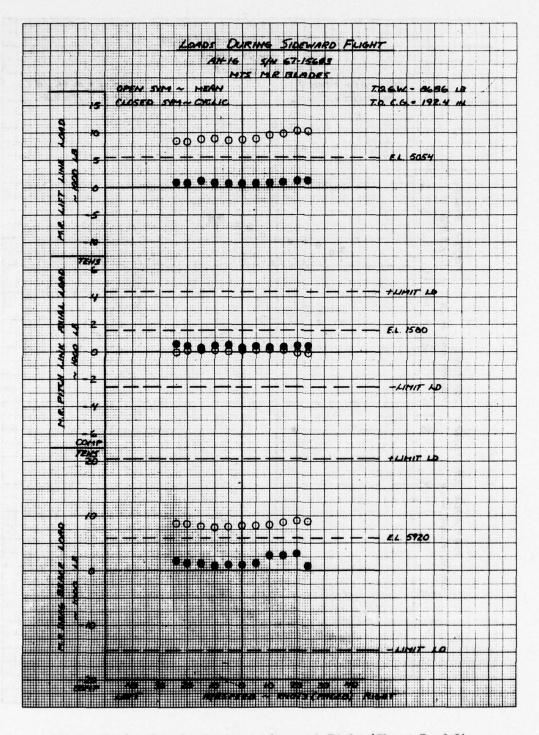


Figure E-6. Loads during sideward flight (Sheet 7 of 8).

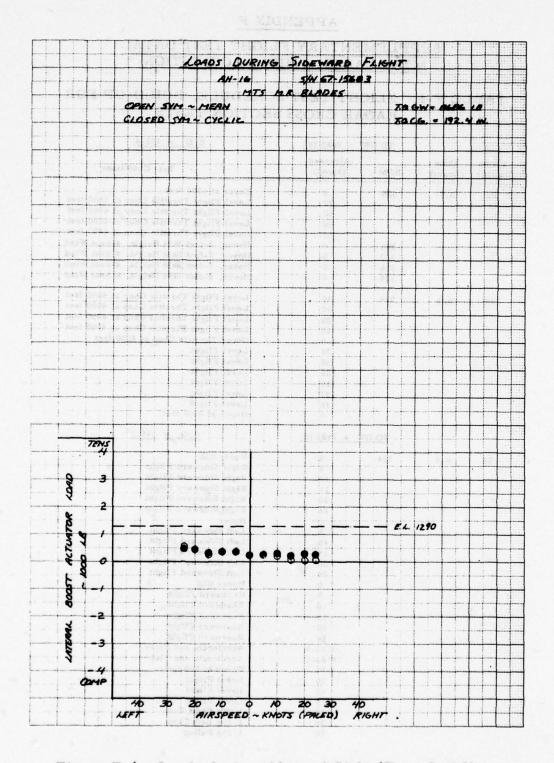


Figure E-6. Loads during sideward flight (Sheet 8 of 8).

APPENDIX F

SUPPLEMENTARY FLIGHT TEST DATA; MTS BLADES - MID-CG CONDITION

TABLE F-1. FLIGHT TEST SCHEDULE, BUILD-UP FOR RADAR CROSS SECTION TESTS

Flight	Time		Airspeed		
Number	(hours)	RPM	(knots)	Test Condi	tions
22	0.7	324	0	Hover at 4000 feet	
			70	Level Flight Throttle Chop	at 4000 feet
			60	Level Flight Throttle Chop	at 4000 feet
			50	Level Flight Throttle Chop	
			40	Level Flight Throttle Chop	
		294	0	Hover, 2-foot Skid Height,	
		300	0	Hover, 2-foot Skid Height,	
		314	0	Hover, 2-foot Skid Height,	
		324	0	Hover, 2-foot Skid Height,	
23	0.9	324	40	Level Flight Throttle Chop	at 4000 feet
-	,		30	Level Flight Throttle Chop	
			20	Level Flight Throttle Chop	
			10	Level Flight Throttle Chop	
			0	Hover Throttle Chop at 400	
			70		o leet
			85	Level Flight	
			105	Level Flight	
			119	Level Flight	
			127	Level Flight	
			136	Level Flight	
			0	Level Flight	
			•	Hover at 4000 feet	
		TO GW	≈ 8685 lb	C.G. = 195.9	
24	0.8	324	0	Hover IGE	
			5	Right Sideward Flight	
			10	Right Sideward Flight	
			15	Right Sideward Flight	
			20	Right Sideward Flight	
			24	Right Sideward Flight	
			0	Hover	
			5		
			10	Left Sideward Flight	
			15	Left Sideward Flight Left Sideward Flight	
			20	Left Sideward Flight Left Sideward Flight	
			24		
			0	Left Sideward Flight Hover IGE	
			5		
				Rearward Flight Rearward Flight	
			10		
			15	Rearward Flight	
			15 20	Rearward Flight Rearward Flight	
			15 20 24	Rearward Flight Rearward Flight Rearward Flight	
			15 20 24 0-40-0	Rearward Flight Rearward Flight Rearward Flight Accelerate and Flare	
			15 20 24 0-40-0 0-80-0	Rearward Flight Rearward Flight Rearward Flight Accelerate and Flare Accelerate and Flare	
			15 20 24 0-40-0 0-80-0 70	Rearward Flight Rearward Flight Rearward Flight Accelerate and Flare Accelerate and Flare Climb at 500 fpm	
			15 20 24 0-40-0 0-80-0 70	Rearward Flight Rearward Flight Rearward Flight Accelerate and Flare Accelerate and Flare Climb at 500 fpm Level Flight	
			15 20 24 0-40-0 0-80-0 70 70 85	Rearward Flight Rearward Flight Rearward Flight Accelerate and Flare Accelerate and Flare Climb at 500 fpm Level Flight Level Flight	
			15 20 24 0-40-0 0-80-0 70 70 85	Rearward Flight Rearward Flight Rearward Flight Accelerate and Flare Accelerate and Flare Climb at 500 fpm Level Flight Level Flight Level Flight	
			15 20 24 0-40-0 0-80-0 70 70 85	Rearward Flight Rearward Flight Rearward Flight Accelerate and Flare Accelerate and Flare Climb at 500 fpm Level Flight Level Flight	

TABLE F-1 - Continued

Flight Number	Time (hours)	RPM	Airspeed (knots)	Test Conditions
25	0.8	324	70	Climb at 1500 fpm
			70	Turn Reversal, 45° Left to 45° Right, Mild
			70	Turn Reversal, 45° Right to 45° Left, Mild
			105	Turn Reversal, 45° Left to 45° Right, Mild
			105	Turn Reversal, 45° Right to 45° Left, Mild
			70	1.5g Left Turn
			70	1.5g Right Turn
			70	1.5g Pullup
			105	1. 25g Left Turn
			105	1, 25g Right Turn
			105	1. 25g Pullup
			70	Level Flight, Throttle Chop at 4000 feet
			50	Level Flight, Throttle Chop at 4000 feet
			30	Level Flight, Throttle Chop at 4000 feet
			0	Hover
			105	Level Flight

This completed the envelope expansion for the R.C.S. tests.

AH-1G S/N 67-15683 HUGHES HELICOPTERS MULTI-TUBULAR SPAR ROTOR BLADES TABLE F-2.

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	TEST CONDITION MEAN. OSC. NO. TEST CONDITION MEAN.

TABLE F-2 - Continued

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1. CONT. REVERSAL - 119 KIAS
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1. LONT. 1339 RPM - 105 KIAS
1. LEFT SIDES.LIP - 70 KIAS
1. LEFT SIDES.LIP - 70 KIAS
1. LEFT SIDES.LIP - 136 KIAS
1. LEFT TURN - 119 KIAS
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1. LUNG RITE PUSHOUER - 70 ENDURANCE LIMIT 30400. - Continued IN-LB STR.60 UNITS IN HD- 4000 FT F-2 TABLE •0 NURTH START 0-100% NR
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LIMB 1000 FPM - 70 KIRS
LIMB 1000 FPM - 70 KIRS
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TABLE F-2 - Continued

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TABLE F-2 - Continued

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PARAMETER M.R. BLADE FLAP BENDING @ TOGM- 9685 LB TOCG- 195.9), TEST CONDITION	NORTH START 0-100% NR	-	HOUER IGE 324 RPM	. HOUER TURN, RIGHT 30 DEG/SEC	I, HOUER, F/A REVERSAL	70	SIDELARD FLIGHT - KIGHT	1. REARLIARD FLIGHT	LEVEL FLIGHT - 85 KIAS	LEUEL FLIGHT - 119 KIAS	1. LEVEL FLIGHT - 127 KIRS	CLIMB, 500 FPM - 70 KIRS	. CLIMB, 1900 FPM - 70 KIRS	CLIMB, 500 FPM - 85 KIAS	55	32	100 E	C ING.	Clieb EX.	LEFT TURN, 7	LEFT TURN.	٠.	RIGHT TURN, 70 KIRS		RIGHT TURN, 119 KIRS	P. P	TURN REVERSAL, MILD - 85 KIAS.	22.2	1084
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TABLE F-2 - Continued

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TABLE F-2 - Continued

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ģ z	MEGN.	စုစုစုစုခုရစုစုစုစု က်ပြုပ်မှုစုစုစုစုစုစုစုစုစုစုစုစုစုစုစုစုစုစုစ
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TABLE F-2 - Continued

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IN-LB ENDURANCE LIMIT 22610. STATIC	NO. TEST CONDITION	51. TURN REVERSAL, MOD. — 136 KIHS 52. CHT. CONT. REVERSAL — 119 KINS 53. CHT. CONT. REVERSAL — 119 KINS 54. DIR. CONT. REVERSAL — 119 KINS 55. PULLUP. LEVEL R. IGHT — 68 KIHS 56. PULLUP. LEVEL R. IGHT — 68 KIHS 57. PULLUP. LEVEL R. IGHT — 105 KIHS 66. PULLUP. LEVEL R. IGHT — 105 KIHS 66. PULLUP. LEVEL R. IGHT — 105 KIHS 66. STRB. AUTO. 324 RRH — 68 KIHS 67. TURN. R. IGHT — 70 KIHS 68. GATO TURN. R. IEFT — 70 KIHS 69. AUTO TURN. LEFT — 70 KIHS 77. LEFT SIDES.L P — 72 KIHS 77. LEFT SIDES.L P — 73 KIHS 77. LEFT SIDES.L P — 74 KIHS 77. LEFT SIDES.L P — 75 KIHS 77. LEFT SIDES.L P — 74 KIHS 77. LEFT SIDES.L P — 75 KIHS 77. LEF
HD= 4000 FT	OSC.	န် 611521 K 611521 K 72 10 10 10 10 10 10 10 10 10 10 10 10 10
	MEAN.	ခ်စ်ခ်စ်တို့ဝင်ခံခံခံရက်ကို ထို့ခံတို့တို့ခံခံခံစ်ခံခံခံခံခံခံခံခံခံခံခံခံခံခံခံခံ
PARAMETER M.R. MAST BENDING @ 90 DEG. TOGH- 8685 LB TOGG- 195.9 IN	NO. TEST CONDITION	1. NORPLE, START 0-100% NR. 3. NORPLE, STUDON 100-0% 3. NORPLE, TREEDER 4. JULP TAKEDER 5. HOVER 10ER 324 RPH 6. HOVER 10ER 10E 324 RPH 10. SIDELARD R. IGHT 30 DEG-SEC 10. HOVER 10ER REVERSAL 11. SIDELARD R. IGHT - LEFT 12. SIDELARD R. IGHT - LEFT 13. SEGREBARD R. IGHT - LEFT 14. EVEL R. IGHT - 102 KIRS 15. LEVEL R. IGHT - 119 KIRS 16. LEVEL R. IGHT - 127 KIRS 17. LEVEL R. IGHT - 126 KIRS 18. LEVEL R. IGHT - 126 KIRS 19. LEVEL R. IGHT - 126 KIRS 19. LEVEL R. IGHT - 126 KIRS 20. CLINB 500 FPH - 70 KIRS 22. CLINB 500 FPH - 70 KIRS 23. CLINB 500 FPH - 105 KIRS 24. CLINB 1000 FPH - 105 KIRS 25. CLINB 1000 FPH - 105 KIRS 26. CLINB 1000 FPH - 105 KIRS 27. CLINB 1000 FPH - 105 KIRS 28. CLINB 1000 FPH - 105 KIRS 29. CLINB 1000 FPH - 105 KIRS 20. CLINB 1000 FPH - 1000 FPH - 1000 KIRS 20. CLINB 1000 FPH - 1000 KIRS 20. CLINB 1000 FPH - 1000 KIRS 20. CLINB 1000 FPH - 105 KIRS 20. CLINB 1000 FPH - 1000 FPH - 1000 KIRS 20. CLINB 1000 FPH - 1000 FPH - 1000 KIRS 20. CLINB 1000 FPH - 1000 FPH - 1000 FPH - 1000 KIRS 20. CLINB 1000 FPH - 1000 FPH - 1000 KIRS 20. CLINB 1000 FPH - 1000 FPH - 1000 KIRS 20. CLINB 1000 FPH - 1000 FPH - 1000 FPH - 1000 KIRS 20. CLINB 1000 FPH - 1000 FPH - 1000 FPH - 1000 KIRS 20. CLINB 1000 FPH - 1000 FPH - 1000 FPH - 1000 FPH - 1000 KIRS 20. CLINB 1000 FPH - 1

TABLE F-2 - Continued

	OSC.	ମୁ ଜୁବ୍ୟୁ ହ୍ୱି ପ୍ରତ୍ତ୍ୱତ୍ତ୍ତ୍ତ୍ତ୍ତ୍ତ୍ତ୍ତ୍ତ୍ତ୍ତ୍ତ୍ତ୍ତ୍ତ୍ତ
STATIC LIMITS	MEAN.	ବ୍ରବ୍ୟକ୍ତି ପ୍ରତ୍ତ୍ର ବ୍ରବ୍ୟ ବ୍ରବ୍ୟ ମଧ୍ୟ ପ୍ରତ୍ତିକ ବ୍ରବ୍ୟ ବ୍ୟ ବ୍ୟ ବ୍ୟ ବ୍ୟ ବ୍ୟ ବ୍ୟ ବ୍ୟ ବ୍ୟ ବ୍ୟ
ENDURANCE LIMIT 5054. STATII	TEST, CONDITION	TURN REVERSAL, MOD. – 136 KIRS F/A CONT. REVERSAL – 119 KIRS DIR. CONT. REVERSAL – 119 KIRS PULLUP, LEVEL FIGHT – 87 KIRS PULLUP, LEVEL FIGHT – 126 KIRS PULLUP, LEVEL FIGHT – 127 KIRS PULLUP, LEVEL FIGHT – 127 KIRS PULLUP, LEVEL FIGHT – 127 KIRS FULLUP, LEVEL FIGHT – 126 KIRS FULLUP, LEFT – 126 KIRS FULLUP, LEFT – 126 KIRS FULLUP, LEFT – 126 KIRS FULLUP, LEVEL FIGHT – 126 KIRS FULLUP, LEFT – 126 KIRS FULLUP, L
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- 4000 FT	.080	ရှိရှိရှိရှိရှိရှိရှိရှိရှိရှိရှိရှိရှိရ
Ŷ	MEAN.	6 4 116.88 6 8 8 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
PARAMETER THRUST LINK LOAD TOGAL* 8685 LB TOCS* 195.9 IN	NO. TEST CONDITION	1. NORMAL START 0-100% NR. 3. NORMAL START 0-100% NR. 4. JUNP TAKEDFF 5. HOUER 10R, 34 RPH 10. FIDERARY 10R, 18FF 30 DEG-SEC 6. HOUER 10R, 18FF 30 DEG-SEC 7. HOUER 10R, 18FF 30 DEG-SEC 10. SIDERARY RIGHT 30 DEG-SEC 10. SIDERARY RIGHT 30 DEG-SEC 10. SIDERARY RIGHT - LEFT 12. SIDERARY RIGHT - REVERSAL 13. SIDERARY RIGHT - REVERSAL 14. EVE. RIGHT - 102 KIRS 15. EVE. RIGHT - 102 KIRS 16. EVE. RIGHT - 102 KIRS 17. EVE. RIGHT - 103 KIRS 18. EVE. RIGHT - 103 KIRS 22. CLIMB, 1000 FPH - 70 KIRS 23. CLIMB, 1000 FPH - 70 KIRS 24. CLIMB, 1000 FPH - 85 KIRS 25. CLIMB, 1000 FPH - 105 KIRS 26. CLIMB, 1000 FPH - 105 KIRS 27. CLIMB, 1000 FPH - 105 KIRS 28. CLIMB, 1000 FPH - 105 KIRS 29. CLIMB, 1000 FPH - 100 KIRS 20.

TABLE F-2 - Continued

	OSC.	ବ୍ରତ୍ତ୍ର ମୃତ୍ତ୍ର ବ୍ରତ୍ତ୍ରତ୍ତ୍ର ବ୍ରତ୍ତ୍ରତ୍ତ୍ରତ୍ତ୍ରତ୍
STRTIC LIMITS	MERN.	ବ୍ୟୁ ବ୍ୟୁ ବ୍ୟୁ ବ୍ୟୁ ବ୍ୟୁ ବ୍ୟୁ ବ୍ୟୁ ବ୍ୟୁ
ENDURANCE LIMIT 1290. STATIC	TEST CONDITION	TURN REVERSAL, MOD 136 KIAS FA CONT. REVERSAL - 119 KIAS DIR. CONT. REVERSAL - 119 KIAS DIR. CONT. REVERSAL - 119 KIAS PULLUP, LEVEL R.164T - 86 KIAS PULLUP, LEVEL R.164T - 105 KIAS PULLUP, LEVEL R.164T - 127 KIAS STARB AUTO, 324 RPH - 165 KIAS STARB AUTO, 324 RPH - 165 KIAS STARB AUTO, 324 RPH - 165 KIAS STARB AUTO, 339 RPH - 165 KIAS STARB AUTO, 339 RPH - 165 KIAS AUTO TURN, RIGHT - 70 KIAS CHOT TURN, RIGHT - 70 KIAS FILET SIDESLIP - 26 KIAS FILET SIDESLIP - 126 KIAS FILET SIDESLIP - 136 KIAS FILET SIDES
	2	4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.
4000 FI	.08C	සු අත්තුලය යු දු වූ දූ වූ දූ අතුතුතුම් දෙන්නේ සිදුන් සිදුන් සුවුන් සුවුන් සුවුන් සුවුන් සිදුන් සිදු
IN HD= 4000	MEAN.	ရစ္စစ္စစ္ကုန္ကိုစ္စစ္စစ္ခတ္ခ် မို႕မိုင္ငံစစ္စစ္စစ္ကိုစ္ခတ္ခ်စ္စစ္စစ္စစ္စစ္စစ္စစ္စစ္စစ္စစ္စစ္တစ္ခတ္ခ်စ္ခတ္ခ်စ္ခစ္စစ္ခတ္ခု မိုက္ခ်စ္ခစ္ခစ္ခတ္ခု မိုင္ငံစစ္ခစ္ခတ္ခ်စ္ခတ္ခတ္ခ်စ္ခတ္ခရစ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခရစ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခံစစ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္မွတ္ခတ္ခ်စ္မွတ္ခ်စ္ခတ္ခ်စ္ခတ္ခ်စ္မွတ္ခ်စ္ခတ္ခ်စ္မွတ္ခ်စ္မွတ္ခ်စ္မွတ္ခတ္ခ်စ္မွတ္ခ်စ္တစ္ခတ္ခ်စ္မွတ္ခ်စ္မွတ္ခ်စ္မွတ္ခ်စ္မွတ္ခ်စ္တစ္မွတ္ခတ္ခ်စ္မွတ္ခ်စ္မွတ္ခ်စ္မွတ္ခ်စ္မွတ္ခ်စ္မွတ္ခ်စ္မွတ္ခ်စ္မွတ္ခ်စ္တစ္မွတ္ခ်စ္မွတ္မွတ္မွတ္မွတ္မွတ္မွတ္မွတ္မွတ္မွတ္မွတ
PARAMETER LATERAL ACTUATOR LOAD TUGH= 8685 LB TOC6= 195.9 J	NO. TEST CONDITION	1. NORTH, START 0-100% NR. 2. NORTH, TAKEDER 4. JUNP TAKEDER 5. HOURR NIGHT 30 DEG-SEC 6. HOURR NIGHT 30 DEG-SEC 7. HOURR NIGHT 30 DEG-SEC 8. HOURR NIGHT 30 DEG-SEC 10. HOURR NIGHT 30 DEG-SEC 11. SIDELARD R. IGHT - REVIESSAL 11. SIDELARD R. IGHT - REVIESSAL 12. SIDELARD R. IGHT - REVIESSAL 13. REARLARD R. IGHT - REVIESSAL 14. LEVEL R. IGHT - REVIESSAL 15. LEVEL R. IGHT - 119 KIRS 16. LEVEL R. IGHT - 126 KIRS 17. LEVEL R. IGHT - 126 KIRS 18. LEVEL R. IGHT - 126 KIRS 19. LEVEL R. IGHT - 126 KIRS 22. CLIMB 1000 FFM - 70 KIRS 22. CLIMB 1000 FFM - 85 KIRS 22. CLIMB 1000 FFM - 85 KIRS 23. CLIMB 1000 FFM - 105 KIRS 24. CLIMB 1000 FFM - 105 KIRS 25. CLIMB 1000 FFM - 105 KIRS 26. CLIMB 1000 FFM - 105 KIRS 27. CLIMB 1000 FFM - 105 KIRS 28. CLIMB 1000 FFM - 105 KIRS 29. CLIMB 1000 FFM - 105 KIRS 29. CLIMB 1000 FFM - 105 KIRS 29. LEFT TURN, 127 KIRS 20. LEFT TURN, 136 KIRS 20. LEFT TURN, 136 KIRS 20. LEFT TURN, 137 K

TABLE F-2 - Continued

	OSC.	ବ୍ରତ୍ତ ମହ୍ନ ପ୍ରତ୍ତ୍ୱର ବ୍ରତ୍ତ ବ
STATIC LIMITS	MEAN.	8 11 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
ENDURANCE LIMIT 38980. STATIC	TEST CONDITION	TURN REVERSAL, NOD 136 KIAS LAT. CONT. REVERSAL - 119 KIAS LAT. CONT. REVERSAL - 119 KIAS PULLUP, LEVEL R. 16HT - 98 KIAS PULLUP, LEVEL R. 16HT - 98 KIAS PULLUP, LEVEL R. 16HT - 198 KIAS PULLUP, DIVE - 136 KIAS PULLUP, LEVEL R. 16HT - 127 KIAS PULLUP, DIVE - 136 KIAS STAB AUTO, 324 RPH - 68 KIAS AUTO PUR, REDOVERY - 70 KIAS STAB AUTO, 24 RPH - 68 KIAS AUTO PUR, REDOVERY - 70 KIAS STAB AUTO, 24 RPH - 68 KIAS BUTO PUR, REDOVERY - 136 KIAS DIVE, STEEDY - 136 KIAS DIVE, STEEDY - 136 KIAS DIVE, RIGHT TURN - 119 KIAS DIVE, RIGHT TURN - 119 KIAS DIVE, R. TURN PULLUP - 136 KIAS DIVE,
IN-LB	Ş	<u>፞</u> ĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸĸ
HD- 4000 FT	OSC.	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
Z	MEAN.	1512289999999999999999999999999999999999
PARAMETER M.R. DRIVESHAFT TORSION TOGA- 8685 LB TOCG- 195.9	NO. TEST CONDITION	1. NURTH. START 0-100% NR. 3. NURTH. TAKEDEF 5. HUER TAKEDEF 6. HUER TAKEDEF 7. HUER TAKEDEF 8. HUER TAKEDEF 10. HUER TAKEDEF 11. SUDE, RICH 130 DEG-SEC 11. SUDE, RICH 130 KIRS 11. LEVEL R. IGHT 130 KIRS 12. CLIMB 1000 FFM - 70 KIRS 13. LEVEL R. IGHT 130 KIRS 13. CLIMB 1000 FFM - 105 KIRS 14. LEVEL R. IGHT 1000 FFM - 105 KIRS 15. CLIMB 1000 FFM - 105 KIRS 10. CLIMB 1000 FFM - 1000 FFM - 105 KIRS 10. CLIMB 1000 FFM - 1000 FFM - 1000 FFM - 1000 KIRS 10. CLIMB 1000 FFM - 1

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LIMITS	MEAN.	88888888888888888888888888888888888888
ENDURRACE LIMIT STATIC LIMITS	TEST CONDITION	TURN REVERSAL, MOD 136 KIHS F.A CONT. REVERSAL - 119 KIHS FULLUP. LEVEL. R. 1641 - 70 KIHS FULLUP. LEVEL. R. 1641 - 70 KIHS FULLUP. LEVEL. R. 1641 - 165 KIHS FULLUP. LEVEL. R. 1641 - 165 KIHS FULLUP. LEVEL. R. 1641 - 177 KIHS FULLUP. LEVEL. R. 1641 - 177 KIHS FULLUP. LEVEL. R. 1641 - 178 KIHS FULLUP. DIVE - 136 KIHS STAB. AUTO. 324 RPH - 85 KIHS STAB. AUTO. 324 RPH - 85 KIHS STAB. AUTO. 324 RPH - 85 KIHS STAB. AUTO. 329 RPH - 85 KIHS STAB. AUTO. 329 RPH - 85 KIHS FULLUP. DIVE. LEFT TO KIHS FULLUP. DIVE. REDOVER OF REPORT OF REP
DEG.	ż	෬෭෦෭෬෭෦෭෦෭෦෭෦෭෦෦෦෦෦෦෦෦෦෦෦෦෦෦෦෦෦෦෦෦෦෦෦෦
UNITS HD= 4000 FT	OSC.	ଡ଼ଡ଼ଡ଼୳ଡ଼ଡ଼ଡ଼ଡ଼୰୳୴୴ଡ଼ଡ଼୰ୠଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼୰୷ଡ଼ଡ଼ଡ଼ୣ୶ୠ୷ଡ଼୷ଡ଼୷ଡ଼୷ଡ଼ୄ ୡୡଌୢୡୄ୷ୡୡୡୡୡ୷୷୴ଡ଼ଢ଼ଡ଼ୠଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼୰୷ଡ଼ଡ଼ଡ଼ୣ୶ଡ଼୷ଡ଼୷ଡ଼୷ଡ଼ୡୄ ୡୡଌୡୄ୷ୡୡୡୡୡୡ୷୷୷ୡ୷୷ୡୡୡୢଌୡୡୡୡୡୡୡୡୡୡୡୡୡୡୡୡୡ
STATES	MEAN.	88888888888888888888888888888888888888
PARAMETER TEETER ANGLE TOGA - 8685 LB TOCG 195.9 IN	NO. TEST CONDITION	1. NORTH, START 0-100% NR. 1. NORTH, START 0-100% NR. 1. NORTH, TAKEDF 1. LUNP TAKEDF 1. HUNER TURN, LEFT 30 DEG-SEC 1. LUNG TURN, LEFT 119 KINS 2. LUNG TURN, LOS FING 2. LUNG SEO FFM - 20 KINS 2. LUNG SEO FFM - 105 KINS 2. LUNG TURN, BOTE 115 KINS 3. LUNG TURN, BOTE 115 KINS 3. LEFT TURN, BOTE 115 KINS 4. KINSTON TURN, BOTE 115 KINS 4. KINSTON TURN, BOTE 115 KINSTON 4. LOS KINSTON 4. LOS KINSTON 4. LOS KINSTON 4. LOS KINSTON 5.

APPENDIX G

SUPPLEMENTARY FLIGHT TEST DATA; 540 BLADES - FORWARD CG CONDITION

TABLE G-1. FLIGHT TEST SCHEDULE SUPPLEMENTARY 540 BLADE PROGRAM

Flight Number	Time (hours)	RPM	Airspeed (knots)	Test Condition
30	1.3	324	68	Level Flight
			85	Level Flight
			105	Level Flight
			119	Level Flight
			127	Level Flight
			136	Level Flight
			85	1.25g Right Turn
			85	1.60g Right Turn
			85	1.90g Right Turn
			85	1.25g Left Turn
			85	1.60g Left Turn
			85	1.90g Left Turn
			85	Turn Reversal, Left to Right, Mild
			85	Turn Reversal, Right to Left, Mild
			85	Turn Reversal, Left to Right, Moderate
			85	Turn Reversal, Right to Left, Moderate
			119	1.25g Right Turn
			119	1.50g Right Turn
			119	1.80g Right Turn
			119	1.25g Left Turn
			119	1.50g Left Turn
			119	1.80g Left Turn
			119	Turn Reversal, Left to Right, Moderate
			119	Turn Reversal, Right to Left, Moderate
			136	1.25g Right Turn
			136	1.50g Right Turn
			136	1.25g Left Turn
			136	1.50g Left Turn
			136	Turn Reversal, Left to Right, Moderate
			136	Turn Reversal, Right to Left, Moderate
31	0.8	324	70	Airspeed Calibration, West to East
			70	Airspeed Calibration, East to West
			86	Airspeed Calibration, West to East
			85	Airspeed Calibration, East to West
			119	Airspeed Calibration, West to East
			120	Airspeed Calibration, East to West
			136	Airspeed Calibration, West to East
			136	Airspeed Calibration, East to West
		324	0	Hover, 2-foot Skid Height, 4-knot Wind
		314	0	Hover, 2-foot Skid Height, 4-knot Wind
		304	0	Hover, 2-foot Skid Height, 4-knot Wind
		294	0	Hover, 2-foot Skid Height, 4-knot Wind
		324.	0	Hover, 2-foot Skid Height, 4-knot Wind

TABLE G-2. AH-1G S/N 67-15683 540 METAL BLADES

+-71987.	980.	ස්දුරුවල් දෙවැන් දෙව බවාදී සිට දෙවැන්
STATIC LIMITS	MEAN.	୍ଷ୍ଟିବର ବିଷ୍ଟି ବିଷ୍ଟ ବିଷ୍ଟି ବିଷ୍ଟ ବିଷ୍ଟି ବିଷ୍ଟି ବିଷ୍ଟି ବିଷ୍ଟି ବିଷ୍ଟି ବିଷ୍ଟି ବିଷ୍ଟି ବିଷ୍ଟି ବିଷ୍ଟ ବିଷ୍ଟି ବିଷ୍ଟି ବିଷ୍ଟି ବିଷ୍ଟି ବିଷ୍ଟି ବିଷ୍ଟି ବିଷ୍ଟି ବିଷ୍ଟ ବିଷ୍ଟି ବିଷ୍ଟ ବି
STATIC		29 KIRS KIRS KIRS KIRS KIRS KIRS KIRS KIRS
.IMIT 7583.	TEST CONDITION	200 - 11
ENDURANCE LIMIT	TEST	PULLUP LEGEL PULLUP PULLUP LEGEL PULLUP LEGE
IN-LB	ġ	<u>፞</u> ዸጜጜኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯኯ
HD= 4000 FT	.080	6 ද 2 ද 2 ද 2 ද 2 ද 2 ද 2 ද 2 ද 2 ද 2 ද
6 e STA.5.0 192.4 IN HD*	MEAN.	ද්‍රික්ක්ක්රිය් ද්‍රික්ක්ක්රිය් දේශයෙන්නෙන්නෙන්න් ස්ව්ක්ක්කික්කෙන්නෙන්නෙන්නේ සේක්ක්ක්කික්කෙන්නෙන් දේශයෙන්නෙන්නෙන්නෙන්නෙන්නෙන්නෙන්නේ සේක්ක්කික්කික්කෙන්නෙන්නෙන්නෙන්නෙන්නෙන්නෙන්නෙන්නෙන්නෙ
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	STATIC LIMITS	MEAN.	ທ່ວຍ ବ୍ରତ୍ତ୍ର ବ୍ରତ୍ତ Ψ
naea	ENDURANCE LIMIT 22610. STATIC	TEST CONDITION	REVERSA. MOD. — 136 KIRS CONT. REVERSA. — 119 KIRS UP. LEVEL R. 16HT — 95 KIRS UP. LEVEL R. 16HT — 195 KIRS AUTO. 324 RRH — 95 KIRS AUTO. 324 RRH — 95 KIRS AUTO. 324 RRH — 95 KIRS AUTO. 339 RRH — 95 KIRS AUTO. 339 RRH — 95 KIRS TURN. RECOVERY — 95 KIRS SIDESLIP — 78 KIRS SIDESLIP — 78 KIRS SIDESLIP — 136 KIRS SIDESLIP —
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o and a	UNITS HD= 4000 FT	.390	% සිට යු
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	PARPMETER M.R. MAST BENDING @ 0. DEG. TOG4- BEGS LB TOG6- 192.4 IN	NO. TEST CONDITION	1. NURPL START 0-100% NR 2. NURPL START 0-100% NR 3. NURPL FAREDFF 4. DUF TAREDFF 7. HOUR THR. LEFT 10. HOUR THR. LEFT 11. SIDELARD FIGHT - REPERSAL 11. SIDELARD R. IGHT - REPERSAL 12. SIDELARD R. IGHT - REPERSAL 13. SIDELARD R. IGHT - REPERSAL 14. LEVE R. IGHT - 102 KIRS 15. LEVE R. IGHT - 102 KIRS 16. LEVE R. IGHT - 102 KIRS 17. LEVE R. IGHT - 102 KIRS 18. LEVE R. IGHT - 102 KIRS 19. LEVE R. IGHT - 102 KIRS 22. LINE 1000 FFM - 70 KIRS 23. LEVE R. IGHT - 105 KIRS 24. LINE 1000 FFM - 105 KIRS 25. LINE 1000 FFM - 105 KIRS 26. LINE 1000 FFM - 105 KIRS 27. LINE 1000 FFM - 105 KIRS 28. LINE 1000 FFM - 105 KIRS 29. LINE 1000 FFM - 105 KIRS 20. LINE 1000 FFM - 1000 FFM - 105 KIRS 20. LINE 1000 FFM - 1000 FFM - 1000 FFM - 1000 KIRS 20. LINE 1000 FFM -

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22610. STATI		113.8 KIRS 113.8 KIRS 113.9 KIRS 113.0 KIRS
ENDURANCE LIMIT 226	TEST CONDITION	17. REVERSAL. MOD. — 17. REVERSAL. MOD. — 18. REVERSAL. — 18. REVERSAL — 18. RE
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PARAMETER M.R. MAST TOGA- 8685	NO. TEST	
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TABLE G-2 - Continued

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STATIC LIMITS	MEGN.	ਜ਼ੑੑਫ਼ਫ਼ੑਫ਼
ENDURANCE LIMIT 71549.	NO. TEST CONDITION	51. TURN REVERSAL, MOD 136 KIRS 52. PGA CONT. REVERSAL - 119 KIRS 53. DATLOP. LEVER R. 1647 - 70 KIRS 55. PULLUP. LEVER R. 1647 - 70 KIRS 55. PULLUP. LEVER R. 1647 - 185 KIRS 56. PULLUP. LEVER R. 1647 - 185 KIRS 57. PULLUP. LEVER R. 1647 - 185 KIRS 58. PULLUP. LEVER R. 1647 - 185 KIRS 59. PULLUP. LEVER R. 1647 - 185 KIRS 60. PULLUP. LEVER R. 1647 - 185 KIRS 61. STAB. AUTO. 324 RRH - 85 KIRS 62. STAB. AUTO. 324 RRH - 85 KIRS 63. STAB. AUTO. 324 RRH - 85 KIRS 64. STAB. AUTO. 339 RRH - 85 KIRS 65. STAB. AUTO. 339 RRH - 85 KIRS 66. STAB. AUTO. 339 RRH - 85 KIRS 67. AUTO TURN, LEFT - 70 KIRS 68. AUTO TURN, LEFT - 70 KIRS 69. AUTO PURN, RIGHT - 136 KIRS 69. DIUE. STEADY - 119 KIRS 69. DIUE. STEADY - 119 KIRS 69. DIUE. RIGHT TURN - 119 KIRS 69. CLIMB. MAX. RATE. RIGHOUR- 136 KIRS 69. CLIMB. MAX. RATE. RIGHOUR- 136 69. CLIMB. MAX. RATE.
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PARPHETER M.R. HUB CHORD BENDING @ 9	NO. TEST CONDITION	1. NORTH. STRRT 0-100% NR 2. NORTH. STRRT 0-100% NR 3. NORTH. TAKEDER 6. HOUR LINE, LEFT 30 DEG-SEC 10. HOUR LINE, LEFT 30 DEG-SEC 10. HOUR LINE, LEFT 30 DEG-SEC 11. SIDELARD R. LIGHT - REPT 12. SIDELARD R. LIGHT - REPT 13. REPRESAL 14. LEVEL R. LIGHT - REFT 15. LEVEL R. LIGHT - REFT 16. LEVEL R. LIGHT - REFT 17. LEVEL R. LIGHT - REFT 18. LEVEL R. LIGHT - REFT 19. LEVEL R. LIGHT - LEFT 19. LEVEL R. LIGHT - REFT 19. LEVEL R. LIGHT R. LIGHT REFT 19. LEVEL R. LIGHT R.

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	STATIC LIMITS	MEAN.	୍ଦିର୍ଦ୍ୱର ବ୍ରତ୍ତ୍ୱର ବ୍ରତ୍ତ
	ENDURANCE LIMIT 5054. STATIC	TEST CONDITION	TURN REVERSAL, MOD 136 K1AS FFA CONT. REVERSAL - 119 K1AS FORLUP, LEVEL FLIGHT - 85 K1AS FULLUP, LEVEL FLIGHT - 85 K1AS FULLUP, LEVEL FLIGHT - 127 K1AS FULLUP, LEVEL FLIGHT - 126 K1AS FULLUP, LEVEL FLIGHT - 70 K1AS FULLUP, LEVEL FLIGHT - 70 K1AS FULLUP, LEVEL FLIGHT - 70 K1AS FULLUP, LINE TO HOUER FULLUP, LEVEL FLIGHT - 136 K1AS FULLUP, LINE FULLUP - 119 K1AS FULLUP, LINE FULLUP - 136 K1AS FULLUP - 1
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	HD= 4000 FT	.080	11 0 11 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	₽ N	MEAN.	ନ୍ତ୍ର ପ୍ରତ୍ତର ପର ପ୍ରତ୍ତର ପରତ୍ତର ପର୍ବତର ପର ପରତ୍ତର ପରତ୍ତର ପର ପର୍ବତର ପର ପରତ୍ତର ପରତ୍ତର ପର୍ବତର ପରତ୍ତର ପରତ୍ତର ପରତ୍ତର ପର ପରତ୍ତର ପରତ୍ତର ପର ପରତ୍ତର ପରତ୍ତର ପରତ୍ତର ପରତ୍ତର ପର ପରତ୍ତର ପରତ୍ତର ପରତ୍ତର ପର ପରତ୍ତର ପରତ ପରତ୍ତର ପରତ୍ତର ପରତ୍ତର ପରତ୍ତର ପରତ ପରତ୍ତର ପରତ ପରତ୍ତର ପରତ ପରତ୍ତର ପରତ୍ତର ପରତ୍ତର ପରତ୍ତର ପରତ୍ତର ପରତ୍ତର ପରତ ପରତ ପରତ୍ତ ପରତ୍ତର ପରତ ତତ ତ ତତ
	PARAMETER THRUST LINK LOAD TOGA= 8685 LB TOGS= 192.4 II	NO. TEST CONDITION	1. NORMAL START 0-1002 NR 2. NORMAL START 0-1002 NR 3. NORMAL START 0-1002 NR 4. JUTP TAKEDFF 4. JUTP TAKEDFF 5. HOURE IGE 234 RPH 11. SIDEJARD R.IGHT 30 DEG-SEC 11. SIDEJARD R.IGHT - RIGHT 12. SIDEJARD R.IGHT - LEFT 13. SIDEJARD R.IGHT - LEFT 14. EVEL R.IGHT - REVERSAL 15. EVEL R.IGHT - RIGHT 16. EVEL R.IGHT - REVERSAL 16. EVEL R.IGHT - REVERSAL 17. EVEL R.IGHT - REVERSAL 18. EVEL R.IGHT - REVERSAL 19. EVEL R.IGHT - REVERSAL 19. EVEL R.IGHT - 102 R.IGHS 19. EVEL R.IGHT - 102 R.IGHS 19. EVEL R.IGHT - 102 R.IGHS 19. EVEL R.IGHT - 103 R.IGHS 19. EVEL R.IGHT - 105 R.IGHS 19. EVEL R.IGHT - 105 R.IGHS 22. CLIMB 1500 FPH - 70 R.IGHS 23. CLIMB 1500 FPH - 105 R.IGHS 24. CLIMB 1500 FPH - 105 R.IGHS 25. CLIMB 1500 FPH - 105 R.IGHS 26. CLIMB 1500 FPH - 105 R.IGHS 27. CLIMB 1500 FPH - 105 R.IGHS 28. CLIMB 1600 FPH - 105 R.IGHS 29. CLIMB 1600 FPH - 105 R.IGHS 20.
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	LIMIT 1580. STATIC LIMITS +4400., -2550.	TEST CONDITION MEAN. GSC.	## MOD. — 136 KIRS ## MOD. — 136 KIRS ## KEUERSAL — 119 KIRS ## KIRSSAL — 119 KIRS ## KIRS #
LE G-2 - Continued	UNITS LB ENDURANCE LIMIT	DSC. NO. TEST	111.5
TABLE	192.4 IN HD= 4880	MEAN.	აგი განამან გ
	PARAMETER PITCH LINK LOAD TOGS-	NO. TEST CONDITION	1. NORTH START 0-100% NR. NORTH TOKENTY 100-0% NR. JUPP TAKEDIT 100-0% NR. JUP

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, STATIC LIMITS +20518,-141	MEAN. OSC.	136 K185 119
ENDURANCE LIMIT 5920.	. TEST CONDITION	TURN REVERSAL, NOD F-A CONT. REVERSAL - LIT. CONT. REVERSAL - DIR. CONT. REVERSAL - PULLUP, LEVEL R. IGHT - RATHER AUTO, 324 RRH - STAB. AU
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HD= 4000 FT	OSC.	#####################################
P NI	MEGN.	මුද්දර්දර්ගී මේ දැන්වා දින්වා
PARAMETER M.R. BLADE DRAG BRACE LOXI TOGA: 8695 LB TOGE 192.4	NO. TEST CONDITION	1. NORTH. STRRT 0-100% NR. 1. NORTH. TAKEDER 1. JUTP TAKEDER 1. HOVER TURN, LEFT 30 DEG-SEC 1. SIDELARD P. IGHT - LEFT 1. SIDELARD P. IGHT - LEFT 1. LEVE R. HIGHT - 119 KIRS 1. LINE 1000 FFM - 85 KIRS 1. LINE 1000 FFM - 110 KIRS 1. LEFT TURN, 105 KIRS 1. LEFT TURN, 10

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TABLE G-2 - Continued	STATIC LIMITS	MEAN.	୪ ୫୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪୪
	ENDURANCE LIMIT STATIC	TEST CONDITION	TURN REVERSAL, MUD. – 136 KIAS LAT. CONT. REVERSAL. – 119 KIAS LAT. CONT. REVERSAL. – 119 KIAS PULLUP, LEUEL F. LIGHT – 85 KIAS PULLUP, LEUEL F. LIGHT – 85 KIAS PULLUP, LEUEL F. LIGHT – 119 KIAS PULLUP, LEUEL F. LIGHT – 127 KIAS PULLUP, 224 RP1 – 28 KIAS PUTO TURN, LETT – 70 KIAS PUTO TURN, LETT TURN – 119 KIAS PUTO, STEBAL P – 70 KIAS PUTO, STEBAL P – 70 KIAS PUTO, STEBAL P – 105 KIAS PUTO, STEBAL P – 105 KIAS PUTO, STEBAL P – 105 KIAS PUTO, TURN PULLUP – 119 KIAS PUTO, TURN, RATE, PUSHOVER – 70 PUTOR, STOP – 136 KIAS TO HOUER.
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	4000 FT	osc.	ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼୷୳୳ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼ଡ଼୴ଡ଼୴ଡ଼୴ଡ଼୷ୠ୴ଡ଼୴ୣୣୣଌ୷ଡ଼୴ଡ଼ୄୡୄୡ ୢୡୡୄଌଌୢଌୡୄଌୡୡଌୄଌୡୡୄଌୄ୷୷୷୷ଌଌୄଌୡୡଌୄଌୡୡୡୡୡୡୡୡୡୡ
	÷	MEAN.	ବିଷ୍ଟ୍ରି କରି ବିଷ୍ଟ୍ର କରି କରି ବିଷ୍ଟ୍ର କରି କରି କରି କରି କରି କରି କରି କରି କରି କର
	PARAMETER TEETER ANGLE TOCG= 192.4 IN	NO. TEST CONDITION	1. NURTH, START 0-1002, NR. 2. NURTH, START 0-1002, NR. 3. NURTH, START 0-1002, NR. 5. HOUER TURN, LEFT 30 DEG-SEC. 6. HOUER TURN, LEFT 30 DEG-SEC. 11. SIDELARD R. IGHT 30 DEG-SEC. 12. SIDELARD R. IGHT - REPERSAL 13. REPRESAL 14. SECRETARY R. IGHT - REPRESAL 15. LEVEL R. IGHT - REPRESAL 16. LEVEL R. IGHT - REPRESAL 17. LEVEL R. IGHT - REPRESAL 18. LEVEL R. IGHT - REPRESAL 19. LEVEL R. IGHT - LEFT RIPS 22. CLIMB 1000 FFM - 70 KIRS 23. CLIMB 1000 FFM - 70 KIRS 24. CLIMB 1000 FFM - 105 KIRS 25. CLIMB 1000 FFM - 105 KIRS 26. CLIMB 1000 FFM - 105 KIRS 27. CLIMB 1000 FFM - 105 KIRS 28. CLIMB 1000 FFM - 105 KIRS 29. CLIMB 1000 FFM - 105 KIRS 20. LIMB 1000 FFM - 100 KIRS 20. LIMB 1000

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	ENDURANCE LIMIT	TEST CONDITION	P. LEUEL P. P. LEGEL
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